

HT-1200 6 Phase Relay & Protection Tester

OPERATION INSTRUCTION

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RELAY PROTECTION TEST ITEM INDEX

The index is designed to guide the tester that all kinds of the relay protection device test can be done by the following series which modules of software.

Relay test:

Relay protection type	Test Item	Proposed test module	Remarks
Signal relay	Corresponding test items	DC Test AC and DC Test	If the intermediate relay is required AC/DC hybrid input, please test in 'The AC And DC Test 'module. If Rated current of the signal relay is too small, please use the voltage loop output of tester to do experiments.
Time relay			
Intermediate relay			
Coincidence relay			
Other DC voltage and current relay			
Current relay	Corresponding test items	AC Test	The sequence component relay can be tested in the special sequence module of 'AC Test'. The inverse time relay can be tested in the "It characteristics" module.
Over (under) voltage relay			
Sequence component relay			
Synchronous check (or phase comparison) relay			
Inverse time current relay			
Differential relay	DC magnetic feature	Differential Relay,	Please refer to point 9 of "Appendix 3" in the manual for correct wiring during the test
	Harmonic braking feature	Differential Harmonic, AC/DC Test, Harmonic Test	
	Proportional braking feature	Differential Relay, AC Test	
Power (directional) relay	Corresponding	Power Direction	Before testing the power (direction)

Impedance relay	test items	&Impedance, AC Test	relay, the type of connection and the action boundary of the protection should be determined in advance.
Synchronous relay	Corresponding test items	Synchronization Test, AC Test	UA, UC of tester is fixed as the system side and the side to side voltage output for 'Synchronization Test' module.
Frequency relay	Corresponding test items	High-Low Frequency Test	When the 'automatic frequency conversion' method is chosen in the single machine, the frequency slip value can be measured.

Computer protection test:

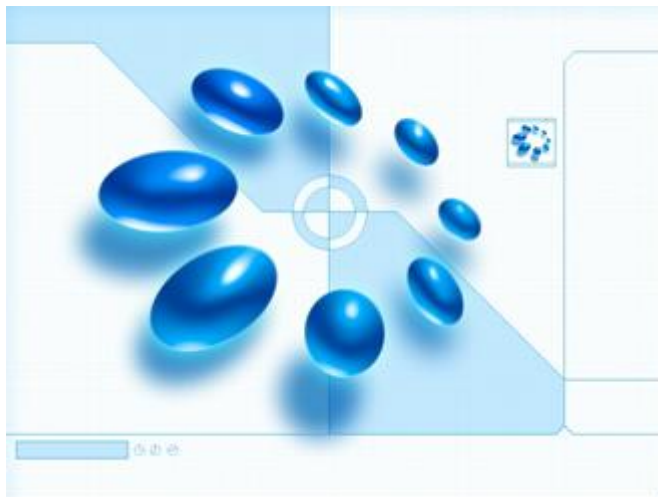
	Relay protection type	Test Item	Proposed test module	Remarks
Line protection	Multi-section over current	Corresponding test items	AC Test	As long as the method is proper, the tests of most relays and microcomputer protection can be done by the 'AC Test' module, which should be selective learning.
	Over (under) voltage			
	Sequence component voltage and current			
	Frequency device			
	Power direction protection			
	Reclosing and transform fault	Corresponding test items	Full Group Test, State Series, Comprehensive Test of Line Protection of 6-35 KV Microcomputer	Requirement that if the Synchronization check and no-voltage check test is done, the Ux as the side and side voltage output and the tester is to use Ua instead of Ux for testing.

	Distance & Zero Sequence Protection,	The Setting value verification of Distance & Zero Sequence Protection	Distance & Zero Sequence Protection, Full Group Test, AC Test	"Distance & Zero Sequence Protection" can automatically test multiple sections, various fault types and other distance and zero sequence value.
		Characteristic of Impedance	Characteristic of Impedance	
	Power frequency variation distance	Setting value verification	Distance & Zero Sequence Protection	The fault current should be large enough, such as 10~15A (when CT is 5A)
	Compound voltage blocking(directional) overcurrent	Over current, low voltage, negative sequence voltage, sensitive angle	AC Test, Comprehensive Test of Line Protection of 6-35 KV Microcomputer	Some of the protection of the "low voltage" and "negative sequence voltage" input by different terminal, replacing the wiring is necessary in the test.
Low cycle, low voltage load shedding device	Corresponding test items	High-Low Frequency Test, Comprehensive Test of Line Protection of 6-35 KV Microcomputer	If other conditions are satisfied, the device cannot move, please confirm whether the device also need to input current and switch contacts	
The generator transformer protection	Differential protection	Proportional braking characteristic	Differential Protection, Differential Value, AC Test	When the differential protection is used in the differential protection of generator, it can be regarded as the transformer

		Harmonic braking characteristic	Differential Protection, Differential Value, Harmonic Test	protection with the connection type of Y/Y, high and low voltage side balance coefficient of 1. "Differential protection" module pay attention to the curve characteristic search and the "differential value" module focuses on the differential value test. Their combination can test the differential protection.
	Loss of magnetic protection	Corresponding test items	AC Test	The angle of output voltage and current should be paid attention in the test.
	Excitation protection			
Other protection	Automatic quasi synchronization device	Corresponding test items	Synchronization Test	To do the automatic adjustment test, the line must be in accordance with the requirements of instruction when testing the input.
	Busbar differential protection	Corresponding test items	AC Test	Please refer to the description of BP-2B and RCS-915 in point 6 of "Appendix 4" "Partial Protection of NARI"
	Optical fiber line differential protection			Before the test to determine whether the device to form a "self loop", if, then the protection of the action value should be equal to half of its set value.

PART 1

Instruction on Relay tester



Chapter 1 Device features and technical parameters

Section 1 Main features

◆ Flexible combination of voltage and current output

Six phase voltage and six phase current can be output, which has made it is possible to be any combination, such as the output mode of the combination of conventional four phase current and three-phase current, six phase voltage mode, six phase current mode and 12 phase output mode. It not only can be compatible with the traditional way of various tests, but also can conveniently carry out differential test of three-phase transformer.

◆ Operation mode

The device is directly connected with a computer or a desktop computer, which is convenient and efficient and stable performance.

◆ A new hi-fi linear power amplifier

The output port has always insisted on using the modular linear power amplifier instead of the switching power amplifier, which has the high fidelity and high reliability function and excellent performance. High-mid frequency will not be produced to disturb the test, also ensure the smoothing accuracy of waveform produced by the whole course of the high current to the tiny current is excellent.

◆ High performance Main.

The output part adopts DSP control, which has fast operation, real-time digital signal processing capability, wide bandwidth and high resolution D/A conversion control. The output waveform has the features of high precision, small distortion and good linearity. With using a large number of advanced technology and precision components and materials and the structure of professional design, the device has the features of small volume, light weight, full function, easy to carry, boot can work, flow test is very convenient.

◆ Powerful software function

It can complete all kinds of high automatic validation work which is large and complex. It can also conveniently test and scan protection setting, playback of fault, real-time store test data, display vector, online print report and so on. Besides, six-phase current can facilitate the test of three-phase differential protection.

◆ Independent DC power output

An 110V and 220V adjustable DC power is designed to supply output.

◆ Complete interface

The device with USB communication port can communicate with the computer and other external devices.

◆ Perfect self-protection function

With reasonable design of the heat dissipation structure and the reliable and perfect hardware protection measures, it has the power soft start function and the software of the fault self-diagnosis and the output latch function.

Section 2 Nominal parameter

◆ Parameter

Type	-
Current channel number	Standard six phase
Voltage channel number	Standard six phase
AC current output range	30A / phase or 180A (six phase parallel)
DC current output range	10A DC /phase
AC voltage output range	120V AC /phase
DC voltage output range	160V DC / phase

◆ Nominal parameter

AC current output

The virtual value of each phase output when six phase current output 0~30A

output precision 0.1 grade

The virtual value of each phase output when three phase current output 0~60A

The virtual value of six phase parallel current output 0~180A

The allowed virtual value when the phase current work long time 10A

The maximum output power of phase current 450VA

The maximum output power when six phase parallel current output 1000VA

The allowed working time when six phase parallel current maximum output 10s

Frequency range (fundamental wave) 0~1000Hz

Harmonic order 0~20

DC current output

Current output 0~±10A / phase output precision 0.2 grade

The maximum load voltage output 20V

AC voltage output

The virtual value of phase voltage output 0~120V output precision 0.1 grade

The virtual value of line voltage output 0~240V

The output power of phase voltage/ line voltage 80VA / 100VA

Frequency range (fundamental wave) 0~1000Hz

Harmonic order 0~20

DC voltage output

The output amplitude of phase voltage 0~±160V output precision 0.2 grade

The output amplitude of line voltage 0~±320V

The output power of phase voltage/ line voltage 70VA / 140VA

Input and output

8 channels input

Free contact 1~20mA, 24V

Electric potential contacts "0": 0 ~ +6V; "1": +11 V ~ +250 V

4 channels output DC: 220 V / 0.2 A; AC: 220 V / 0.5 A

Time measurement range

0.1ms ~ 9999s , measurement accuracy <0.1ms

Chapter 2 Hardware Structure

Section 1 Hardware Structure

◆ Digital Signal Processor Microcomputer

High-speed digital controlling processor is adopted as the output core of the tester. 32 bit double precision arithmetic is employed in the software, through which arbitrary high-accuracy waveforms of each phase can be produced. Since integrative structure is adopted, the structure of the tester is layed compactly. The distance of data transmission is short with tight structure, which overcome the problem of fewer points of waveform output due to long data communicational line and narrow frequency band when using the test controller controlled directly by PC.

◆ D/A Conversion and Low-Pass Filtering

High precision D/A converter is employed for ensuring the precision and linearity of current and voltage in the whole range.

Due to high density of fitting ponit, fidelity of waveform is high and harmonic component is small, which don't have a strict requirement on the low-pass filter. Consequently, it has good characteristics of transient, phase frequency and amplitude frequency, which is easy to perform accurate phase-shifting and harmonic superposition and ensures very high precision even when the frequency is high.

◆ Voltage and Current Amplifier

For phase current and voltage, we persist in adopting high performance linear amplifier output mode in order to make the current and voltage source to directly output all kinds of waveforms from the DC waveform to the waveforms including all kinds of frequency components, such as square wave, combined waveform overlapped by each order harmonic, fault transient waveform, etc. In addition, the output waveform is clear and smooth without high-frequency radiated interference with neighboring equipments. It can simulate well all kinds of current and voltage characteristics under the circumstance of short circuit fault.

For power amplifier circuit, we adopt import power parts with high-power and hi-fi module style as power output, combining with heat dissipation structure layed elaborately and reasonably, it has enough large power redundancy and thermal capacity. The power amplifier circuit has overheat, overflow, overvoltage and short circuit protections. When overflow occurs in the current

circuit and overload or short circuit occurs in the voltage circuit, it will limit the output power automatically, switch off the whole power amplifier circuit and give alarm signal. In order to prevent the overheat of the power amplifier for long time operating under large current, a software time terminating system under large current is set in this tester. It can work for a long period when outputting is 10A or below. When the current is over 10A, the tester will start up the software time termination order. When time is up, the software will forbid power output automatically and give alarm signal. The higher output current is, the shorter the limiting time will be.

◆ Input and output

This tester has 8 channels input and 4 channels output.

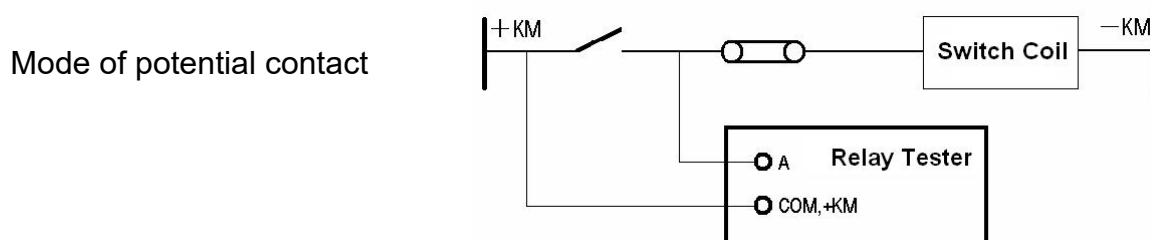
The switching input circuit is compatible for both the empty contacts and 0-250V electric potential contacts in the input and output circuit. When the electric potential contacts are selected, 0-6V belongs to closed switch and 11-250V belongs to open switch. The switching capacity can test the action time and the action time interval of every phase switch's contact conveniently.

The part of the digital input is isolated from the resources of the mainframe and the amplifier. The end of the digital input is hung, so the common end of the digital input is separated from the Common End UN, IN of current and voltage parts.

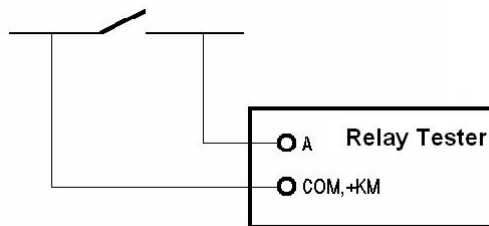
Switching potential input has directivity, you should connect the common end with the positive terminal of potential, and connecting the input end with negative terminal of potential for ensuring the potential of common end is higher than the one of input end. In practice, you should connect the input common end with +KM, and connecting the negative terminal of contact with input end.

The output part is the idle contact output of relay. Output capacity is DC: 220V / 0.2A, AC: 220V / 0.5A. Output of switching capacity is independent of voltage, current, input and all other parts. Action process of each digital output part is different in each testing module. For details, please refer to the operation instruction on software module.

The connection diagram of two kinds of familiar digital output is as follows:



Mode of free contact



◆ Auxiliary DC Power Supply Output for Special Use

A circuit of special adjustable DC power supply output is allocated on the rear panel, which has 110V and 220V two shifts that can be used as test standby power supply on the spot. We still set a potentiometer for this power supply, it can be adjusted within the range of 80% – 110%. Rated current of this power supply is 1.5A, which can be used as DC power supply of protective tester or switch loop supply. If overload or short circuit occurs, corresponding protector tube will be burned out (2A / 250V), you will only need to change this protector tube at that time.

Chapter 3 Please Read the Following Instruction before Operation

Section 1 General Rules for Use

- ◆ Please do not shut off power supply directly during outputting so as to avoid the wrong protection action due to incorrect output.
- ◆ When switch quantity is compatible with both idle contact and the potential (0 ~ DC250V) and uses charged contact, the high terminal (anode) of contact potential should be connected with the common end +KM.
- ◆ When taking the tester into operation, make sure that the air slots, the power switch and the power supply plug at the test set remain unobstructed. The instrument should be laid uprightly, or unfold the bracket for slightly tilted placement
- ◆ Do not lead external AC/DC power into the voltage and current output sockets of tester.
- ◆ If the disturbance is stronger on the spot or high safety is required, before doing the test, please ground the outlet of power source or the protective earth of the tester.
- ◆ If the interface data is wrong or you can not input correctly when using this tester, you can settle the problem as follows: delete the 'para' file under the 'E\Relaytestar\, and then restart the running program, all data on the interface will be resumed to the default.

Section 2 Procedures of turning on/off Tester

◆ Procedures for Turning On

- Plug the power line of tester in AC220V outlet. If using external computer, please connect well the serial communication line with computer's serial interface and the communication interface on the bottom of the tester.

Method one: Start up the Windows operating system firstly, and then enter the main software interface of 'Relaytestar'.

Method two: It wills automatic recover the Windows operating system, which will need four minutes. Then enter the interface which can choose the way of starting up. This way is mainly used when the Windows operating system is damaged and cannot normal start, which can make the Windows operating system restore to factory settings. The user cannot worry that the previous test report and data will be losing after self-recovery. But this way will take much time and it is not the best choice to often use.

Method three: This way will enter DOS state and mainly used by the management personnel. If the user enters DOS state carelessly, please turn off the power and wait a moment to boot again.

You can use the up and down key or '1','2','3' number key to choose the boot way within five seconds, otherwise the system will automatic start up by method one. The software interface will be showed after the Windows operating system started up. On the main interface, click all kinds of functions testing module logo by using the left key of external connected mouse or tracking ball mouse for doing all tests.

◆ Procedures for Turning Off

Please do not close down the power switch on the faceplate directly. You should terminate the Windows operating system firstly, and then press the power supply button when indication for safe turning off appears on the screen.

- Move cursor on the main interface through mouse or press the 'QUIT' key on the faceplate to quit all functional testing units. After backing to the main interface, press the 'QUIT' key again, a dialog window for confirmation will be ejected on the screen. After your confirmation, you can turn off the power supply switch on the front panel when 'You can turn off the power supply now' appears on the screen, so the machine can be closed safely.
- You can also turn off the device by choosing the 'start' menu of the operation system.

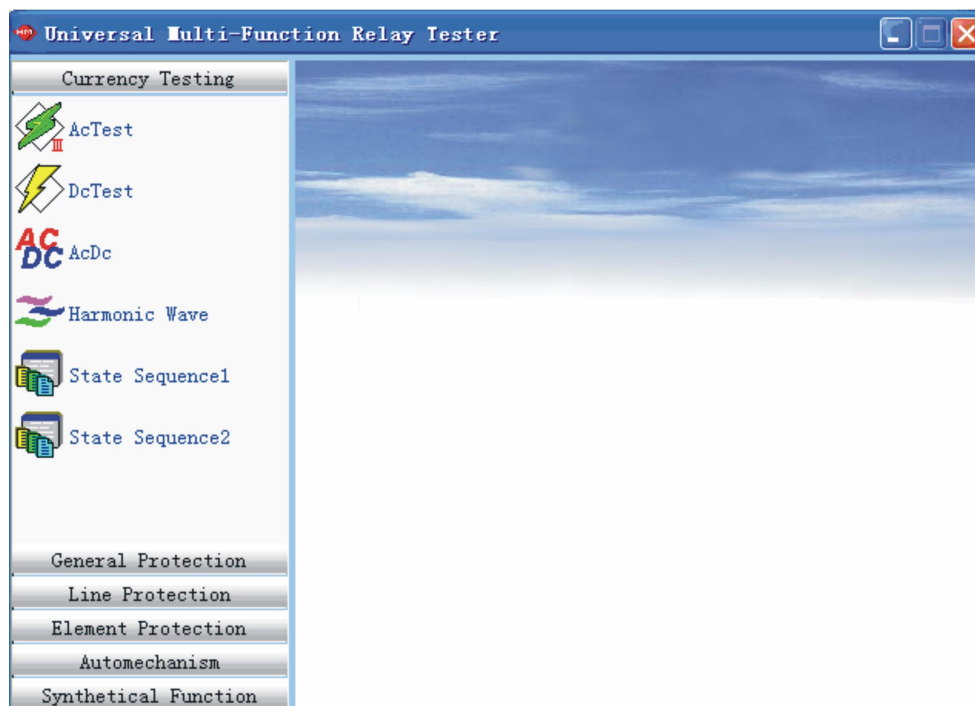
PART 2

Instruction on Software Operation of Relaytestar



Chapter 4 Brief Instruction on Software Operating Method

The Relaytestar software is new generational testing software developed by Wuhan human Company. Its characteristics are more friendly and beautiful interface, more complete and powerful functions, and it also preserves its unique characteristic of simple and concise interface, easy operation and easy to learn. According to different functions of each testing module, we separate the testing modules to five groups, general testing, common protection, circuit protection, components protection and comprehensive function. Each group includes some sub-menus, such as the 'common testing' includes 'AC Test', 'DC Test', 'Harmonic Superposition', 'State Series I' and 'State Series II', and it can be extended at will. On the right of this window, it displays rolling introduction about the company.



Section 1 Introduction on Common Functions in Menu Bar

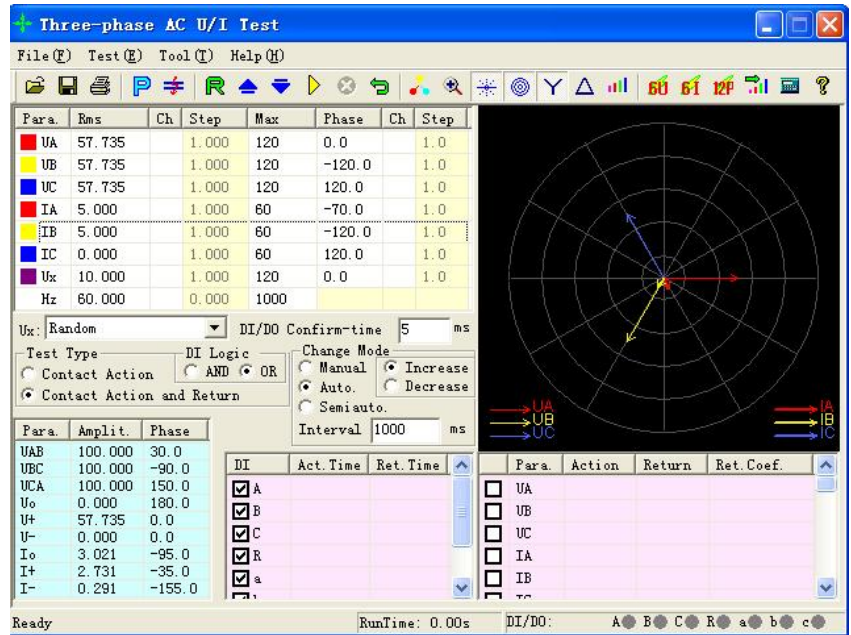
Name or symbols of menu items in every testing module are the same, and its definition and function are almost identical. We take the 'AC Test module as example for introduction, which can be applied for all functional modules.

- **Opening file :** The shortcut key is Ctrl+O, which is used for calling out testing parameters saved in appointed file and showing the parameters on software interface. If clicking

this function, the testing parameters of current module will be saved as the following default path :E:\Relaytestar\Para\name of current module\.

● **Saving parameters:**

The shortcut key is Ctrl+S, which is used for saving the testing parameters on software interface and call out them again by using 'Opening parameter' later. Data will be saved in the default file of the current module.



● **Reporting Test :**

Shortcut key is Ctrl+R, which is used for calling out the test report saved in appointed file.

The contents of test report will be displayed in the test report window and revising or printing the test report can be completed in this window. After every test, a dialog box will be ejected by the system to save the test report. The report will be saved as the following defaulted path: E:\Relaytestar\Test Report\name of current module\

- **Exit:** Shortcut key is Ctrl+X, which is used for exiting current testing module.
- **Start Test:** It has identical function as the run key, which is used for starting the test.
- **Stop Test:** It has identical function as the ESC key, which is used for ending the test normally or compelled terminating program running.
- **Short Circuit Calculation:** After clicking it, a 'short circuit calculation' dialog box will be opened, which is used for short circuit calculation and automatically fill the interface with the calculated results when fault occurs just like the right chart shows. Note that zero sequence compensating factors must be set correctly when the fault type is grounding fault.

Section 2 Introduction on Common Button in the Tool Bar



Button for opening test parameters (the function is the same as above-mentioned one)



Button for saving test parameters (the function is the same as above-mentioned one)



Button for returning data (for returning parameters to the initial value before the test,

which is very convenient for many times repeatable tests)



Button for printing test report (the function is the same as the above-mentioned one)



Button for starting the test (the function is the same as the above-mentioned one)



Button for stopping the test (the function is the same as the above-mentioned one)



Short Circuit Calculation Button (the function is the same as the above-mentioned one)



Button for starting power displaying interface In the module of 'AC Test', you can open the power displaying interface during the test and compare the actual output power of tester with the power measured by the measurer on the spot.



Synchrometer In the module of 'synchronization test', you can start the synchrometer during the test to observe the test visually.



Variable Step Increase Button When the 'manual operation' is selected, press this button to increase manually one step size of variable value. It do the same function as the "↑"button on keyboard of tester. This button is noneffective during automatic testing and it will become gray automatically.



Variable Step Degression Button When the 'manual operation' is selected, push this button to reduce manually one step size of variable value. Its function is the same as the "↓"button on keyboard of tester. This button is noneffective during automatic testing and it will become gray automatically.。



Vector Diagram Some testing modules can't contain voltage-current vector diagram due to layout problem. You can open it through this button.



Magnifier for magnifying or reducing the current-voltage vector diagram on every module's interface.





Help Button for checking the version information of the current testing module.and others





Balanced output button for outputting symmetrical current and voltage, which means you only need to change the value of any phase, then other phases will output amplitude and phase automatically according to symmetrical three-phase AC quantity. If


one phase is changeable, other phases will be variables correspondingly.

 **Recover Ex-factory Parameter Setting** Click this button for recovering all testing parameters on the interface to the state of ex-factory default setting. Its function is equal to delete the 'para' file in the'Relaytestar' folder.

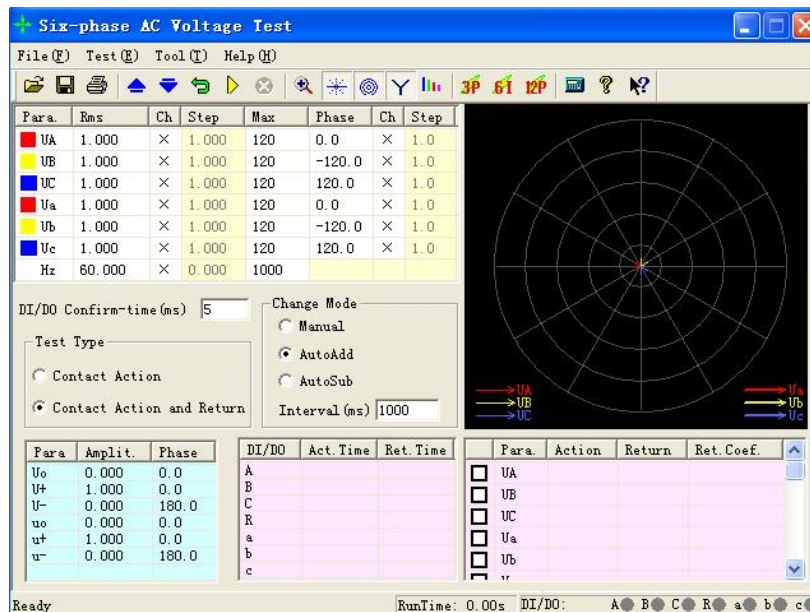
 **Switch to sequence component output** It is a latest developed function. You can switch to a special sequence component testing interface by clicking this button. For utilizing this function, the following conditions must be required: 1. There is this icon In the tool bar of current running 'AC Test' interface ; 2. There is the document of 'thres-phase AC test—output component in sequence' in the folder of 'Relaytestar'

 **6-phase Voltage Testing Interface** Click this button into the 6-phase voltage testing interface. Then, the message 'whether really getting into another testing program' appears, you should select confirmation to enter 6-phase voltage testing interface. The interface is shown below. (a 3P button will appear on the interface at that time, click this button to return to the 3-phase system interface showed above.

 **6-phase Current Testing Interface** Click this button into 6-phase current testing interface. At that time, the hint like the above 6U will appear on the system, then select the confirmation for getting into 6-phase current testing interface.

 **12-phase Testing Interface** Click this button into 12-phase (6phase current 6-phase voltage) testing interface, and getting into the 12-phase testing interface according to the above mode.

Attention :



Para.	Rms	Ch	Step	Max	Phase	Ch	Step
UA	1.000	×	1.000	120	0.0	×	1.0
UB	1.000	×	1.000	120	-120.0	×	1.0
UC	1.000	×	1.000	120	120.0	×	1.0
Va	1.000	×	1.000	120	0.0	×	1.0
Vb	1.000	×	1.000	120	-120.0	×	1.0
Vc	1.000	×	1.000	120	120.0	×	1.0
Hz	60.000	×	0.000	1000			

Para.	Amplit.	Phase
Uo	0.000	0.0
U+	1.000	0.0
U-	0.000	180.0
uo	0.000	0.0
u+	1.000	0.0
u-	0.000	180.0

DI/DO	Act. Time	Ret. Time
A		
B		
C		
R		
a		
b		
c		

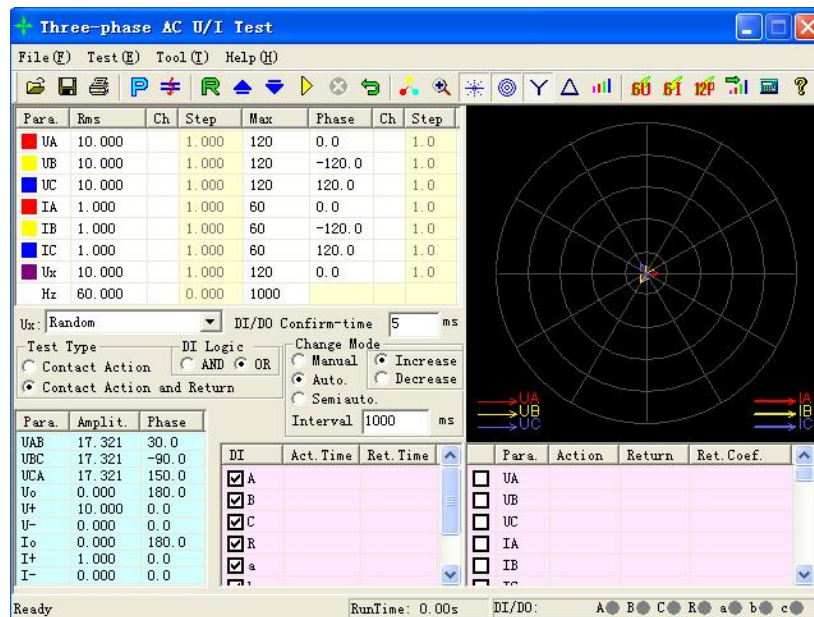
Para.	Action	Return	Ret. Coef.
UA	<input type="checkbox"/>		
UB	<input type="checkbox"/>		
UC	<input type="checkbox"/>		
Va	<input type="checkbox"/>		
Vb	<input type="checkbox"/>		
Vc	<input type="checkbox"/>		

During the operation, if interface data is wrong or you can not input correctly, you can settle these problems as follows: delete the file of 'para' under 'E: \ Relaytestar \ in Windows system, and then restart the operating program, all data on the interface will be recovered to the default.

Chapter 5 AC Test

The 'AC Test' module is a universal and comprehensive testing module. It has an independent testing unit with 4-phase voltage and 3-phase current output, also independent testing units with six phase voltage and six phase current output and an testing unit according to sequence component output, which can be switched between each other through 3P, 6U, 6I, 12P and five buttons of sequence component. Making use of these modules, we can carry out AC testing under all conditions in power system (note: 6 phase voltage, 6 phase current, 12 phase voltage-current function are only intended for Model 1000/1200). Their common features are as following: through setting corresponding voltage or current as variables, giving the variable certain changeable step size and selecting suitable testing mode ('manual operation', 'semi-automation' and 'full-automation' three modes are available) to test action value, return value, action time and return time of all kinds of voltage and current protection conveniently, and calculating return factor automatically. Since the 'four phase voltage and three-phase current' unit is used often and the operating method of other units is basically the same as it, so we only take the 'four phase voltage and three-phase current' as the example to introduce in detail.

- Flexibly controlling output four phase voltage, three-phase current six phase voltage, six phase current, outputting full twelve phase at the same time.
- Having the function of outputting according to phrase sequence component. Through setting the value of phrase sequence component directly, the module combines each phase voltage and current output automatically.
- For each phrase voltage and current output, both amplitude and phase can be set arbitrarily. The amplitude can be set the upper limit.
- Every component's amplitude value, phase and frequency are variable, and the variable step size can all be set at will.
- Ux can be set to be many kinds of output modes combination and also can be set arbitrary value
- Full-automation, self-automation and manually operating are available, which can be switched between each other in the process of output.
- Amplitude, phase, step size and numbers of variable can be revised directly in the status of output.
- Power value can be displayed directly for verifying power measurer.
- Action value, return value, action time and return time can be measured.



Section 1 Interface Instruction

■ Set AC Component

After entering the effective value of voltage and current, click the 'confirmation (enter)' key or move the cursor to other place, the data entered will automatically be saved to three places of decimals. The default unit of voltage is V, and the default unit of current is A. When setting the phase, you can enter any angle in the range of -180° ~ 360° . If the angle overflows the above range, the system will switch it automatically into this range. For example, if entering -181° , it will be altered to be 179° automatically. In the vector diagram window, you can observe the real-time diagram of each AC vector.

The single phase largest output of AC voltage is 120V. If you need to output higher voltage, you can connect any two-phase voltage in series. Their amplitudes may not be the same, but the phases should be reversed. For example: set U_a to output 120V, 0° , and set U_b to output 120V, 180° , then the effective output value of U_{ab} will be 240V.

The single phase largest output of AC current can reach 40A (when six phase current of Model 1000 output at one time, the largest output current of each phase can achieve 20A, and that of Model 1200 can achieve 30A). If larger current output is required, you can adopt parallel connection and the phase of each phase should be the same when operating in parallel. When selecting heavy current output, thicker and shorter lead wire is preferred, in addition, make sure

that output time is as shorter as possible.

The 'variable' column alongside of the effective value set for AC component is used for choosing whether the output component is alterable. If you click the 'variable' column at the back of certain phase's effective value or phase for ' $\sqrt{\quad}$ ', it means that the output phase is alterable. Meanwhile, the 'Step Size' column will be changed from gray to highlight, which indicates the 'Step Size' setting permissible. The smallest value of variable step size of amplitude is 0.001, and the smallest value of variable step size of angle is 0.1.

The column of 'upper limit' is used for setting the largest output effective value of each phase. When doing the test,once the output of certain phase can't be estimated and will result in damage to the relay, you can set an 'upper limit value' for this phase,therefore ,the output of this phase will be controlled within the limit value, which ensure the safe operation of relay.

■ U_x

U_x is a special phase, it can set many kinds of output situations:

- When setting it to be $+3U_0$ 、 $-3U_0$ 、 $+\sqrt{3} \times 3U_0$ 、 $-\sqrt{3} \times 3U_0$, combining U_A and U_B with U_C output currently to obtain $3U_0$ component ,and then multiply their coefficient respectively to obtain the U_x output value.The value always varies along with the change of U_A, U_B and U_C.
- If U_x is set to equal the value of certain phase such as U_A, the output of U_x is the same as the one of corresponding phase.
- If selecting the 'Any Mode', the output of U_x is the same as other three-phase voltage in the range of output and also can vary its amplitude and angle according to certain step size.

Attention:

There are 6 phases voltage output in the Relaytestar-1000/1200 tester, but there is not an independent special phase U_x . Consequently, the program assigned the fourth phase voltage U_a as the special phase U_x.

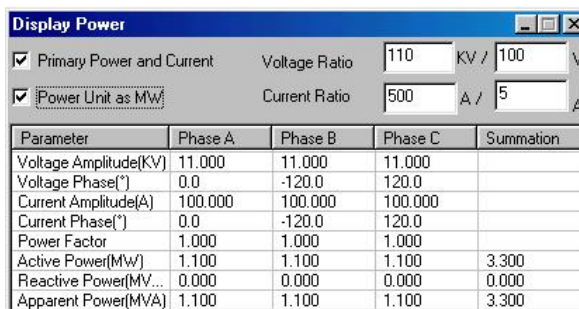
■ Parameters Display

The line voltage, zero sequence, positive sequence and negative sequence components will be shown on the left side of the interface. Through this window, you can monitor the variable situation of 'sequence component' and 'line voltage'. The values of this part are calculated completely according to each phase's component value given above and can't be obtained by setup. Through this window, the operator can observe each sequence component and values of

line voltage when protection is performed, which is convenient for recording the operation data of protection according to different demands. For example, when doing low-voltage latching overcurrent test, if the line voltage is given for protection setting value, you can not only see the value of phase voltage when protection acts visually, but also can read directly the value of phase voltage from this window without calculating by operator themselves.

■ Power Measurer Display Button

When clicking this button, a 'Power Display' box will be ejected just as the right figure shows.



Parameter	Phase A	Phase B	Phase C	Summation
Voltage Amplitude(KV)	11.000	11.000	11.000	
Voltage Phase(°)	0.0	-120.0	120.0	
Current Amplitude(A)	100.000	100.000	100.000	
Current Phase(°)	0.0	-120.0	120.0	
Power Factor	1.000	1.000	1.000	
Active Power(MW)	1.100	1.100	1.100	3.300
Reactive Power(MV...)	0.000	0.000	0.000	0.000
Apparent Power(MVA)	1.100	1.100	1.100	3.300



In this displaying box, all kinds of amplitude, phase, power and other data of secondary side will be displayed default. If the data of primary side needs to be displayed, for example, when verifying on-the-spot meter, you only need to select the 'primary side power and current' and input corresponding TV and TA ratio. Click the 'Power unit is megastage' for conversion the power unit from 'KW、Kvar' to 'MW、Mvar' automatically.

■ 'Contact Action' and 'Action and Return'

- When selecting the 'Contact Action' in the column of testaim, the tester will stop the test automatically when it receives signal of protective action, and will record the data of relay action at that time.
- When selecting the 'Action and Return' in the column of test aim, the tester can test the data of relay action and return, and it can also calculate the return coefficient automatically.

■ Modes of Manual Operation, Semi-automatic and Full-automatic Operation

● Mode of Manual Operation

All variables are controlled by hand. Press the  key or  key on the tool bar, or press the "↓" key or "↑" key on the keyboard on front panel, each variable will increase or decrease one step. When relay acts, the tester will give a sound of 'Di' and record the action value and time. If needing to test the return value of the relay, decreasing or increasing the variable till the relay's contact return, the sound of 'Di' will disappear. The tester will record all necessary return data and calculate the return coefficient automatically.

- **Mode of Semi-automatic Operation**

In this mode, all variable will increase or decrease automatically after starting the test when selecting 'Increase' or 'Decrease'. You can set the interval of increase or decrease. When the relay acts, the tester will record action value of selected variables automatically and maintain output but the variety will be stopped temporarily. Meanwhile, a dialog box will be ejected for asking the change direction of next step, will you 'increase', 'reduce' or directly 'stop' the test? You should select an order according to the requirement of test.

- **Mode of Full-automatic Operation**

In this mode, all variables will increase or decrease according to step size after starting the test when you select 'Increase' or 'Decrease'. You can set the interval of increase and decrease when protection acts; it will record necessary data automatically. If the 'only contact operation' has been selected, the tester will stop the test after obtaining the action data automatically; if the 'test action value and return value' has been selected, the tester will automatically change direction after obtaining the action value and alter the value in the opposite direction till the contact of tester returns so as to measure the return value, record it and calculate the return coefficient.

Attention:

1. In the mode of 'manual Operation', the speeds of increase and decrease variable can not be very quickly when it almost achieve the value of protective operation, so as to ensure the variable stays for enough times at every step size for producing the action. Only doing like this, the result measured will be more accurate.

2. During the automatic test, the internal calculator will be reset to zero with each step process. When measuring the action time of relay, please select the mode of 'manual Operation' and make it to vary slowly if longer time is needed.

■ Directly Set Parameter to Alter Output Value in the Output State

During the test, the software permits to use many functions to directly change output in the state of output:

- You can switch the mode of 'Manual Operation', 'Self-automation' and 'Full-automation' in the output state, switch between 'Increase' or 'Decrease', or switch between 'Contact Action' or 'Action and Return'. You can change the 'Time interval of automatic variety' in the mode of manual operation.

- Whenever parameters need to be amended, it can be changed among all kinds of

modes. Click corresponding 'Alteration' box to tick '√' or cancel to complete this operation.

- In the mode of 'Manual Operation', you can change output of each phase at one time. The concrete operating procedure is as following: directly input the amplitude and phase of each phase needing to be amended one by one (please do not press the 'confirmation' key before completing it). After finishing inputting all values, please press the 'Confirmation' key. Then, the tester will synchronously change output of each phase to be the corresponding input value .

- **■ Input**

All input of 'Relaytestar' Series Tester share one common terminal. When connecting the protective action contact, connect one end with the common terminal of tester and connect another end with any one of input A、 B、 C、 R、 a、 b、 c. Please note that if the connector has the positive potential,do connect this connector with common terminal.

In this testing module, input A、 B、 C、 R、 a、 b、 c are effective in default state. The relationship between them is 'or'. When certain digital input is not needed, you can select to close it. When doing the test, switch-off and switch-on contacts of relay can be connected with any digital input (during the line protection, the software defaults the digital input R to be the signal incoming end of reclosing. When connecting the input common terminal (red terminal) with active contact, we normally connect it with the positive end of power supply. The tester will record the time in the column of input as soon as the tester receives the trigger signal of the digital input.

If the trigger signal occurs in multichannels digital input ,the corresponding data wii be recorded.

■ Confirme the Switch State Change Time

Off/on of contacts of all kinds of relay and microcomputer protection normally has certain oscillation. To prevent the oscillation from influencing the test result, we usually set certain 'Confirme the Switch State Change Time'. For common relay, 'Confirme the Switch State Change Time' is set to be 20ms,as for the microcomputer type protection, 'Confirme the Switch State Change Time' only needs to be set to be 5ms.

Record Test Result

There is an area for recording the 'action value', 'return value' and 'return coefficient' of test result on the lower right of the interface. It can record three-phase voltage, current, line voltage, voltage, positive sequence, negative sequence and zero sequence component of current, phase and frequency of AC, etc. You only need to tick the box before any item. Just as

	Para.	Action	Return	Ret. Coef.
<input type="checkbox"/>	UA			
<input type="checkbox"/>	UB			
<input type="checkbox"/>	UC			
<input type="checkbox"/>	IA			
<input type="checkbox"/>	IB			
<input type="checkbox"/>	IC			

the right diagram shows

Short Circuit Calculation Button

'AC Test' module is a popular module. When more complex test needs to be simulated, please click the Short Calculation button in the tool column. A dialog box of 'Short Calculation' will be ejected, in which you can set arbitrarily.

- **Type of Fault**

Four types of fault are available in the pulldown menu: single phase earthing short circuit, two phase short circuit, three-phase short circuit or normal state, among which the normal state means that the three phase voltage is positive sequence rated voltage and three-phase current is 0A.

- **Fault Direction**

It is 'Forward Direction Fault' in the default mode. When reverse fault needs to be simulated for some directivity protection, you can select the 'Reverse Fault' in pulldown menu.

- **Rated Voltage**

It represents the rated phase voltage of the system. The rated voltage usually is 57.735V.,which refers to the Non-fault phase voltage.

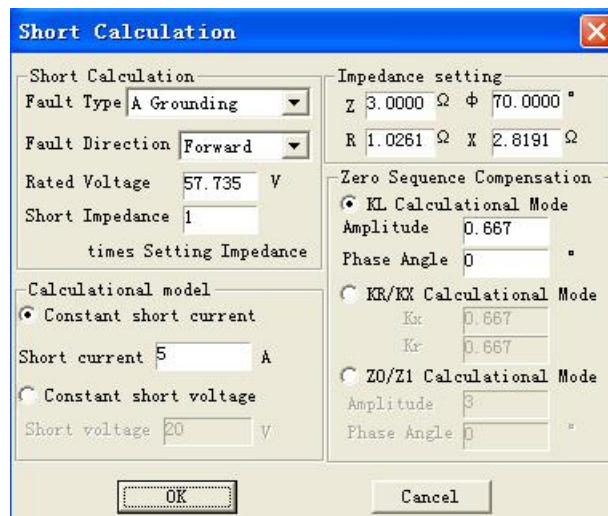
- **Setting Impedance**

According to different setting valued given by the setting value list, you can set fault impedance according to 'Z / Φ' or 'R / X' two kinds of modes on the interface. Selecting which kind of mode to set setting impedance depends on the setting value list. Whatever you choose,the value of another kind of mode will be obtained through automatic calculation of the computer..

- **Multiple of Short Circuit Impedance**

Above we set the 'Setting Impedance' in the setting value list, but we often verify it in 0.95 times or 1.05 times when doing the test. So 'Short Circuit Impedance' = 'Times Value' × 'Setting Impedance',involving 'Short Circuit Impedance' with short circuit calculation again. When doing the 'Zero Sequence Protection' test, the preemptive action of distance protection can be standed aside through flexible setting of short circuit impedance and in the case of not exiting the distance protection.

- **Model for Calculation**



When selecting the 'Maintaining Short Circuit Current', certain short circuit current needs to be set. You can calculate the 'Short Circuit Voltage' of corresponding fault type by using the 'Short Circuit Impedance' and this 'Short Circuit Current' given. When selecting 'Maintaining Short Circuit Voltage', certain short circuit voltage needs to be set. You can calculate the 'Short Circuit Current' of corresponding fault type by using the 'Short Circuit Impedance' and this 'Short Circuit Voltage'. When doing the 'Distance Protection' Test, flexible setting the short circuit impedance may avoid the priority-action of the 'Distance Protection' under the condition of not exiting the zero sequence protection.

Attention:

'Short Circuit Voltage' represents the fault line voltage when two phases is short circuit, while it refers to the fault phase voltage in the event of other types of short circuits.

- **Zero Sequence Compensating Factor**

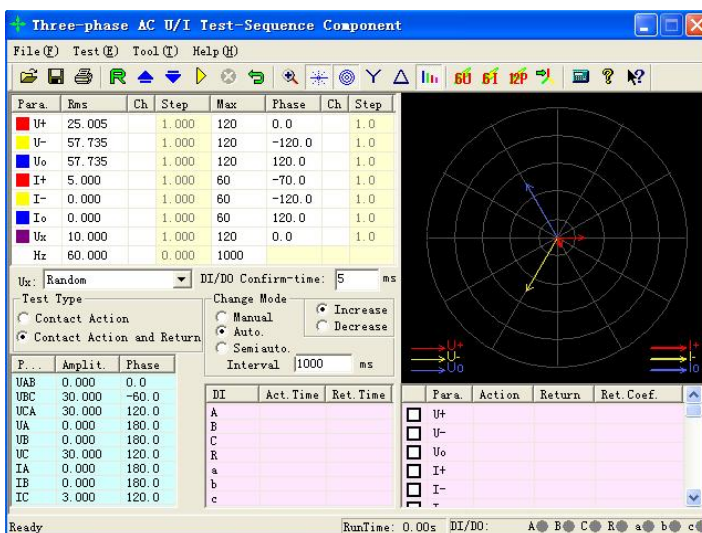
When simulating the 'Earthing Distance Protection' Test, the corresponding zero sequence compensating factor must be considered. Software gives three setting modes, please set according to the setting mode of zero sequence compensating factor given in the setting value list.

After finishing the above testing parameters setting, please click the 'confirmation' button, then the software will calculate the short circuit voltage, current and corresponding angles and fill these data on the 'AC Test' interface at once.

Function of outputting according to sequence component

The following diagram shows the testing interface of sequence component:

Set directly all kinds of sequence component of voltage-current needed to be output on the interface. For example, when needing to output three phase negative sequence voltage, fill the blank after 'U - ' with this value and software can calculate automatically the amplitude and phase relations of output voltage of each phase.



Attention:

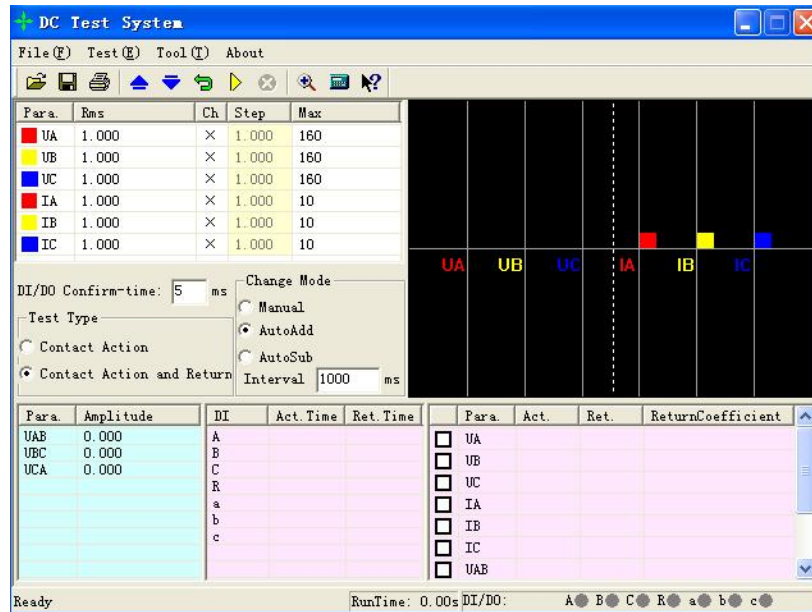
1. You should note that the amplitude, variation step size and phase are all sequence components, which are combined by three-phase voltage or three-phase current but not

actual output of single phase of tester. If changing any sequence component value on the interface (including amplitude and phase) ,software will real-time calculate corresponding three-phase voltage and current ,which will be displayed in the listing area on the lower left side of interface. The tester output voltage and current displayed on the interface rather than sequence component.

2. U_0 、 I_0 、 U_- 、 I_- on the interface are value of each sequence component, equaling to one third value of $3U_0$ 、 $3I_0$ 、 $3U_-$ 、 $3I_-$ in general use, which is the same as the value displayed in the result list on the lower left corner of three-phase AC Test interface. When doing the test, firstly identify which one is the setting values given by protection, U_0 、 I_0 、 U_- 、 I_- or $3U_0$ 、 $3I_0$ 、 $3U_-$ 、 $3I_-$. If being U_0 、 I_0 、 U_- 、 I_- , you can set parameter directly according to the setting value; if being $3U_0$ 、 $3I_0$ 、 U_- 、 I_- , the actual setting value should divide by 3, and then set parameters according to new setting value.

Chapter 6 DC Test

DC test module provides special DC voltage and current output ,mainly satisfying the requirements of doing tests including DC voltage relay, time relay and auxiliary relay. Main interface of DC module is as the following figure shows:



Section 1 Interface Instruction

Interfaces of 'DC Test' module and 'AC Test' module are very similar, and their operating manner are basically the same. Using DC test, please refer to the 'AC Test'. Here we only illustrate their difference as follows:

Parameter Setting

The largest output voltage of each phase is $\pm 160V$. When higher voltage needs to be output, you can adopt two-phase voltage output. One numerical value is positive, and another is negative, then the highest output voltage can achieve 320V. For example, if $UA=100V$, $UB=-100V$, then $UAB=100 - (-100) = 200V$. The amplitude of line voltage is displayed on the lower left corner of main interface. Values of UA and UB are not always equal to each other and the positive and negative polarity should be paid attention to.

The largest current output of single phase is 10A. If higher current is needed to be output, you can use the mode of paralleling two-channels or three-channels current. The amplitude of each phase should be equal basically.

Attention:

When doing the time test of the relay, the 'Manual Operation' testing mode should be selected due to normal action time is longer. It need not change after loading rated voltage on relay, and just waiting for its action. When connecting wires, the time-delay contact of relay should be connected with the digital input of tester.

■ Independent DC output

There is one channels independent heavy power DC output power supply on the back panel of tester. When doing test on the spot, we adopt DC power supply to provide one channels DC power supply for relay. This power supply provides 110V or 220V two shifts for outputting, and also have OFF shift closing the output. This DC power supply outputs is through rectifying and filtering of transformer winding, so it has not the function of voltage stabilization and can't ensure high precision.

If the display of relay can't work well, please measure the working voltage of DC output by the multimeter firstly and check whether the voltage is normal and protector tube works well.

Attention:

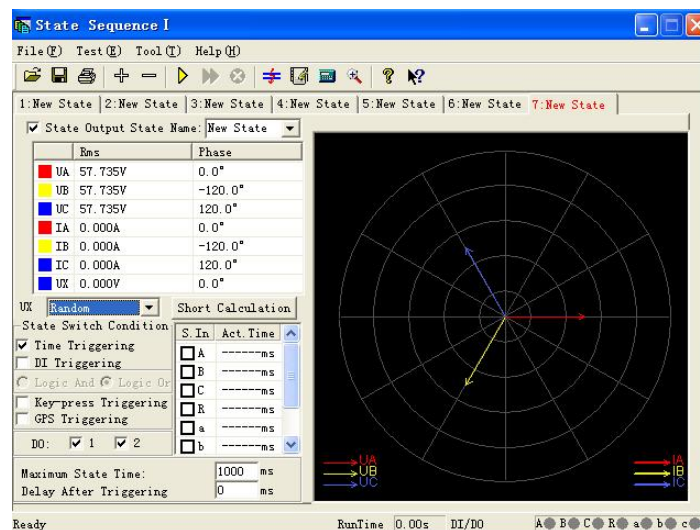
The output can produce as soon as the tester is provided with DC power supply, so please pay attention on safety in utilizing the tester!

Chapter 7 State Series I & II

State Series Module are divided into 'State Series I' and 'State Series II', The 'State Series I' outputs 4 phase voltage and 3-phase current, which can be applied for the series of 'Relaytestar-1000'. 'State Series II' outputs 6-phase voltage and 6-phase current, which can only be applied for 'Relaytestar-1000'. The software functions and operating modes of two modules are basically the same. So we only introduce 'State Series I'.

The state series is mainly for satisfying demands of some special protective tests in power system. For example, for doing the tests of quick switching of power supply for station and automatic switch test of standby power supply ,many times reclosing of protective tester of distribution system. During the state series tests, you can add up to nine states at most. In every state, you can define the voltage-current data and simulate state variety of complex electric network freely according to actual operation. Through reversal on seven pairs input, you can obtain and measure the action value and time of relay. Main interface of State Series I is as the figure shows:

- Flexible control nine state output at most. 4-phase voltage, 3-phase current or 12-phase voltage-current can be output in every state.
- Every state can be closed, increased, cancelled, inserted, named ,and set many kinds of trigger mode.
- Ux can set many kinds of output combination modes
 - It can simulate all kinds of complex fault conveniently and flexible ,for testing complex logical combination.



Section 1 Interface Instruction

■ Increase or Delete State

Press the “+”、“-”button for increasing or deleting current state. Nine states can be added at most. If adding new state,it will be added to default current state,the user can also add new state to suitable place in the dialog box ejected.



When you need to delete the state, please select this state by mouse (when certain state is in the current state, its title will be displayed in red characters), then press “-” button.

■ Option for ‘State output’

According to actual demand, you can jump over certain state through deleting the ‘√’ before this option. At that time, this state will be displayed in gray, and it won’t be included in the whole testing process.

■ Name of State

Since this testing module is always used for doing the ‘Reclosing and Post Acceleration’ test, the software has defined the names of five state defaulted :‘Before the Fault’, ‘Fault’, ‘After the Trip’, ‘Reclosing’ and ‘Permanent Trip’ in the pulldown menu of state for user’s selection. Users can also input the self-defining name of state directly in the blank according to requirement. The self-defining name of state won’t be setting in this pulldown menu, which can be changed at any time. The self-defining name of state involving in the test still exists when reopening this testing module.

■ State Parameters Setting

The AC parameters in every state can all be set freely, and the mode is the same as the ‘AC Test’. When simulating complex test, you can obtain it automatically through opening the function of ‘Short Circuit Calculation’ on the interface. The results can also be amended.

■ Ux Option for Every State


Ux is a special component, for which you can set several kinds of output forms:

Assuming the parameters are $+3U_0$ 、 $-3U_0$ 、 $+\sqrt{3} \times 3U_0$ 、 $-\sqrt{3} \times 3U_0$, firstly combining current output U_A 、 U_B with U_C to obtain $3U_0$, then multiplying by corresponding coefficient to arrive at U_x .

If selecting to be equal to the voltage value of certain phase, then U_x output will be changed with the voltage change of this phase and always follow the change..

If selecting 'Any Mode', you can input any number in the range of 0~120 in the parameters column for U_x , and its value is equal to the voltage value and keep constant.

■ Short Circuit Calculation

Click 'Short Circuit calculation' or press the  button, then a 'Short Circuit Calculation' dialog box will be opened, which is used for simulating the short circuit calculations when all kinds of faults happen, and it will fill the calculated result in current state. You need to pay special attention to set correctly zero sequence compensating factor when it is earthing fault.

■ Conditions of State Reversing

Only the 'Time Trigger' and 'Input Trigger' can be selected synchronously, other states must be selected separately. They are preconditions of reversing from a state to next state.

- **Time Trigger:**

When this triggering mode is selected, you can input respectively certain values in the 'Longest State Time' and 'Time Delay after Triggering'. During the test, it will enter next state after the abovementioned time delay. 'Longest State Time' stands for the longest output time in this state. Function of 'Time Delay after Triggering' is similar to confirmation time of switch triggering in AC test module, which is used for avoiding the error due to protective oscillation and usually it is set around 10ms. Please pay special attention that time delay can't be set when simulating the faults of reclosing or post acceleration. Because the post acceleration fault causes by reclosing fault state, the post acceleration protection will act correctly only when it enters the Permanent Trip state e. If it output fault component during the period of 'Longest State Time', and also the 'Input Trigger' is selected to be the reversal condition of this state synchronously before the test, the tester will jump over the state of 'Longest State Time' left and get in the state of 'Time Delay after Trigger' when the tester receives the action signal of protection.


In addition, it often avoids the oscillation of protective contacts through setting 'Time Delay after Trigger'.

- **Digital Trigger:**

When this triggering mode is selected, seven channels input A、 B、 C、 R、 a、 b、 c will all be effective. Relationship of these seven channels input is 'or', and you can cancel redundant input through deleting the '√' in front of it as required. When the tester tests action of the input selected, it will reverse to next state through the 'Time Delay after Trigger'.

In order to avoid 'Oscillation' of contacts influencing the test, you should normally set certain 'Time Delay after Trigger' in this triggering way.

- **Key Trigger:**

When the 'Key Trigger' is selected, during the test, click the  button or press the 'Tab' key on tester's front panel to realize the state trigger reversal . This is a kind of effective mode for controlling the test process by hand.

- **GPS Trigger:**

When GPS trigger is selected, you can use minute impulse or second impulse of GPS clock to test several testers synchronously.

Attention:

1. The Time Trigger and Input Trigger could both be ticked at the same time, then the one whose condition arrives in advance will trigger the reversal.

2. When the Switch Trigger is selected, normally certain 'Time Delay after Trigger' (about 5—20ms) needs to be set for avoiding reversal due to many times error trigger led by contact oscillation.

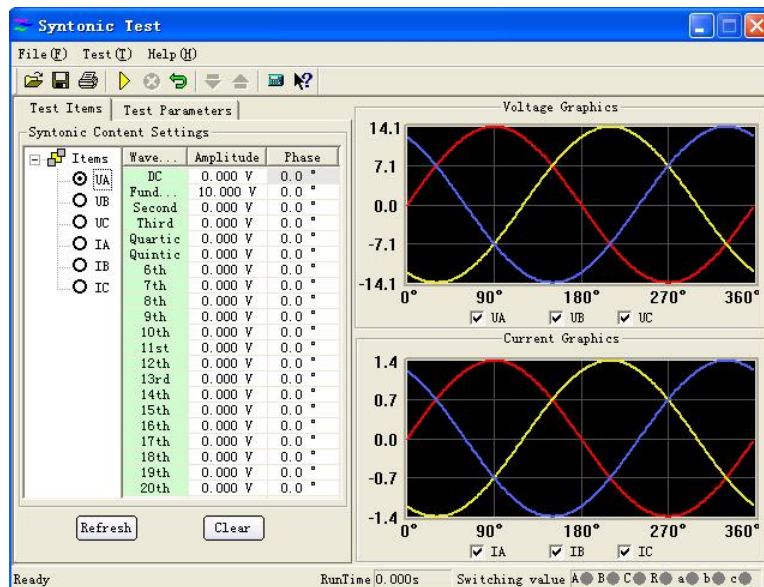
■ State of Digital Output

You can set the output state of digital output 1 or digital output 2 in each state. If you tick it as '√', so the output of this channel will be closed in this state; otherwise it will be opened. You can set different output of digital output in each state, which can implement switching variety of output during reversal in all state

Chapter 8 Harmonic Superposition Test

The 'Harmonic Superposition' Test unit can implement superposition output of each order harmonic component of 3 phase voltage and current, which is used for testing the working behavior of equipment of power system in all kinds of harmonic conditions. It is often used for verifying constraint coefficient of differential harmonic.

- UA、UB、UC、IA、IB、IC can be overlapped DC and 2~20 order harmonic output.
- Each component can be displayed and recorded according to amplitude, and it also can be displayed and recorded according to percentage of fundamental wave
- You can select automatic variety or manual variety, and the amplitude and phase will all be changed.
- It can measure action value, return value, action time and return time.



Section 1 Interface Introduction

■ Set Harmonic Data

There are two kinds of displaying modes for harmonic in this module, one is the mode of amplitude and another is percentage of fundamental wave, meanwhile, the amplitude of harmonic has

This table is a close-up of the 'Syntonic Content Settings' table from the software interface. It shows the configuration for various harmonic components across three phases (UA, UB, UC, IA, IB, IC). The 'Fund...' row is highlighted in green.

Items	Wave...	Amplitude	Phase
UA	DC	0.000 V	0.0 °
UB	Fund...	10.000 V	0.0 °
UC	Second	0.000 V	0.0 °
IA	Third	0.000 V	0.0 °
IB	Quartic	0.000 V	0.0 °
IC	Quintic	0.000 V	0.0 °
	6th	0.000 V	0.0 °
	7th	0.000 V	0.0 °
	8th	0.000 V	0.0 °
	9th	0.000 V	0.0 °

direct relation with the amplitude of fundamental wave. In addition, the waveform output after superposition also has relation with the amplitude of this fundamental wave. Generally speaking, when doing the harmonic suppression test, the amplitude of fundamental wave should be set larger than the action setting value of relay (such as the starting value of differential protection) in order to ensure the protection can be acted reliably when the harmonic is smaller or is 0.

Set amplitude and phase of harmonic in this page. Data phase of the state selected on the left of diagram stands for the channel of corresponding phase that will superpose harmonic. The amplitude valued can be expressed in two modes. The mode of amplitude value is adopted in this diagram, so its unit is the one of corresponding current-voltage. If you would like to express it in percentage of fundamental wave, then it will display the percentage it accounts for the fundamental wave. Here the phases of fundamental wave and harmonic have little influence on test results, so usually using the default set is OK. In case of any set is needed, please set the phase between the fundamental wave and harmonic according to the setting value of protection.



Data Revert Button: Please set test data before the test. Amplitude and phase during the test may vary. Please just press this key after completing the test to make data 'revert' to the state before the test.



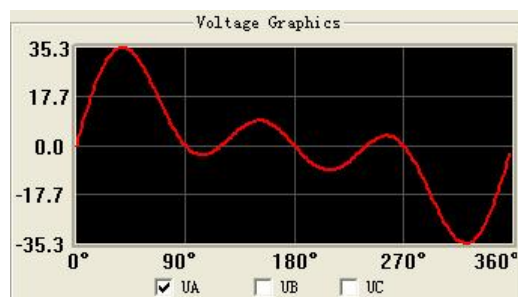
Refresh Button: This button is invalid to parameters participated in previous test, but only be valid to new data amended before doing next test. It can 'refresh' new data amended to be the state before the amendment.



Clear Button : It clears the amplitude values of all waveforms including fundamental wave, DC and 2~20 order harmonic displayed in current window, and the phase will return to its default state, i.e, the phase A returns to '0', the phase B returns to '-120°', the phase C returns to '120°'. This key is only valid to the parameters displayed on current interface.

Here displays the waveform after superposition.

You can select to display all three phases, and also select to display the waveform of single phase. The graph shows the waveform of Phase A voltage after harmonic is superposed. This graph can be compared with the waveform of oscillograph conveniently.



DC output range of each phase voltage is -160~160V, and the output range of fundamental wave and harmonic is 0~120V; DC output range of each phase current is -10~10A, and the output range of fundamental wave and harmonic is 0~40A.

Summation of waveform effective value superposed in the same channel can't be over 120V (40A). If it is over the range, software will give a hint. At that time, please check the total amplitude. The amplitude superposition test should all be checked when inputting data and outputting variety.

■ Testing Parameters

- **Variable Option**

Variable: Select the channel needed to change from the pulldown menu. In this diagram, A Phase voltage is selected to be variable.

Waveform: represent harmonic change from DC to 20th order harmonic.

Step Size of Amplitude Value: The step size here is also corresponding with 'Harmonic Expressing Mode'. When 'Express in amplitude value' is selected, the step size can also be expressed by amplitude, and the unit is A or V; however, when selecting the 'Express in percentage of fundamental wave', step size is also the percentage.

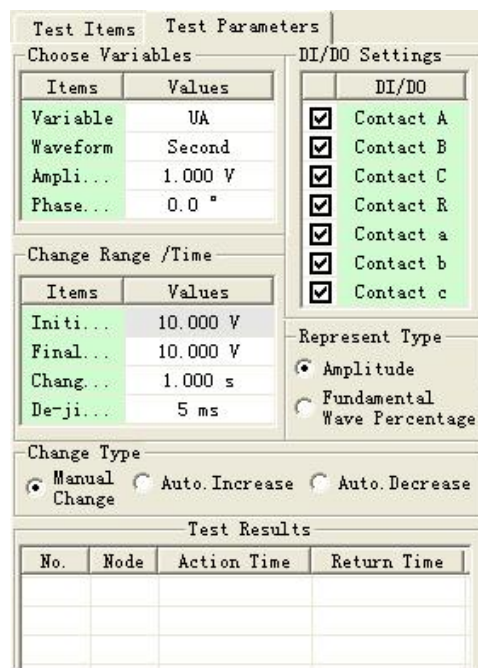
- **Range and Time of Variation**

Initial Value of Variation : The initial data of variation come from the data of foregoing harmonic set, which could not be amended. If the initial value needs to be amended, you must do it on the page of harmonic data. The initial value here is expressed in the way of amplitude.

Upper Limit of Variety: It is the output upper limit value of variable, which can ensure the output value not to be very large and avoid ruining the tester.

Variation Time: Variation time stands for the interval of each step variation, and it is normally set to be slightly larger than the setting action time of protection.

Anti-Oscillating of Contacts : The default value is 5ms. When doing the relay test, you



should set longer Anti-Oscillating time according to requirement.

- **Expressing Method of Harmonic**

You can select 'Express in the mode of amplitude', and also can select 'Express in percentage of fundamental wave' to express data of harmonic component of each phase. When 'Express in percentage of fundamental wave' is selected, the data of each order harmonic on the page of 'harmonic' will be displayed the percentage related to the amplitude of fundamental wave. The step size of amplitude of variable will also be expressed in the percentage of fundamental wave. For example, when the 'Express in amplitude value' is selected, amplitude of the second order harmonic of certain phase voltage is 2V and the amplitude of fundamental wave is 10V, then the second order harmonic displayed is 20% when selecting 'Express in percentage of fundamental wave'.

- **Set Digital Quantity**

The page of digital quantity is used for defining the action of which channel is effective. It defaults that digital quantity of all seven channels A、B、C、R、a、b、c are effective. When doing the test, you can define the digital quantity of which channel is effective (tick '√' means effective). Relation of each is 'or'.

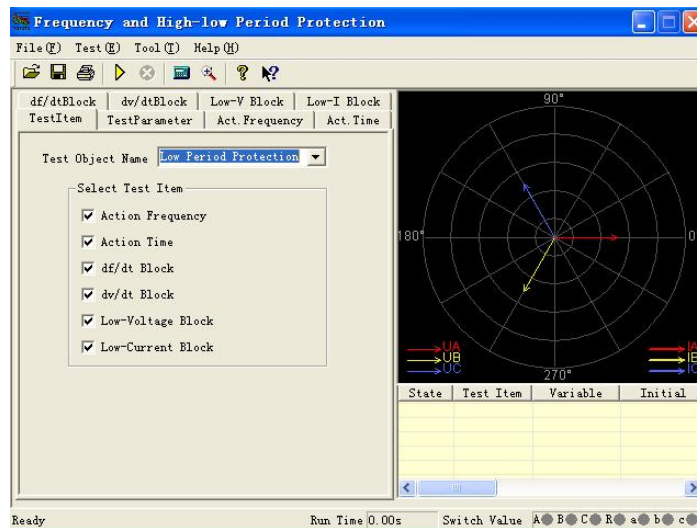
- **Way of Variation**

Here Manual Operation and Automation (automatically increase and decrease) two kinds of variation are available for implementing change to harmonic components of each phase during the test.

Chapter 9 High-Low Frequency Test

The 'High-Low Frequency Test' module is mainly used for testing all functions of frequency protection including low frequency load-reduction and high frequency generator_shutting. According to its functions, this module is divided into six test units.

- All test items includes almost all frequency and high-low circle protection
- The frequency can slip down to do low- frequency load-reduction test, and can also slip up to do high-frequency test

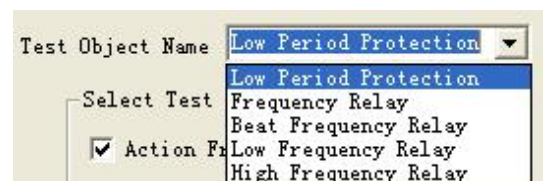


Section 1 Interface Explanation

■ Test items

There are six test items available, they are 'Action Frequency', 'Action time', 'df/dt block', 'dv/dt block', 'Low Voltage block' and 'Low Current block'. According to request, one or more items can be selected. When more than one are selected, corresponding dialog box will be ejected after completing a test item to tell you next test item.

testing objects includes 'Low Cycle Protection', 'Frequency Relay', 'Beat Frequency Relay', 'Low Frequency Relay' and 'High Frequency Relay' five kinds



of relays. The 'Low Circle Protection' will be selected under the default situation. Its pulldown menu is as the diagram shows:

■ Testing Parameters

- **Time Delay before Variety of Frequency**

During each changing process of variable, the device will firstly output the rated power 50Hz, which will be maintained to the end of 'Time Delay before Variety of Frequency', then it begins to vary. For testing some protection this is very useful, which can be used for releasing block after the frequency protection is blocked.

- **Test Interval**

After completing one test the device will stop output till the end of 'Test Interval', and then it outputs to do next test.

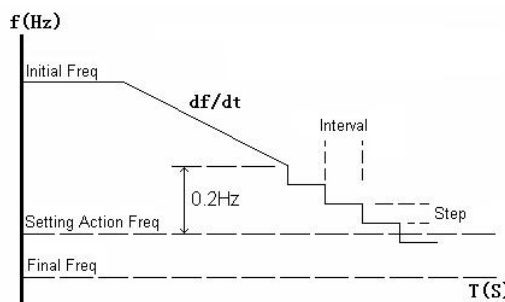
- **Setting Value**

There is inputting box of setting value in every page of test function. Most of these setting values do not work during the test, which only has a function of reference and contrast after the test. You can set the 'Error Allowance' if need. After contrasting the 'Test Value' got from test with the 'Setting Value', a relative error will be obtained for reflecting performance of protection.

■ Action Frequency

- **Frequency Test Range**

During the test, frequency varies from original value to final value in the test range, the original and final value should be set so that the action frequency is placed between them, When Varying from original value to final value frequency should stride over the setting action value so that the protection can act.



Test mode of action frequency: Frequency will vary in two stages during the test: At the beginning, it output the origin frequency. After delaying the time before the variety, it will firstly slip down (or up) evenly according to df/dt to the frequency 0.2Hz higher (or lower) than setting action value. Then, it will descend (or rise) the frequency step by step in certain time interval according to setting step size. If the protection acts during this process, the action value will be obtained. Otherwise, it will consider that the protection won't act and end this test item when frequency varies to the final value.

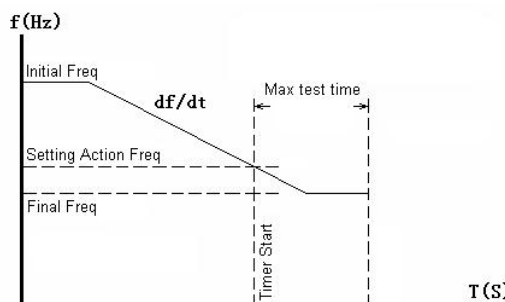
The time interval of step-by-step frequency varying is confirmed automatically according to setting action time, and this time interval is 0.2s longer than setting action time. So the setting action time must be set correctly in order to ensure that the protection has enough time to act in

the time interval of variety. Similarly, the setting action frequency also must set correctly in order that the protection can act in the stage frequency varying step-by-step.

For example: known low frequency action value is 48.5 Hz, the test range should be set 50 — 48Hz, and the step size is 0.05Hz, the testing final value should not be set too lower (normally higher than 45Hz), otherwise, the protection maybe will block.

■ Action time

Test mode of action time: frequency slips down, (or up) from original value (normally 50Hz) to final value and waiting for action. This final value should be lower than frequency action value for ensuring action of protection. But the timer for testing action time begins to time it from 'Setting Action Frequency'



So if the setting value has deviation, it will influence the time measuring precision. For process of test, please see the right diagram.

■ df/dt Block

- **df/dt Test Range**

When testing the 'df/dt block value', it will do tentative test point by point in the test range. The frequency will slip down (or up) from original value to final value every time. The df/dt value slipping down (or up) will vary point by point in this range. When the protection acts in certain time test, the boundary value of df/dt block at that time will be tested out.

Since the protection is blocked when the df/dt value is larger than setting value, the original value of df/d should be higher and the final value should be lower than the setting block value of protection, which means during the test from protection no action to action, the dv/dt block value will be tested out.

- **Range of Frequency Variety**

In each period, testing frequency slips down (or up) from original value to final value. The original value is normally 50 Hz, and the final value is lower (or higher) than setting action frequency.

Attention:

Time delay before frequency variety when doing this test could not be too shorter in order that there are enough times for protection to release block.

■ dv/dt Block

This testing item is very similar to 'df/dt block' mentioned in the above paragraph. Their

difference is that the variable in each test period is dv/dt value. We only introduce their differences in the following paragraph.

- **dv/dt Test Range**

It will do tentative test point by point in this range when testing 'dv/dt block value'. Voltage will slip down from original value to final value when doing the test every time. The dv/dt value slipping down will be varied point by point in test range. When the protection acts in certain period of tentative test, the boundary value of dv/dt block will be tested out.

Since the device is in the block state when the dv/dt is higher than the setting block value, normally the original value should be set higher than the setting block value, and the final value should be set lower than the block value. Which means during the test from protection no action to action, the dv/dt block value will be tested out.

- **Varying Range of Voltage**

For simulating the process of voltage's descension, normally the 'Original Value of Variety' of voltage should be set higher than the 'Final Value of Variety'. Meanwhile, for avoiding the low frequency protection from being blocked due to low voltage, the 'Final Value of Variety' of voltage set should be higher than the setting low-voltage block value of the protection.

- **df/dt value in testing**

Frequency in this testing item always varies along according to given df/dt , so df/dt should be set lower than the setting df/dt block value of the protection.

■ Low Voltage Block

This item is similar to ' df/dt block' and ' dv/dt block' in above paragraph. We introduce their difference as follows:

- **Test Range of Voltage**

Voltage will do tentative testing point by point in test range. In every period of test frequency will vary but voltage will be fixed to certain value. Voltage increases from the original value to final value step-by-step. When it is increased to certain value, the device release block to act, so this value is the boundary value of low voltage block.

Since the protection is blocked when voltage is lower than the block value, normally the original value of voltage should be lower and the final value be higher than the block value. Which means during the test from protection no action to action the dv/dt block value will be tested out.

■ Low Current Locking

This testing page is very similar to 'Low Voltage Block'. Please refer to the instruction for ' df/dt block', ' dv/dt block' and 'low voltage block'.

Segment 2 Guidance for Test

We only take the 'Test of Low Frequency Action Value' as example, to explain the test method in details.

■ Connecting Mode

Connecting three phase voltage UA, UB and UC of tester with three phase voltage of relay; connecting UN of tester with UN of relay; connecting digital input A and B of tester respectively with the trip terminal of primary and secondary stage load-reduction of relay, and connecting common end of digital input of tester with the trip common terminal of relay, then turn on the power supply of relay. (If the relay needs DC power supply, the power can be lead out from the Aux DC power supply on the rear panel of tester.)

■ Option

In the "Frequency and High-Low Circle Protection" testing module, select the 'Action Frequency' test item and testing object of 'Low Circle Protection';

■ Set

Switch to 'Action Frequency' test interface to set testing data, like the right diagram shows:

- **Setting Action Frequency**

Set this item according to the settings list of relay or actual action valued by protection. This setting item is only for reference during the test and do not influence test result.

- **Setting Action time**

Set this item according to the settings list of relay. The interval of frequency varying step by step in the second stage is 0.2s longer than this value. If

it is too short, the relay may has not enough time to act, so this value should be set correctly.

- **Test Range of Action Frequency**

'Initial Frequency' must be higher than the action frequency set by protection, and 'Final Frequency' must be lower than it, that means action frequency should be placed between them.

- **Step Size of Variety of Frequency**

'Variety Step Size' should be set according to the precision required by the test, normally it can be set in 0.05Hz defaulted.

- **df/dt Value When doing the Test**

It stands for the speed of evenly frequency conversion in the first stage during the process of

df/dtBlock	dv/dtBlock	Low-V Block	Low-I Block		
TestItem	TestParameter	Act. Frequency	Act. Time		
Voltage	Rms V	Phase°	Current	Rms A	Phase°
UA	57.735	0.0	IA	0.000	0.0
UB	57.735	-120.0	IB	0.000	-120.0
UC	57.735	120.0	IC	0.000	120.0
Present F(Hz)					
Setting Value			Action Frequency Test Range		
Action F	59.000	Hz	Initial	60.000	Hz
Action Time	0.500	s	Final	58.000	Hz
Tolerance	± 5.0	%	F Change Step	0.050	Hz
			Testing df/dt	0.500	Hz/s
Warning: 1. Please set up Action Frequency and Action Time properly. 2. df/dt Value During Testing should be smaller than df/dt Block Value.					

descending frequency, and df/dt value should be lower than the locking value set by protection.

■ Button for Starting the Test

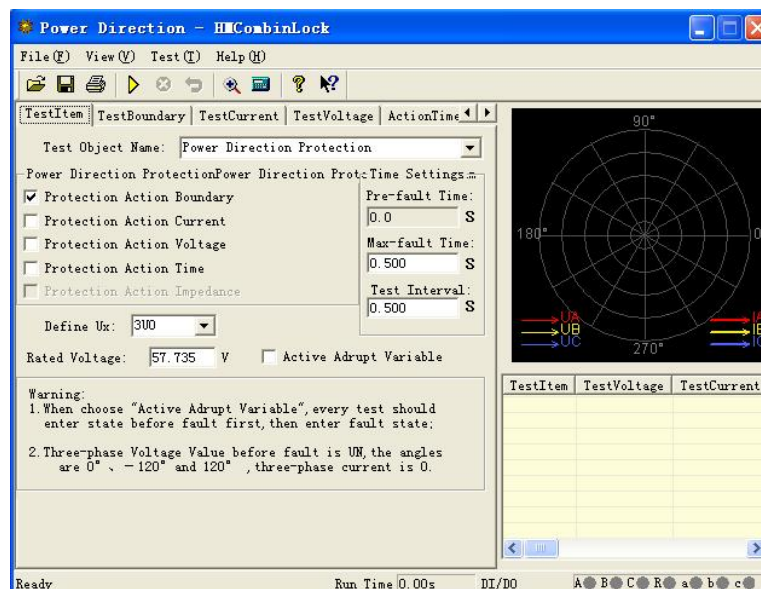
After confirming all testing parameters are correct, the test can be started. During the test, current real-time frequency output by tester can be observed through the column of 'Current Frequency Hz'. When the tester does not output voltage, the 'Abnormity' lamp on protection will light up. When output frequency of tester is lower than the 'Start-up Value', the 'start-up' lamp on protection will light up, that is to start up low circle action components.

Process of test is as follows: output 50Hz voltage-current, after delaying time before variety—— frequency slips down evenly in the speed of df/dt to 'Original Value of Test' —— press 'Step Size of Variety' to reduce frequency in the time interval of 'Setting action time + 0.2 seconds' step by step, and also record whether the protection acts.

Chapter 10 Power Direction & Impedance Test

The Power direction and impedance test module is mainly used for testing the protections related to 'direction', such as power direction protection, negative sequence power direction, zero sequence power direction, phase-phase power direction, reverse power direction, phase-phase impedance, grounding impedance, etc. It tests their action boundary, the sensitive angle, and action value of voltage and current, action time and action impedance. We only take 'Power Direction Protection' as example to introduce all testing item of this module. Its main interface shows as the following diagram:

- It includes not only all kinds of test items for power direction protection, but also the test of phase-phase and grounding impedance protection.
- Software introduces the option of 'Enable Abrupt Variable' for satisfying the testing requirements of some protections which need abrupt variable to start protection
- Adopting two vectorgraph display modes to make the test process more conveniently to observe visually.
- In boundary test, the two action boundaries line can be drawn automatically and the sensitive angle can be computed and drawn on the graph automatically.



Section 1 Interface Instruction

■ Test item

- **Name of Testing Object**

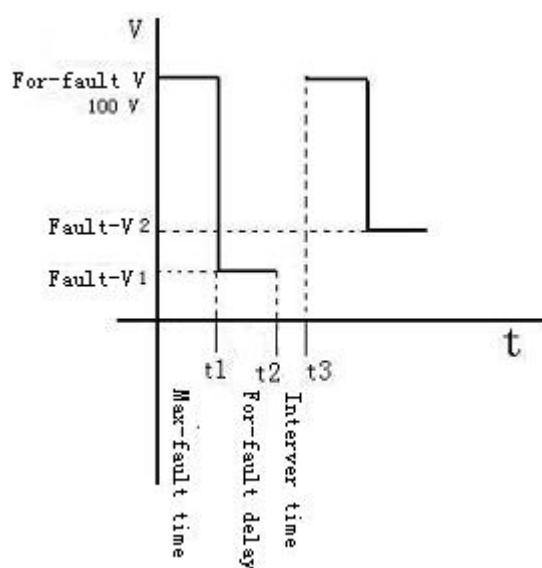
There are many types of protection device available, it includes ‘power direction protection’, ‘negative sequence power protection’, ‘negative sequence power direction’, ‘zero sequence power’, ‘zero sequence power direction’, ‘phase-phase power direction’, ‘reverse power protection’, ‘phase-phase impedance’ and ‘grounding impedance’.

- **Abrupt Variable Start up Protection**

When ‘Enable Abrupt Variable’ is selected, the tester will firstly output the voltage and current of state before fault every time during the test, then output the voltage and current set on the interface. For satisfying the demands of abrupt variable starting up protection of some protection relay, the ‘Time before Fault’ must be set at that time. If you do not select the ‘Enable Abrupt Variable’, the ‘Time before Fault will be invalid (automatically be 0). It will output directly the voltage and current set every time during the test, which will vary continuously.

Take ‘Test Voltage’ as example, the meaning of abrupt variable can be showed as the right diagram After clicking the ‘Start Test’ button, the tester will output firstly normal voltage, and maintain it till the end of ‘Time before Fault’; then, the tester will output ‘Fault Voltage 1’ (the fault voltage set on the interface), and maintain it till the end of the ‘Max Fault Time’; then, the tester will stop output for the test interval time (if the ‘Test Interval ’ is not 0).

After that, tester will output again normal voltage, and maintain it till the end of ‘Time before Fault’; then, output ‘Fault Voltage 2’ (the voltage after varying one step size), and maintaining it till ending the ‘Max Fault Time’; then, the tester will stop output for the test



TestItem	TestBoundary	TestCurrent	TestVoltage	ActionTime
Value settings				
Test Voltage:	UBC	100.000 v	Sensitive Angle:	-45.0
Test Current:	IA	5.000 A	Boundary 1:	0.0
φ (UBC, IA) Search From:	Val	-180.0	Boundary 2:	0.0
To:		90.0	Tolerance:	± 5
Step:		1.0	Test Sensitive Angle:	0
3U0	0.000 v	-0.0	Define Action Angle: φ	(UBC, IA)
U2	0.000 v	180.0	Present Action Angle:	0
3I0	5.000 A	90.5	Display Vector Diagram	<input checked="" type="radio"/> Display 3-Phase V and I <input type="radio"/> Display Action Angle
I2	1.667 A	90.5	Warning: 1. Origin and end of φ search range should be out of action area	
Other Phase Volt.:	57.735 v		2. Other phase should keep symmetry with the test	
3. The angle is angle of Voltage leading Current				

interval time. The test will progress periodically like that, every cycle the voltage always vary from normal voltage to fault voltage abruptly.

■ Test Action Boundary

It tests automatically two action boundaries of power direction protection, and calculate the sensitive angle automatically. In the mode of 'Display vectorgraph of action angle', you can observe visually two boundary lines and the sensitive angle line from the diagram on the right of main interface.

- **Testing Parameters**

Selecting one voltage and one current output, its angle $\Phi(U, I)$ varies in given range measure left and right action boundaries.

Considering that protection is normally connected in the way of 90° connection, so we normally adopt line voltage and phase current of the third phase, such as adopt voltage U_{AB} and Current I_C . Sometimes you can also select single phase voltage and single phase current to do test, but normally the line current is not selected. Please pay attention that, the selected voltage and current are set value, but the voltages of unselected phases are equal to rated voltage and symmetrical, and the currents of those phases are 0.

When setting the searching range of $\Phi(U, I)$, you should firstly know the setting value of the 'Sensitive Angle' of protection and ensure the searching range set can cover two actual action boundaries of protection. That means original value and final value of searching should all be set outside the action zone, and tester will search from the 'Non Action Zone' to 'Action Zone'.

Protection does not act when starting the search at the original angle. It acts when angle varies to certain value and one action boundary angle is found, then lined the diagram. Then, it reverse the searching direction immediately to search another boundary angle (notes: now tester will search from the final angle set to original angle). When the second action boundary is found, it will be lined again. Then the Sensitive Angle can be calculated and lined on the diagram automatically.

- **Definition of Action Angle**

Select the action angle as 'Test Phase Angle', ' (U_0, I_0) ' or ' (U_2, I_2) ' according to protection type tested. If it is power direction or impedance relay, select the 'Test Phase Angle', that is the angle between testing voltage and current selected. If it is zero or negative sequence protection, you should select (U_0, I_0) or (U_2, I_2) .

- **Vectorgraph Display**

When 'Display the vectorgraph of 3 phase voltage and current' is selected, it displays the vectorgraph of each phase voltage and current in the graph.

When 'Display the vectorgraph of action angle' is selected, only the components of voltage and current of the action angle selected are displayed in the graph. If (U₂, I₂) is selected, it will only display the value and angle between U₂ and I₂.

This display mode is convenient for observing visually the searching process of action boundary.

■ Testing Current

Mode for testing operating current is: Fix voltage and the angle between voltage and current, increase current step by step from low to high till the protection acts and test out action current value. During the test, angle $\Phi(U, I)$ should be normally set the sensitive angle of protection. shown as the right diagram.

3U0	0.000	V	-0.0
U2	0.000	V	180.0
3I0	1.000	A	-59.5
I2	0.333	A	-59.5
Other Phase V:	57.735	V	

When doing the test, select a line voltage to be fixed and the third phase current to be variable. The variety range of current should includes setting action current of protection. When voltage leading current the angle is positive. So please pay attention to the positive angle and negative angle when setting angles. Normally, when the setting angle is equal or near sensitive angle, the protection acts the most sensitively, and the action current tested also is the most exact. When the setting angle is deflected too much, the action current tested may be larger or even relay may not act.

■ Testing Voltage

Mode for testing operating voltage is: Fix current and the angle, increase voltage from low to high step by step till the protection acts and test out action voltage value. During the test, angle $\Phi(U, I)$ should be normally set to be the sensitive angle of protection.

When doing the test, selecting one phase current to be fixed and the line voltage of other two phases to be variable. Variety range of voltage should include setting action voltage of protection. The angle is equal to the sensitive angle.

■ Testing Action time

Mode for testing action time is: Directly set a voltage and a current which can make protection acts, when action occurs, record the action time.

■ Testing Impedance

Mode for testing action impedance is very similar to 'Testing Voltage' and "Testing Current" above, it also make the protection act through changing solely voltage or current. The difference is: this unit records action impedance value of protection but not operating voltage or operating current. As the following diagram shows:

The angle Φ (U, I) should certainly be in the action zone of protection, and we normally set it equal to the sensitive angle.

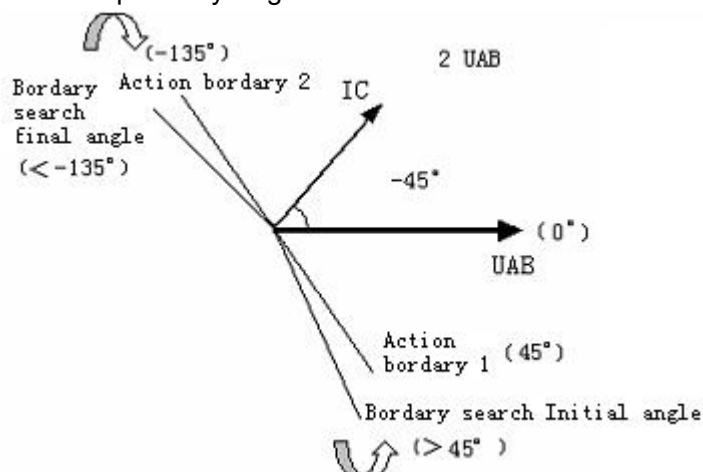
Impedance value is calculated according to voltage and current when protection acts. Please pay attention that: when testing grounding impedance, zero sequence compensating coefficient should be considered and set correctly. the default value is 0.667.

Section 2 Guidance for Test

■ Definition of Angle Made by Microcomputer Protection

Normally, the definition of angle made by microcomputer protection is: direction of voltage leading current is positive. On the contrary, it is negative. In addition, it often default the angle of voltage to be 0° , which means voltage is the reference for angle of current. Right diagram shows the active characteristics of certain power directional protection. Its largest sensitive angle is -45° . Two action boundaries are respectively $-135^\circ \leq \Phi \leq 45^\circ$, which is just opposite to the angle concept in x/y coordinate.

The shadow parts in the diagram stands for action zones of protection, which is corresponding to two action boundaries: 45° and -135° . When setting testing parameters, you should ensure two searching boundaries are respectively larger than 45° and smaller than -135° , which means they are in the non-action zone. Then it will search from non-action zone to action zone.



■ Searching Action Boundaries

When it is at the largest sensitive angle of testing protection, if you do not know its actual action boundary, you can adopt the following mode to search:

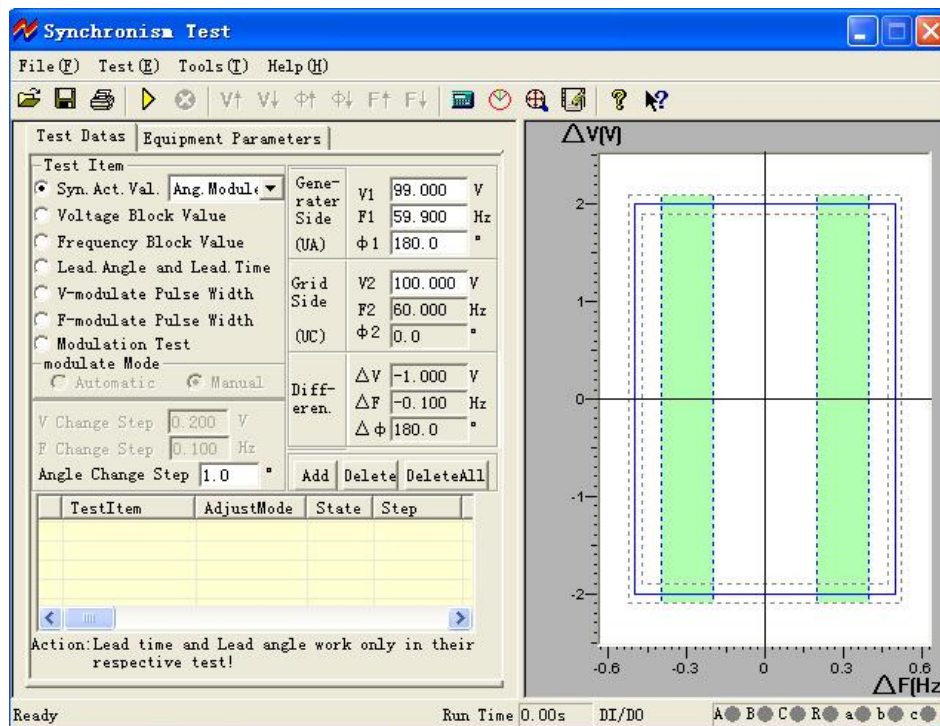
Set the 'Searching Range Collection of $\Phi(U, I)$ ' in the page of 'Testing Boundary' to be 0° , then start the test. If the protection does not act, set this parameter to be 30° . By analogy, suppose the protection does not act when $\Phi(U, I)$ is 20° , which means one action boundary of protection is between $0^\circ \sim 20^\circ$. Finding rough range of another boundary of protective action by using the same mode, supposing it is between $-130^\circ \sim -120^\circ$.

When setting searching angle on the software interface, please pay your attention to that the software always begin to increase in step size from the angle of ' $\Phi(U, I)$ Searching Range Collection'. After measuring one action boundary, it begins to reduce in step size from the angle of 'Arrival'. So supposing ' $\Phi(U, I)$ searching step size' is set to be 1° (positive value), we take the above data as example, ' $\Phi(U, I)$ searching range collection' should be set to be -130° , and the 'Arrival' should be set to be 20° .

Chapter 11 Synchronization Test

This test module is used for testing quasi-synchronization device, and it can also be used for testing some protections which detect synchronization or nonvoltage to reclose.

- It can test synchronization various action value, voltage locking value, frequency locking value, leading angle and leading time, pulse width of voltage regulation and frequency regulation.
- Can do the automatic regulating test of automatic quasi-synchronization device.
- Can test automatic quasi- synchronization device, and also can test all kinds of synchronous relays
 - Can test line protection reclose with synchronization or nonvoltage detection
- Can test automatically, and also can test by hand.



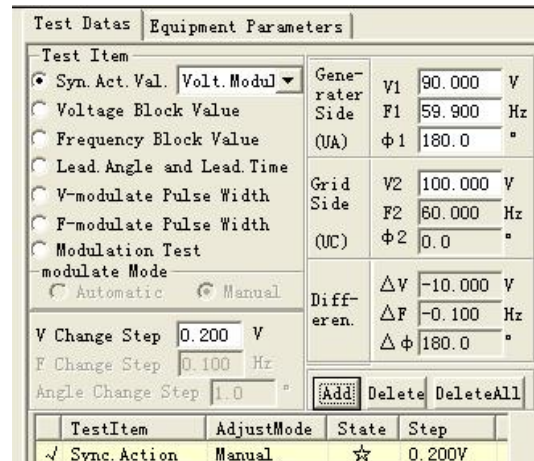
Section 1 Interface Instruction

■ Test item

- **Synchronization Action Value**

For testing action values of synchronous voltage difference, frequency difference, angle

difference. There are three options of 'Adjust voltage', 'Adjust angle' and 'Adjust frequency' in the pulldown menu on the right side. After one option is selected, set the 'Voltage (Frequency or Angle) Change Step'. You can start the test, then increase or decrease the variable step by step by hand till synchronization device acts. Then, the corresponding synchronous action value will be tested out. You can also test the line protection reclose with synchronization or nonvoltage detection by using this function.



When any one of the above-mentioned parameters needs to be tested, you should always make other two parameters to satisfy synchronization condition in advance. Through changing value of parameters needs to be tested to make the synchronous device to act finally after satisfying fully synchronization requirements.

We hereby take the test of synchronization voltage value as example for explaining the mode of test:

Set firstly 'Adjust Voltage', set generator side voltage V1 to be 90V, and it does not satisfy synchronization condition. Set generator side frequency F1 and phase $\Phi 1$ to satisfy synchronization condition (F1 can be set to be 49.9Hz that is very close to the grid side frequency; arbitrary phase, and can also be set to be equal 50Hz and the phase to be equal 0°), and set certain 'Voltage Change Step'. Clicking 'Add' button to add the parameters set into testing data area. After starting the test, pressing 'increase \blacktriangle (or decrease \blacktriangledown)' key by hand to change voltage till synchronization device acts.

During the test, you can observe the continuous change of angles in columns of 'generator side' and 'difference' if frequency is different. If pressing the 'synchronization indicator' button in buttons column, you can even observe from the synchronization window opened that voltage vector of generator side rotates continuously and its length varies at the same time. If frequencies of both sides are equal, the voltage vector of generator side won't rotate, and only its length varies. When three conditions - voltage, frequency and phase angle all satisfy synchronization requirements (two voltage vectors of both side are close to the allowable range), synchronization device will send out close-switch signal. Tester will record the voltage difference, frequency difference and angle difference when it acts.

Attention:

Mode for changing generator side voltage and angle value manually is to press ▲ and ▼ key on the keyboard. Mode for changing generator side frequency manually is to press key ◀ and ▶ on the keyboard. There will be hints when moving cursor to the button column.

Frequency of grid side in software is fixed to be 50Hz, angle be 0°, the default voltage of grid side is 100V but can be adjusted. Generator side voltage is output by UA of tester, and grid side voltage by UC of tester.

- **Voltage Locking Value**

Before the test, firstly set voltage and frequency of generator side for satisfying synchronization conditions but voltage and frequency has certain difference so that the angle difference can recede or close periodically. After starting the test, since voltage and frequency of two sides satisfy synchronization condition, the synchronization device will send out the close-switch signal whenever the angle put into the action range (it can be observed from the action indicating lamp of device). Increase or decrease the generator side voltage manually or automatically till synchronization device is locked (it will no longer act in angle action range). When it changes automatically, the tester changes generator side voltage towards the direction of increasing voltage difference each time, which make voltage difference to be increased gradually till synchronization device will no longer act (action locked), then the voltage difference locking value is tested out.

- **Frequency Locking Value**

Before the test, firstly set voltage and frequency of side for satisfying synchronization conditions but frequency has certain difference so that the angle difference can recede or close periodically. After starting the test, since voltage and frequency of two sides satisfy synchronization condition, the synchronization device will send out the close-switch signal whenever the angle put into the action range. Increase or decrease the generator side frequency manually or automatically till synchronization device is locked (it will no longer act in angle action range). When it changes automatically, the tester changes generator side frequency towards the direction of increasing frequency difference each time, which make frequency difference to be increased gradually till synchronization device will no longer act (action locked), then the frequency difference locking value is tested out.

- **Leading Angle and Leading Time**

Set voltages of two side to be equal before the test, and the frequency does not satisfy synchronization condition. After starting the test, synchronization device does not send out close-switch signal during angle rotation due to larger frequency difference. Increase or decrease frequency of generator side manually or automatically. When frequency is on the critical allowable action value, and when angle puts into the action range, synchronization device will act to send out close-switch signal first time. Tester will calculate and record the leading angle and leading time when frequency just satisfies the synchronization condition.

The following relation exists between leading angle and leading time:

$$\Delta\Phi = \Delta t / T_w \cdot 360^\circ \qquad T_w = 1 / |f_1 - f_2|$$

Among which: $\Delta\Phi$ is leading angle Δt is leading time

f_1 is frequency of generator side f_2 is frequency of grid side

In the state of automatic test, the tester always examine whether closing pulse is transmitted from the synchronization device in every period. If the tester does not receive closing pulse in one period, it will change automatically the frequency of generator side towards the direction of decreasing frequency difference. It adjusts like that in each period till the synchronization device signals. Software will calculate and record leading angle and leading time at that time.

- **Pulse Width of Voltage Regulating or Frequency Regulating**

When voltage difference and frequency difference do not satisfy synchronization conditions, the automatic quasi-synchronous device can transmit pulse width signals of increasing/ decreasing voltage or frequency automatically. The pulse width and period of this signal can be measure by this function.

Testing Mode of Pulse Width of Voltage Regulating:

Before the test, set the voltage of generator side not to satisfy synchronization condition (lower or higher than grid side voltage), set frequency of generator side to satisfy the condition but not to equal to the other in order that the angel difference can recede and close periodically. Connecting signals of increasing or decreasing voltage of synchronous device respectively with tester digital input A and a. When doing the test, the device won't transmit the closing signal due to voltage does not satisfy synchronization condition but it transmits 'Voltage increase (or decreasing)' signal periodically. Tester can measure the pulse width and period of voltage regulating under this voltage difference. The pulse width of voltage adjusting is normally linear

relation with voltage difference.

Testing Mode of Pulse Width of Frequency Adjusting:

Before the test, set the voltage of both sides to satisfy synchronization condition, but set frequency not to satisfy the condition (lower or higher than grid side frequency). Connecting signals of increasing or decreasing frequency of synchronization device respectively with tester digital input B and b. When doing the test, the device won't transmit the closing signal due to frequency does not satisfy synchronization condition, but it transmits 'Frequency increase (or decreasing)' signal periodically. Tester can measure the pulse width and period of frequency regulating under this frequency difference. The pulse width of frequency adjusting is normally linear relation with frequency difference.

- **Adjusting Test**

Before the test, set the voltage and frequency of generator side differ largely from those of system side, which could not satisfy synchronization condition. During the test, the synchronization device will transmit signals of 'increase voltage', 'decreasing voltage', 'increase frequency' or 'decreasing frequency', tester adjusts automatically generator side voltage and frequency towards the direction of 'satisfying synchronous condition' according to signals received at the variety ratio set. It won't be stopped until the synchronization device transmit closing order in the situation of voltage, frequency and angle all satisfying the synchronization condition. Tester will record the difference of voltage, frequency and angle when closing switch.

During the test, the voltage difference eligible lamp or frequency difference eligible lamp on synchronization device lights up when voltage difference or frequency difference satisfy the condition; if the angle difference also satisfy the condition, synchronous device will transmit closing signal at once. The above is the necessary three conditions of synchronization actions: frequency and voltage of both side is basically equal, and angle difference is smaller than certain value.

■ Other parameters

- **Adjusting Mode & Step Size**

In all test items, the software set different adjusting modes. When test items of 'synchronous action value', 'pulse width of voltage adjusting', 'pulse width of frequency adjusting', etc., the software only needs to be adjusted by hand. That is OK no matter several other items is adjusted by "hand operation' or 'automation'. In the adjusting way of "Hand Operation', it is required to

change output of variable through press ▲▼ and ◀▶ key on keyboard or press corresponding buttons on software's interface during the test; In the adjusting way of 'Automation', tester adjusts automatically output of variable according to signals of adjustment transmitted from synchronous device.

- **Add, Delete and Delete All**

You can complete all tests in one time when setting well several items. The basic operational process is as follows: Select test item——set all parameters required for testing this item——click the 'add' button after confirming all parameters are correct, and add this item into the listing box—— click the button of 'start test' to start the test, and it will test in sequence of items added. If you would like to delete certain item in test item list, select it through the mouse, then, click 'delete' button. If you would like to delete all items in the list, directly click 'delete all' button.

- **Synchronous Window**

Setting values of ΔV 、 ΔF 、 ΔF_{min} 、 ΔF_{max} and $\Delta \phi$ according to setting value of synchronous device. These values are only for your reference during the test, which do not influence the test. After completing the set, you can observe visually corresponding effect graph through the right graph. You will watch the testing track during the test.

- **Two Sides Fixed Angle Difference**

It is the combination of all fixed angle difference including wiring angle difference, transformer Y/ Δ angle difference, etc. of two sides. The software will compensate this angle automatically during the test.

- **Closing Time of Circuit Breaker**

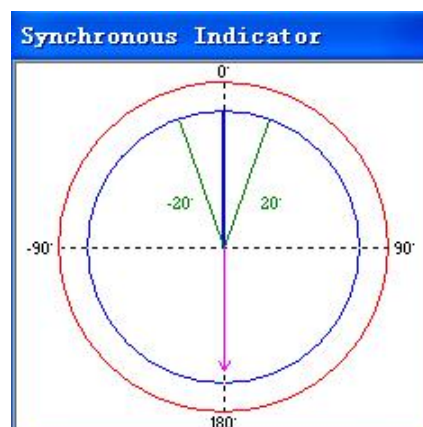
Closing time delay of circuit breaker: Time delay closing of circuit breaker after simulating synchronous device to issue the closing order.

- **Time of input flutter-proof**

For eliminating the influence on test due to contact flutter of protective relay during the test. For microcomputer synchronous device, it is normally set to be 5ms; for relay, it is normally set to be 20—40ms.

- **Synchronous Indicator**

Clicking the 'synchronous indicator' button to open the synchronous indicator during the test, then you can observe the variety vectorgraph of voltage amplitude



value, frequency and phase angle of generator side and system side during the test.

Section 2 Guidance for Test

■ Connection of Test

● Voltage Connection

Connecting the generator side voltage U1 with UA of tester; connecting system side voltage U2 with UC of tester; connecting common wire UN with UN of tester.

● Input connection:

Connecting the output signals of 'increase voltage', 'reduce voltage', 'increase frequency' and 'reduce frequency' of synchronous device respectively with input A, a, B and b of tester; connecting the export signal of closing action with input R of tester; short connecting another end of above-mentioned signals of synchronous device; connecting them to the public end (red end) of input of tester. If each output of protection is active contacts, please do connect positive power supply of each output contact with the public end of input of tester.

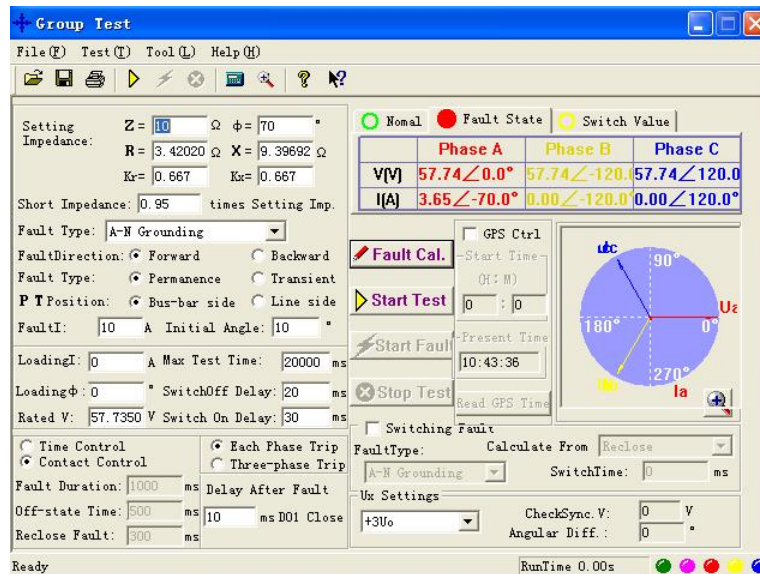
Attention:

When doing synchronous test, you should press the Start button of synchronous device firstly. Please check the input end of synchronous starting signal on the device for leading out two wires. After starting the test, firstly short connect them with start synchronous device. In addition, some synchronous device can be set synchronous time. During the test, if synchronous process is beyond this time, the device will lock out this time synchronous closing, and transmit alarm signal. You should press the synchronization start button or short connect the above-mentioned two wires for restarting synchronization.

Chapter 12 Full Group Test I & II

Overall test is equal to the static simulation test of relay protection tester. It simulates all kinds of faults of instant and nonvolatile single-phase earthing, phase to phase short circuit or convertibility for doing full group test for distance, zero sequence protective tester and action of reclosing or for verifying setting value. We hereby take the 'Overall Test I' as example to introduce briefly to its operating mode. The software interface is as the diagram:

- Testing the protection for overcurrent, zero sequence and distance of the full group, doing full group transmission test.
- Can test the action of reclosing and after acceleration under the condition of having or having not the synchronization detection and detecting non-voltage.
- Can simulate convertibility fault and negative direction.



Section 1 Interface Instruction

■ Setting Component of Fault

● Type of Fault

You can set it to be the fault of Type AN、BN、CN、AB、BC、CA、ABN、BCN、CAN、ABC.

● Setting Impedance

According to the impedance setting mode given by the setting value list, the fault impedance can be input in the Z or Φ mode or be output in R or X mode. When inputting it in one mode, software will work out automatically the value of another mode.

● Multiple of Short Impedance

It is $n \times$ 'Setting Impedance'. Take this value to be impedance on short circuit point for doing the simulation. Normally it does the test in 0.95 or 1.05 times of setting value. If it could not be satisfied, you can also do the test in 0.8 or 1.2 times of setting value. It is the testing limit to 'Tolerance'. If the protection still could not be operated correctly, please examine whether there are other reasons exist.

- **Zero Sequence Compensating Factor**

$$K_0 = (Z_0 / Z_1 - 1) / 3$$

If the Zero Sequence Impedance Angle $\Phi(Z_1)$ is not equal to the Zero Sequence Impedance Angle $\Phi(Z_0)$, K_0 will be a plurality. Then normally K_{or} , K_{ox} will be used for calculation.

$$K_{or} = (R_0 / R_1 - 1) / 3 \quad K_{ox} = (X_0 / X_1 - 1) / 3$$

For some protections that is calculated in the mode of K_0 , Φ (such as Series 901), if $\Phi(Z_1) = \Phi(Z_0)$, then $PS_1 = PS_0$, so K_0 will be a real number. You should set $K_{or} = K_{ox} = K_0$ at that time.

- **Fault Direction**

It protection has directivity, please do select correct fault direction.

- **Character of Fault**

Difference of option 'instantaneity' and option 'permanence' is: in the testing mode of 'Time Control', when the 'instantaneity' fault is selected, the tester will stop output fault and enter next state when it acknowledges the action signal of protection though the fault time still has not been ended at that time; however, in the testing mode of 'permanence', the component of fault will still exist till the 'fault standing time' is up even though the tester acknowledges the action signal of protection. Which means fault output time of the tester is only controlled by the 'fault standing time' when it is in the mode of 'permanence' fault. So doing test in the mode of 'permanence' fault leads to the action of after acceleration protection easily, which also leads to that the reclosing could not be reclosingd. So we suggest that you select normally the fault mode of 'instantaneity'.

- **Fault Current**

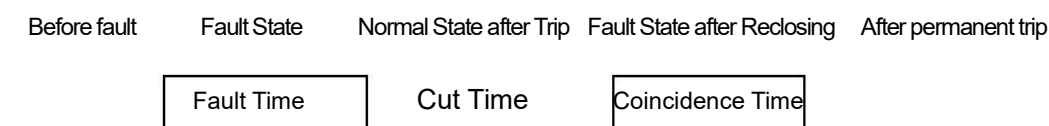
Only short circuit impedance is set above. If you tell software certain fault current furtherly, the software will work out corresponding fault voltage automatically, and the tester will output corresponding fault voltage and current to protection. The fault current set should satisfy the following requirements: 1. Larger than pickup current of protection; 2. Product of fault current and short circuit impedance should not be larger than 57.7V.

- **Time Control/ Contact Control**

When 'Contact Control' is selected, the testing state will be controlled by signals of trip, reclosing and permanent trip contact displacement of protection received by tester, which will

decide that the tester outputs current and voltage at corresponding state.

When 'Time Control' is selected, the tester will output all kinds of component including 'before fault', 'during the fault', 'trip', 'reclosing', 'after permanent trip' in sequence according to the time sequence set, and the it only record time but do not change output process of all kinds of component when the protection trips.



- **Fault Time, Cut Time and Reclosing Time**

The mode of time control is used for controlling the standing time of output of failure component, the standing time of output of normal component after cutting the fault, and the standing time of re-output of failure component of reclosing as the above graph shows. It does not work in the mode of contact control.

- **Convertible Fault / Non-convertible Fault**

Being used for setting convertible fault. Beginning from the start of fault, it will all trip the breaker and enter the state of 'fault after conversion' no matter the protection acts or not as soon as the convertible time is up. But the voltage-current of trip phase does not influenced by the state of convertibility fault. Its voltage $V=57.7V$ (PT is set on the bus side) or OV (PT is set on the line side), and $I=0A$. The Fault Convertible Time stands for the time calculated from the beginning of the first fault.

- **Fault Type after Conversion**

It can be set to be Type AN、BN、CN、AB、BC、CA、ABN、BCN、CAN、ABC. Normally we set the fault type after conversion to be different form the first fault type, which is more tally with the actual situation.

- **Convertible Original Moment and Convertible Time**

It can be set to begin calculation from starting the first fault, or after tripping of protection, or after coinciding the gate for deciding when the fault conversion happens.

- **Original Angle of Fault**

It is the original angle of voltage when the fault happens. Since phases of three phases voltage-current are different, switch-on angle relates to the fault type. Normally it calculates according to reference phase of this type of fault: for single phase, it calculates according to fault phase; for two-phase short circuit or two-phase earthing, it calculates according to non-fault phase; for three-phase short circuit, it calculates according to Phase A.

- **PT Mounted Position**

Deciding where the primary side voltage transformer should be mounted, bus side or line side. When PT is mounted on bus side, after this phase is cut off, current of fault phase is zero, and voltage gets back to normal phase voltage ($V=57.7V$, $I=0A$); When PT is mounted on line side, after the fault phase is cut off, current and voltage of this phase will all be zero ($V=0V$, $I=0A$).

- **Split Phase Trip/ Three-phase Trip**

Being used for defining input A, B and C three terminals, regarding them as Terminal 'Trip A', 'Trip B' and 'Trip C' or Terminal 'Three Trip'?. If it is set to be 'Split Phase Trip', it can simulate the situation of only tripping fault phase when it is single phase fault. Which means which signal among 'Trip A', 'Trip B' and 'Trip C' arrives first, it will simulate the trip of those corresponding phases.

- **Breaker off/on Delay**

For simulating off/on time of breaker. After acknowledging off/on signals of protection, it will wait switch's off/on delay for a while, then, switching voltage-current to the state after switching off or on.

- **Output 1 delayed closing time after fault**

Output 1 will delay this time closing after outputting component of fault. This function can be used for: simulating the 'offside signal collecting input' of receiver and transmitter by using 1 given when testing high frequency protection.

- **Output 2**

Output 2 varies by tracking the state of breaker. Which means Output 2 cuts off when the protection trips; output 2 will close when the protection reclosings. So output 2 can be used as analog breaker.

■ **Setting Synchronization Detection Reclosing & Ux**

- **Ux Option**

Ux is a special phase that can be set for outputting $+3U_0$, $-3U_0$, $+\sqrt{3} \times 3U_0$, $-\sqrt{3} \times 3U_0$, Synchronization Detection Ua, Synchronization Detection Ub, Synchronization Detection Uc, Synchronization Detection Ucb, Synchronization Detection Uca and Synchronization Detection Uab.

For the first four kinds of $3U_0$ situations, output value of Ux is obtained by $3U_0$ combined by Ua with Ub and Uc output currently being multiplied by all factors, and it will vary along with them.

If selecting it to be equal to the extract voltage value of certain synchronization detection, Ux

will be used for simulating the extract voltage of line side when the testing line is protecting reclosing of synchronization detection. Take the Synchronization Detection U_a as example, U_x output value is always equal to bus side U_a (but the numerical value is 100V) in the state of closing breaker; U_x value will be equal to the amplitude value and phase angle of synchronization detection voltage set in the state of cut-off after the protection trips, and this value can be set as the U_a numerical value or differed phase at that moment for testing the synchronization detection reclosing when the protection is in the situation that two sides voltage differs.

■ Instruction to Full Group Test II

Function of Full Group Test II is basically as same as the one of Full Group Test I. In Full Group Test I, all fault situations are set according to impedance modes for protecting full group test. But it could not acknowledge the fault impedance but only have fault voltage and current for certain protection, such as zero sequence protection or 35 KV line protection. At that time, you can use Full Group Test II to do the test.

- **Type of Fault**

It can be set as AN、BN、CN、AB、BC、CA、ABC type fault.

- **Fault Voltage U**

For single phase fault and three-phase fault, the Fault Voltage U is the value of fault phase voltage; for phase to phase fault, the Fault Voltage U is the line voltage value of two phases of fault.

- **Setting Current I**

It is the setting current value for protecting certain segment.

- **Multiple of Short Circuit Current**

Short circuit current is the 'Setting Current' of Test Multiple nX , it will do analog test by regarding this value as short circuit point current.

Attention:

1. In the full group test, all fault data will be completed by computer. Every phase of short circuit voltage obtained by calculating the fault current and fault impedance set by computer should not be larger than rated voltage (57.7V). If it is too large, the fault current value will be reduced automatically for satisfying the condition of $V_f \leq \text{rated voltage (57.7V)}$.



2. If the fault impedance is smaller, you should normally set heavier fault current; if

the fault impedance is heavier, you can set smaller fault current so as to give suitable fault voltage, which is also in accordance with actual operation. Otherwise, it may influence the testing result.

Other options and testing process are all completely as same as the Full Group Test 1.

Section 2 Test Instruction

■ Explanation of Process of Full Group Test

Complete the data set, press , the tester will output symmetrical component of every phase of 'Normal State'. All phase voltage is the rated voltage (57.7V) and current is load current at that time. Press the '' button or connect 'Input c', the tester will get into fault state, output fault current, and add it to the protective tester. After the protection trips, the tester will output component of state after tripping. After the protection coinciding the gate, the tester will output normal component (each phase voltage is 57.7V, current is load current) if it is the instant fault; If it is the permanent fault, the tester will output the component of fault again till protection trips for the second time (permanent trip), then, resuming output normal component.

- **Tester enters the fault state automatically when 'Input c' is switched on**

It has two functions: 1. It can accelerate to trip after it arrives at the fault line by simulating the manual closing mode. It can measure action time conveniently. Detail operation is to connect the manual contact or TWJ contact with 'Input c', the contact action tester will output the component of fault when closing it by hand, which can test the action of protection. 2. The fault can be started by contacts of GPS tester for simulating synchronous fault on two sides of line.

During the test, whenever you press the 'Stop' key, the testing process will be terminated and it will escape.

After completing the test, computer will file automatically the testing result in the testing record area under the subdirectory 'Test Report\Full Group Test\' in text formatting, and it can also be displayed or printed by the 'Printing' button, or it can also be copied for being edited or amended.

■ GPS Control Test

Process of full group test can be controlled by GPS for simulating the simultaneous and synchronous test of the protection on two sides of double power supply circuit, which means these two testers on two sides will be started simultaneously and synchronously by GPS controller to enter the state before fault and the state of fault. Loading the protection for each side

given by component of fault for testing the simultaneous action of two sides' protection.

- **GPS Pulse Output:**

The pulse export of GPS tester will output two lines of pulse, one is PPS pulse that will be transmitted every second; another is PPM pulse that will be transmitted every minute. Every time when PPS or PPM pulse is transmitted, a PPS indicating lamp and a PPM indicating lamp on faceplate will twinkle. We hereby do test by using PPM pulse. Output of pulse is terminal output.

- **Outputting GPS Clock Signals**

There is RS232 out let in GPS tester for outputting clock. Out let is Type D 9 needle socket. Connecting this out let with RS232 port of PC, and PC machine will read GPS time.

- **Connection between GPS Tester and Tester Tester:**

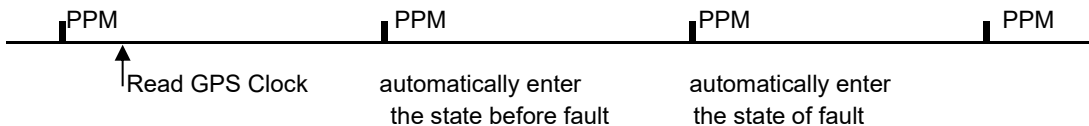
By using the special GPS connecting wire provided by us, connecting the pulse output terminal and clock output Rs232 port of GPS tester with the GPS communication port on backplate of tester.

- **Comparing the time with GPS tester:**

For ensuring test's synchronization, click 'read GPS clock' on the 'Full Group Test' interface of PC machine to implementing the synchronous clock with GPS tester. If comparing the time with it is successful, a hint will be displayed.

- **Start Test:**

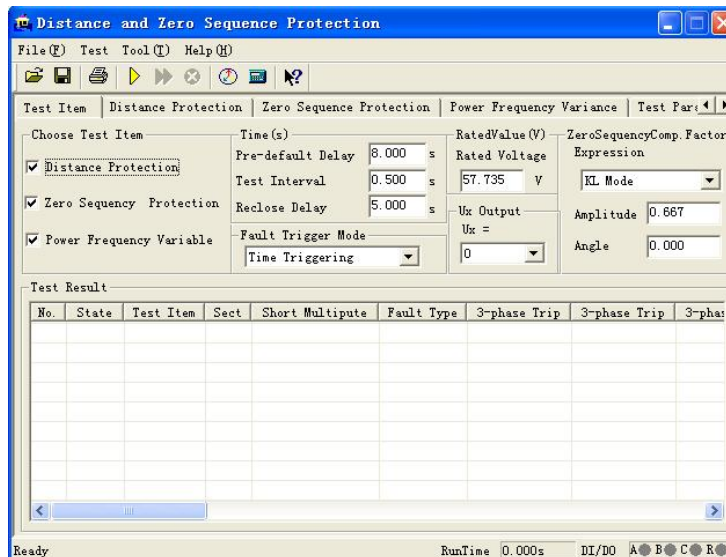
Tick the option of 'GPS control begins to test' on the interface of 'Full Group Test', and click 'Read GPS Clock' to implement the clock synchronization with GPS tester. Then, two sides' operators all set the 'Start Test Time' to be the same time (this time must be later than current time). When 'Start Test Time' is up, two sides testers start the current-voltage before the synchronous output fault at the moment when PPM twinkles, and enter the fault state and output component of fault synchronously at the moment when next PPM twinkles. The whole process is as the following graph:



Chapter 13 Distance & Zero Sequence Protection

In 110KV and above line protection, normally distance and zero sequence protection is set as main protection of line, and they often concentrate in a set of protective tester. The testing module of distance and zero sequence protection is a software developed aiming at this situation, which can complete automatically all kinds of earthing distance, phase to phase distance and zero sequence protection.

- Can automatically complete verification of all fault setting value of several segments direction and zero sequence protection.
- Can test the time when protective three-phase trips synchronously or not in the same fault.
- Can set permanent fault, test the time of reclosing and permanent trip.
- Not only can adopt Mode Z、 Φ , but also can adopt Mode R、X to set impedance setting value.
- Through setting the mode of 'pressing key for trigger', you can control output of component of fault by hand.



Section 1 Interface Instruction

■ Test items

'Distance Protection', "Zero Sequence Protection" and 'Power Frequency' three test items are available, which can be selected separately, and also can be selected simultaneously.

- **Time Parameter**

Time Delay before Fault This time is often used for waiting full group revert of protection after each time action, or disappear of "TV break of conductor" signal, or waiting for charging of reclosing. If it is only used for testing protective setting value but not been put into reclosing, this time is normally set 2~10s. If doing synchronously the reclosing test, it will be normally 15~25s. Every time when doing the fault test, tester will firstly enter the state of 'Time delay before fault', outputting three-phase rated voltage 57.7V, three-phase current is 0, and then entering the fault state again for outputting the component of fault set.

Off-hours of Test Every time when the fault test is ended, tester will stop output, it will wait for revert of protective contacts at this time state, normally setting it to be 0.5s is OK, and can also be set as 0.

The largest delay of reclosing If putting it into reclosing, doing reclosing test synchronously every time when doing fault test, the waiting for signals of reclosing within this time. This time should be larger than the time delay of setting reclosing.

- **Mode for triggering fault**

There are four kinds of triggering mode from the state of 'before fault' to state of 'fault': time control, key trigger, input c trigger and GPS trigger.

Time Control In this triggering mode, standing time of the state of 'before fault' will be confirmed by 'time delay before fault'. When time is up, it will enter the state of fault automatically. Under the control of time, the tester will do test automatically. You only need to switch shunt corresponding platen during the test.

Key-press Trigger In the state of 'before fault', press any key on keyboard of faceplate, or click the trigger key on software by mouse, it will enter the state of fault. The key-press trigger mode implements the process of manpower controlling test conveniently, which is convenient for observing message of protection or printing testing result during the test.

Input c trigger Input c of tester will enter the state of fault as soon as acknowledging the signal of displacement. This function can be used for doing tests for many testers synchronously.

GPSTrigger Connect GPS signal with communication port on backplate, doing combined adjusting test for two testers in different interspace through PPM pulse of GPS. It will enter the fault state when PPM pulse arrives

- **Zero Sequence Compensating Factor**

Providing K_L 、 K_r/K_x 、 Z_0/Z_1 totally three kinds of expressing modes. For detail instruction, please refer to the instruction in the chapter of ‘Intercommunicate Experience’. When doing earthing distance test, you must set correctly zero sequence compensating factor.

Distance Protection

Only when the test item of ‘Distance Protection’ is selected, this page will be at the active state, and it will allow setting corresponding parameters as shown on the right diagram:

Sect	Z (Ω)	Φ (Ω)	R (Ω)	X (Ω)	TestI (A)	TestTime (s)	SettingTime (s)	Direction
<input checked="" type="checkbox"/>	2.000	90.000	0.000	2.000	5.000	0.200	0.000	Forward
<input checked="" type="checkbox"/>	4.000	90.000	0.000	4.000	4.000	0.700	0.500	Forward
<input checked="" type="checkbox"/>	6.000	90.000	0.000	6.000	3.000	1.200	1.000	Forward
<input type="checkbox"/>	8.000	90.000	0.000	8.000	2.000	1.700	1.500	Forward
<input type="checkbox"/>	10.000	90.000	0.000	10.000	1.000	2.200	2.000	Forward

InterphaseZ-Φ Mode
 InterphaseR-X Mode
 A-B Fault
 B-C Fault
 C-A Fault
 3-Phase Fault

Sect	Z (Ω)	Φ (Ω)	R (Ω)	X (Ω)	TestI (A)	TestTime (s)	SettingTime (s)	Direction
<input checked="" type="checkbox"/>	2.000	90.000	0.000	2.000	5.000	0.200	0.000	Forward
<input checked="" type="checkbox"/>	4.000	90.000	0.000	4.000	4.000	0.700	0.500	Forward
<input checked="" type="checkbox"/>	6.000	90.000	0.000	6.000	3.000	1.200	1.000	Forward
<input type="checkbox"/>	8.000	90.000	0.000	8.000	2.000	1.700	1.500	Forward
<input type="checkbox"/>	10.000	90.000	0.000	10.000	1.000	2.200	2.000	Forward

Grounding Z-Φ Mode
 Grounding R-X Mode
 A-N Grounding
 B-N Grounding
 C-N Grounding

Test Impedance Multiple

0.800
 0.950
 1.050
 1.200

- **Phase to phase Short Circuit Impedance & Earthing Distance Impedance**

- 1、 You can tick ‘√’ for selecting the protection tests you needs to do.
- 2、 Input directly the setting value of protection in the box of impedance data. You can select to input setting value in Mode Z-Φ or Mode R-X.
- 3、 Each segment of current set must be larger than the inrush current of protection. Also the product of its impedance and current should better to be in the range of 20 — 40V during the phase to phase distance test, which must not be over 57v; During the earthing distance test, you’d better set the product of its impedance and current to be about in the 20 — 30V, that must not be over 57V. Normally you should also abide by the principle of the smaller the impedance (or reactance) is, the heavier the current will be, then you can ensure the test to be more accurate.
- 4、 Every segment of ‘Testing Time’ set must be larger than the setting action time of this segment. For example, suppose the action time of Segment I is 0s, then the one of Segment II is

0.5s, and the one of Segment III is 1.0s. Considering that trip of the protection itself has certain setting time delay, you can set the testing time of Segment I, II and III respectively to be 0.2s, 0.7s and 1.2s as the above diagram shows. So the ideal result of test will be: local segment acts when it is 0.95 times; local segment does not act when it is 1.05 times; it could not act if the next segment of time is not enough. You can also set three segments of times above-mentioned all to be larger than the third segment of action time. So the ideal result of test will be: local segment acts when it is 0.95 times; local segment does not act when it is 1.05 times.

5、 Input all segments of setting action time in the box of 'setting time', and this time parameter is only used for reference, that won't influence the test result.

6、 Clicking in the column of 'direction', you can switch between 'forward direction' and 'reverse' so as to test conveniently some distance protections of directivity.

7、 Finally selecting the fault type needs to be test, among which the single phase earthing fault is used to verify earthing distance impedance; two-phase short circuit and three phase short circuit are used to verify phase to phase distance impedance. If you want to do earthing distance test, the zero sequence compenstating factor should be input correctly.

- **Multiple of Testing Impedance**

According to normal requirements for protective verification, the software provides 0.8 times, 0.95 times, 1.05 times and 1.2 times four kinds of default verifying multiple, and its numerical value can be amended. If the protection does not act in 0.95 times or 1.05 times, you can select 0.8 times or 1.2 times at that time, and you also can define the multiple by yourself to do test.

■ Zero Sequence Protection

Only when the test item of 'zero sequence protection' is selected, this page will be at the active state for allowing set of corresponding parameters as shown on the right diagram. Set of testing parameters for zero sequence protection is basically the same as the set of testing parameters for distance protection. When setting it, please refer to the instruction of above paragraph.

- **Calculating Mode of Short Circuit**

Mode for making voltage to be constant

For directly setting fault phase voltage in this mode. During the test, the fault phase voltage output by tester will maintain unchanged whatever how heavy the fault current is. 'Fault Phase

Voltage Angle' stands for the included angle of fault voltage and fault current.

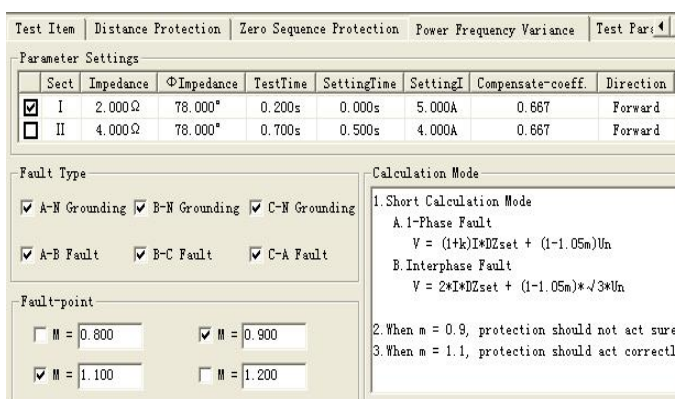
Mode for making impedance to be constant

In this mode, the fault phase voltage will be calculated by fault current and fault impedance during the test.

■ Verifying setting value of power frequency variable impedance component

This test item is used for testing the action behavior of power frequency variable impedance relay, and it can verify the setting value of power frequency variable distance protection of certain lines as shown on the right diagram:

This mode allows verifying two segments of setting value at the same time, and simulating all types of fault once. When doing the test, you only need to tick the test item needs to be test, then setting parameters of all kinds of setting value in sequence according to the setting value list.



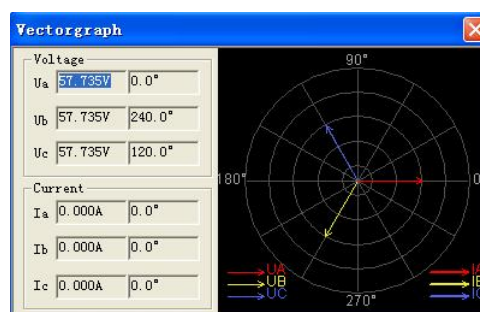
M has 0.9 and 1.1 two kinds of value in the default situation. Normally, the protection does not act reliably when M=0.9; the protection should be act reliably when M=1.1. You can measure the action time of protection when setting M=1.2

The parameter of 'short circuit current' should be set larger, 10~20 A is suggested. Since the short circuit current is too low, voltage calculated according to the above-mentioned formula may be a negative value. When doing the test, the 'distance protection' platen should be used.

Setting of the testing parameters is basically the same as setting of protection. Please refer to its instruction.

■ Vectorgraph

Click the 'vectorgraph' button during the test, you can observe actual vectorgraph of amplitude value and phase of voltage and current vector from the vectorgraph window opened. As shown on the right diagram:



Section 2 Guidance for Test

Correct Connecting

When split phase trips, connecting Trip A, Trip B, Trip C and reclosing signal of protection with input terminal A, B, C and R; When the third trip happens, putting the trip signal in any terminal of A, B and C, and connect reclosing with R terminal.

Put-in or recede platen

Please input the protective platen corresponding to the item tested.

Select the test item, and set parameters of all items. For normal trigger mode, it will be set as the 'Time Control' mode.

No.	State	Test Item	Sect	Short Multipute	Fault Type	3-phase Trip	3-phase Trip	3-Phase Trip
1	☆	Interp...	I	0.950	A-B Fault			
2	☆	Interp...	I	1.050	A-B Fault			
3	☆	Interp...	II	0.950	A-B Fault			
4	☆	Interp...	II	1.050	A-B Fault			
5	☆	Interp...	III	0.950	A-B Fault			
6	☆	Interp...	III	1.050	A-B Fault			
7	☆	Ground...	I	0.950	A-N Gro...			
8	☆	Ground...	I	1.050	A-N Gro...			
9	☆	Ground...	II	0.950	A-N Gro...			

Software will go back to the

first page after the test, and doing tests in the sequence of testing data in list as shown on the right picture.

If you test synchronously earthing distance and zero sequence protection, the software will drop a hint of 'please recede zero sequence protective plate, and input distance protective plate' during doing the test of earthing distance protection; software will drop a hint of 'please recede distance protective platen, and input zero sequence protective plate' when doing the test of zero protection.

After ending the test, please save the test report according to the hint.

0.95 times and 1.05 times are two testing boundary points defaulted. When 0.95 times is selected, the local segment of distance protection should act reliably, and the local segment of zero sequence protection should not act reliably; when 1.05 times is selected, the local segment of distance protection should not act reliably, and zero protection should act reliably. In addition, Option 0.8 times and 1.2 times are available for reducing requirements for protective action when tests of 0.95 times and 1.05 times could not satisfy requirements of the above-mentioned action, those are tests of 'tolerance'. If it still could not act correctly, please check reasons of protection and contact with protection manufacturer for settling this problem.

During the test, if Segment II or Segment III should act, but you find that the action time

recorded by tester is the action time of Segment I, please check whether the after acceleration of reclosing mis-operates. If so, please recede the after accelerate platen of reclosing or control words, then to do the test again.

When doing the test, if Trip A, B and C of protection is connected with Input A, B and C of tester, and you always hear that the tester sounds long 'woo' for alarming occasionally, but actually the tester could not record the action time of protection. Then, please check the fault phase always relates to which phase. For example, this situation occurred while the AC phase to phase fault, and it also occurred while BC phase to phase fault, so you can determine preliminarily that tester did not receive the signal of switching displacement transmitting from Protection Trip C. Please check whether the Protection Side Trip C is connected well. You can also short connect three signal lines of Protection Trip A, B and C, and connecting them together with Input A of tester.

If you want to make the protection to be under the multiple of certain setting value, make next segment of protection to act when local segment of protection does not act. Please set the 'largest fault time' of this segment to be larger than next segment of protective action time, 0.2s or above.

Attention:

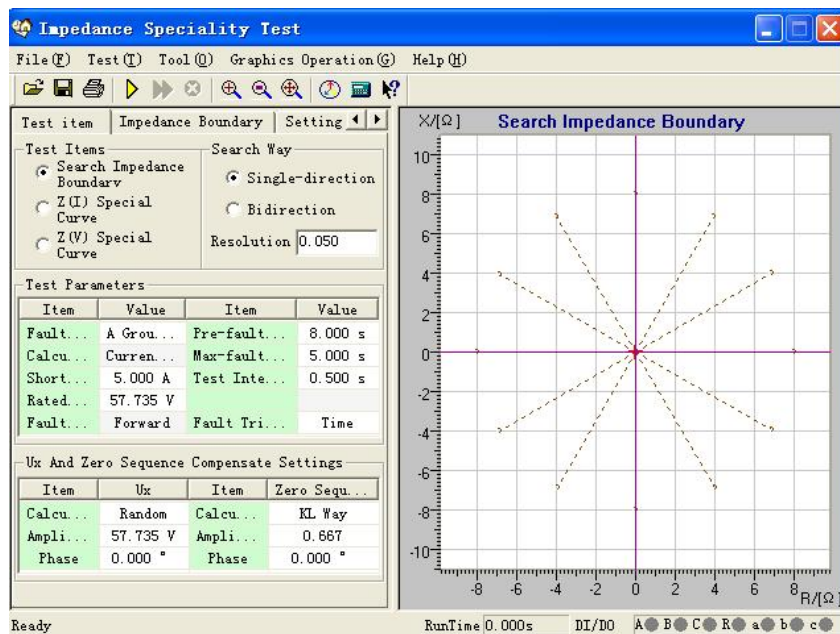
1. The setting value of some protections such as the parallelogram characteristic protection of the Sifang Company is given in the way of reactance XX1—XX4、XD1—XD4, you only need to set the component of Reactance X, its component of Impedance R should be set as 0.

2. If you do the test of earthing distance protection, please set correctly zero sequence compensating factor according to the zero sequence compensating type and numerical value given by the setting setting value list.

Chapter 14 Characteristic of Impedance

This testing module is mainly used for searching the boundary of impedance action of distance protection aiming at its characteristic of action. It can search the boundary of impedance action of circular characteristic, polygon characteristic, arc, beeline and other characteristics. This testing module provides two different searching methods, 'Unidirectional Search' and 'Bidirection Search' as the following diagram shows:

- searching the characteristic graph of circle, polygon and other impedance.
- Setting parameters according to hints; software can draw graph approximately and can be compared with the searching graph conveniently.



Section 1 Interface Instruction

■ Test item

For every test, only one item of 'impedance boundary search', 'Z (I) characteristic curve' or 'Z (V) characteristic curve' should be selected.

- **Fault Type** All kinds of fault types are available for testing all kinds of distance protections. For earthing type distance relay, single-phase earthing fault should be selected; for phase to phase type distance protection, the phase to phrase fault should be selected.

- **Calculation Model** Two kinds of Calculation models, 'Constant Current' and 'Constant

Voltage, are available. When 'Constant Current' is selected, short circuit current can be set in the following box. The software will work out corresponding short circuit voltage according to short circuit current and short circuit impedance; when 'Constant Voltage' is selected, short circuit voltage can be set in the following box. The software will work out corresponding short circuit current according to short circuit voltage and short circuit impedance.

- **Searching Mode** Two kinds of modes are available, 'Unidirection Search' and 'Bidirectional Search'. For detail introduction, please refer to corresponding instruction on the chapter of 'Differential Protection'. The resolution is only effective for 'Bidirectional Search', and it decides the testing precision of bidirectional searching mode.

- **Mode of Fault Triggering** In the triggering mode of 'Time Control', software will test circularly in the sequence of 'time delay before fault' — 'the largest fault time' — 'interval of test'. For detail instruction, please refer to corresponding instruction on 'Line Protection'.

- **Direction of Fault** Setting it according to the setting value menu of protection, which is suitable for protection of directivity impedance.

- **Zero Sequence Compensating Factor** If you do the test of earthing distance relay, please do set correct zero sequence compensating factor. Please refer to corresponding instruction on 'Line Protection'.

■ Searching Boundary of Impedance

When the test item of 'searching boundary of impedance' is selected, radial scanning beam needs to be set as shown on the right diagram. For setting the scanning beam, please refer to the following mode:

- **Scanning Centre** The scanning centre should be set around the central position of characteristic graph of theoretical impedance of protection. You can put data directly in scanning centre, and also can click for selecting the scanning centre by the mouse. After the scanning center is revised, the coordinate axis will be adjusted automatically for ensuring that the scanning circle is always in the central position of graph, which means the scanning centre should be in the centre of graph.

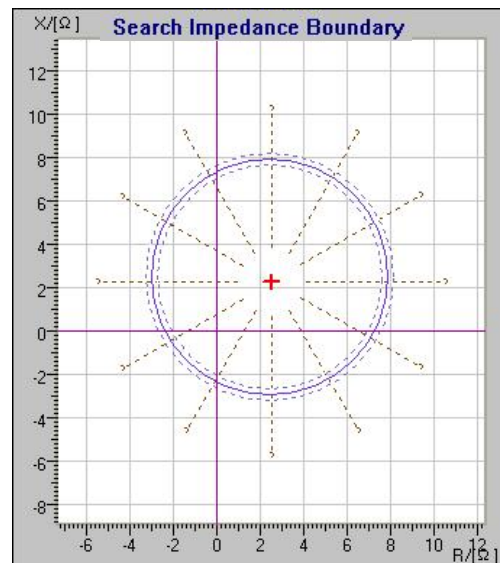
- **Scanning Radius** The Scanning radius should be larger than half of the setting value of protective impedance for ensuring that scanning circle covers all action boundaries of

Impedance Boundary		Setting Parameters		
Center Parameters				
Items	Center Position	Mouse Position		
Z	9.063 Ω	20.747 Ω		
Φ	42.019 °	46.302 °		
R	6.733 Ω	14.333 Ω		
X	6.067 Ω	15.000 Ω		
Course Parameters				
Items	Value	Items	Value	
Radius	8.000 Ω	Start...	0.000 °	
Step	1.000 Ω	End A...	360.000 °	
Range	100.000 %	Angle...	30.000 °	
		Line ...	12	
Test Results				
No.	State	Current	Setting imp...	Se

protection. Scanning will begin from the non-action area (points outside scanning beam) . During the test, if you find that the protection acts when it is scanning the outside point of certain search track, it represents that this scanning beam does not go beyond actual impedance's boundary, which means the whole search beams are in the active area, which does't conform to the principle of 'part of every search beam should be in the active area, but other part should be outside the active area'. At that time, please increase the 'scanning radius' properly.

● **Scanning Step Size** It is only effective for the mode of 'Unidirection Search', which influences directly the testing precision when the mode of 'Unidirection Search' is selected.

● **Scanning Range** It scans in one hundred percentage range in the condition of default. Setting suitable scanning range can normally avoid misoperation of other segment of impedance. For example, setting the scanning range to be 80%, searching beam is shown as the right diagram:



● **Searching Angle** Setting a series of searching beam through setting start angle, end angle and step size of angle. If the step size of angle is set very small, though it finds out many points that are favorable to increase precision of boundary search, the testing time will also be increased largely. So please select suitable step size of angle when you do actual test.

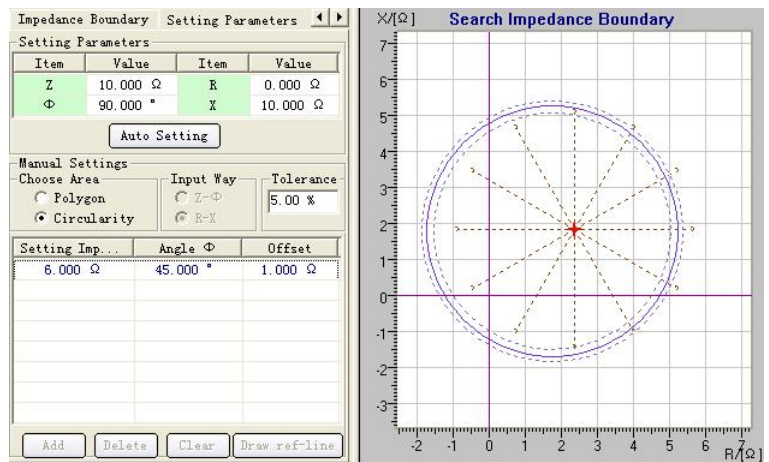
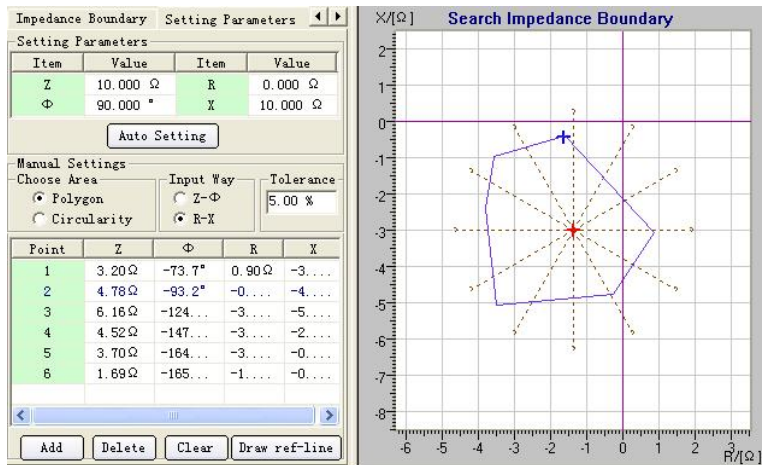
● **Automatically setting scanning parameters** On the the parameters setting page, after finishing impedance value setting, the software will automatically work out scanning central position and empiric value of scanning radius according to impedance value setting . If this value is still not appropriate ,you can adjust it based on above operation.

■ Setting Parameters

You can do the test without drawing the boundary graph of theoretical impedance on the interface of 'Setting Parameters', however, the user can determine more easily the central point of search and length of searching beam if the theoretical graph is available, which is also convenient for comparing the testing results. We explain the drawing method in the following paragraph.

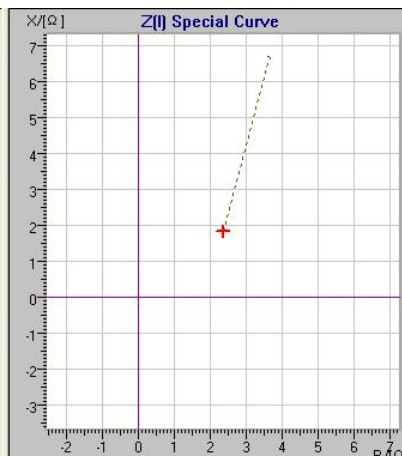
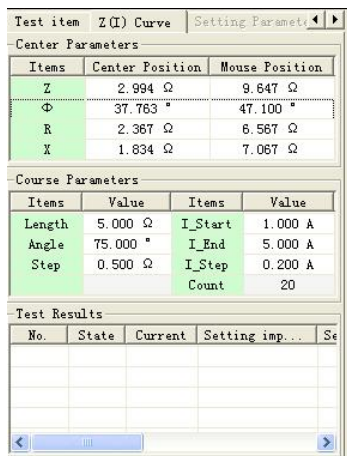
Drawing Polygon Select the characteristic of polygon, and select Data Input Mode

'R-X' or 'Z-Φ', then set the coordinate (R1, X1) of the first point of the angle in the column of 'angle point'. Usually the first point of the angle should be set as (0, 0). After completing the setting, click the 'add' key, and set the second point of the angle in the same way. The right diagram shows that these two points construct a line. Add several points in sequence according to setting parameters of protection. When setting parameters, R and X can all be set as negative numbers. Click the 'drawing' button after completing the addition. then the software will draw the curve of theoretical impedance boundary and corresponding error curve (as the dashed shows), you can move the cursor to central position of diagram, then click the left key of mouse to set scanning central point as the right diagram shows.



Drawing Circle Select

'Circle' in set 'setting' of 'offset' following interface real-time



Characteristic above diagram, and parameters such as impedance, 'angle impedance' and quantity' in the diagram. The right will display its figure. Click the

centre of diagram by mouse, and set enough large scanning radius and corresponding step size on the interface of 'search impedance boundary' as the right diagram shows.

■ Characteristic Curve

Select the test item of 'Z (I) characteristic curve' on the interface of 'test item' for testing relation between current and impedance. Please refer to the diagram above.

Parameters Set On the interface of 'Z (I) characteristic curve', set origin point, length and angle of searching beam, and original value and final value of current according to hints and setting value list. Afterwards you can observe actual effect diagram.

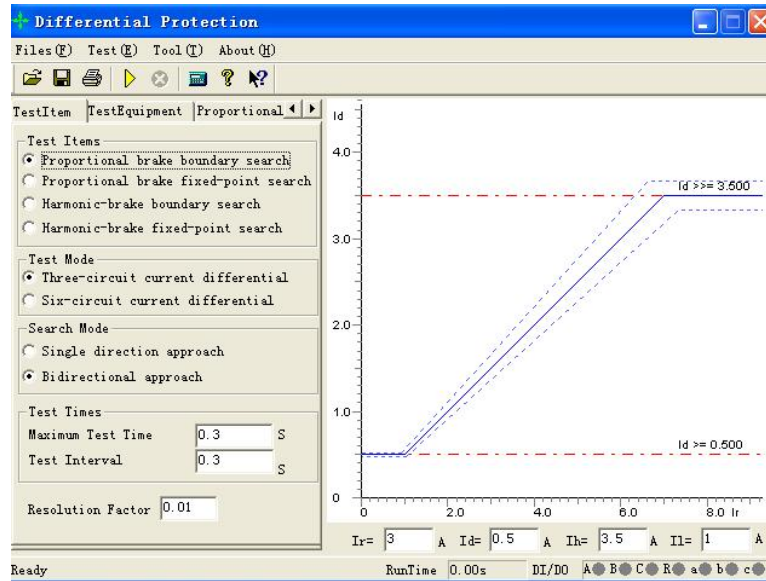
The process of this test resembles that of differential relay. If we can consider the impedance here as the 'differential current' of differential test, the current here is equivalent to the 'operating current'. When doing the test, the original value of impedance is 0 that will be increased in certain step size of search. It tests the operating current of protection of every impedance value. After completing the test, software will draw corresponding curve automatically. For 'Z (V) Characteristic Curve', please refer to 'Z (I) characteristic curve'.

Chapter 15 Differential Protection

The unit of differential protection is designed according to the characteristics of micro-computer type or integrates circuit type transformer, generator and differential protection of Motor. It is used for testing automatically its characteristics of ratio control, harmonic control, action time, etc.

Different from the 'characteristic test of differential relay control', this module does not do the test by directly loading action current and brake current on test, but loading primary current and secondary current on differential protective tester by simulating them, then it will combin action current and brake current by the protection.

- Automatically searching characteristic curve of ratio control and harmonic control;
- Setting points for doing ratio restraint control test and harmonic restraint control test by will, and it can test action time;
- Drawn the theoretical characteristic curve of ratio restraint and harmonic restraint test in advance and estimate error range;
- Setting many kinds of arithmetic of brake current and action current controlled of ration restraint and harmonic restraint test;
- Secondary current verification of TA can be implemented by high side adjustment, low side adjustment or internal connecting adjustment (selecting the 'do not adjust' in the software);
- For harmonic control, you can select 2~7 order harmonic;
- Fundamental wave and harmonic can be output separately from two sides, and also can be superposed to output from one side;
- Directly setting balance coefficient, and it can automatically finish calculation according to parameters of transformer. It can be used for testing differential protection of per unit value.
- Can output three channels current for doing single-phase differential test, and also can output six channels for doing high-low side full 6 phases differential test.



Section 1 Interface Instruction

■ Test item

The software provides four kinds of test items, they are 'Ratio Control Boundary Search', 'Ratio Restraint Setting Point Search', 'Harmonic Restraint Boundary Search' and 'Harmonic Restraint Setting Point Search'. 'Ratio Restraint Boundary Search' stands for that all action boundary of whole differential protection will be found out, which is the search of the whole action curve of protection; 'Ratio Restraint Setting Point Search' stands for that searching the action state of certain important point, observing whether the action of this point is correct; the search aim of 'Harmonic Restraint Boundary Search' and 'Harmonic Restraint Setting Point Search' are the same as that of 'Ratio Control Setting Value Search', which includes searching the boundary of the whole action of harmonic and the protective action of certain setting point.

- **Testing Method**

'Three-channel Current Differential' and 'Six-channel Current Differential' are available for selection. The differential testing unit can control the output of three-channel current when doing single-phase differential test, and it also can control the output of six-phase current for doing full six phases differential test on high-low voltage side. The function of three-phase current differential test is included in Tester 'Relaytestar-802' and Tester 'Relaytestar- 1000/1200', but the test of six-phase current differential only included in Tester 'Relaytestar- 1000/1200'. Six channels current can simplify the connecting and parameters setting of transformer differential test.

Attention:

1. When adopting the 'Three-phase Current Differential test', IA of tester is permanently connected with the current output end on the high voltage side of differential protective tester; IB with current input end on the low (or middle) voltage side of protection; IC will be used for compensating current. When the phase of high voltage side be adjusted, IC is used for the compensating current on high voltage side, IC is also used for low (or middle) voltage side compensating current when the phase of low (or middle) voltage side is adjusted. For detail connection, please see the appendix.

2. When 'Six Phases Differential' is selected, IA, IB and IC should be permanently connected with Current input ends A, B and C on the high voltage side and connecting settingly Ia, Ib and Ic with current input ends of non-uniform low (or middle) a, b and c three phases of protection.

3. For 'Relaytestar-802', only 'Three-Channel Differential' can be selected; for 'Relaytestar- 1000/1200 ', both 'Three-Channel Differential' and 'six phases current Differential' can be selected.

- **Way of Search**

Two ways of 'Unidirectional Approaching' and 'Bidirectional Approaching' are available for selection

Unidirectional approaching: Begin from the starting point, and search step by step from the direction of original value to the direction of final value. When it searches out certain point and the protection acts, this point is regarded as the action point. After recording this point, it will start searching for another line.

Bidirectional approaching: It is dichotomizing search. After detecting the action of starting point (in non-action area) and final point (in the action area), you can do the test by taking the middle point between two points. If it acts, replacing the end point with this point; if it does not act, replacing the starting point with this point, then, continuing to take the middle points between starting point and terminal point. Approaching like this till the value of differential between the last two testing points is in the range of 'Resolution Ration', and then we think the action boundary point is found. By using bidirectional approaching search, more accurate action boundary point will be found, and the searching speed will be quicker.

No matter which mode is selected, the starting point should usually be set in the non-action area, and the final point should be set in the action area.

Resolution: It is only effective in the mode of 'Bidirectional approaching'. The smaller the resolution is, the higher the searching precision will be, but it takes longer time.

- **Testing Time**

The longest testing time: It means the longest fault time of every step output by tester. Usually it should be set longer than setting action time of protection.

Interval: It represents the time between one fault and next fault protection output. The tester won't output any status quantity within this time.

- **Testing Equipment**

Main parameters of transformer are set on this interface.

- **Connecting Mode**

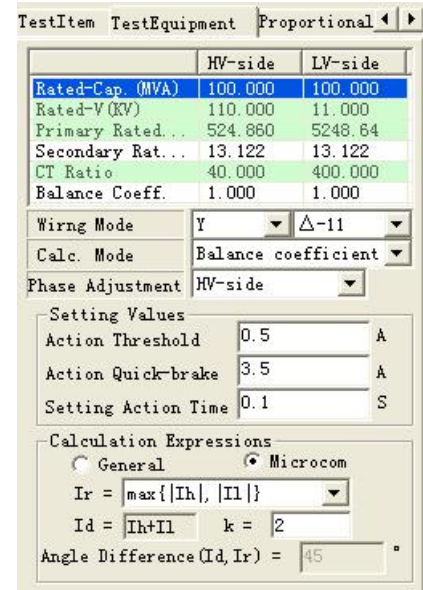
For high voltage side, Style Y and Style Y0 can be selected; for low voltage side, four kinds of connecting modes can be selected, they are Δ -11, Δ -1, Y and Y0. For three-coil transformer, you should respectively do the test by taking two sides every time. For example, 'High - Low' and 'Low-High'. Connecting mode of the parameters selected should be the same as the one of corresponding transformer

- **Setting Mode of Equilibrium Factor**

Three kinds of setting modes are available for selection: setting equilibrium factor directly, calculating by rated voltage and CT variable ratio, calculating by primary rated current and calculating by secondary rated current. The equilibrium factor has significant influence on the test, so its concrete setting mode should be done according to local condition. If the equilibrium factor of protection is given in the setting value of protection, we can select 'setting equilibrium factor directly', and input the equilibrium factor of high voltage side and low voltage side respectively. If the equilibrium factor is not given in the setting value of protection, we can select other three kinds of modes to set it. But please note that the mode of calculating equilibrium factor given in some protection instruction may be different from the setting mode of our program, we recommend that you calculate equilibrium factor firstly, and then selecting the mode of 'setting equilibrium factor directly' for directly inputting the equilibrium factor of high-low voltage side.

- **Mode of Phase Adjustment**

- 1、 When the connection type of the transformer is Y/Y, two sides possess the same phase. TA connection type is normally Y/Y. Selecting 'not adjust phase'.
- 2、 When connection type of transformer is Y/ Δ , two sides possess the different phrase, and the TA connection type of microcomputer protection is normally Y/Y. If the protection is designed to compensate by internal phase of high voltage side, selecting 'High

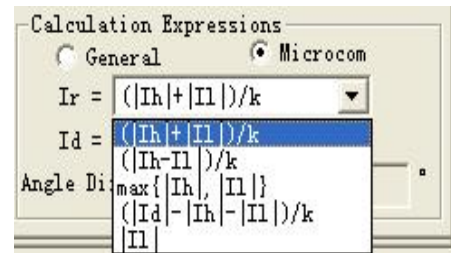


Voltage Side Phase Adjustment'; If the protection is designed to compensate by internal phase of low voltage side (such as the Type RCS-978 Protection of the Nanrui), selecting 'Low Voltage Side Phase Adjustment'. If the protection is designed for compensating by non-internal phase, it will be compensated by outside connection of TA, then selecting 'do not adjust'.

- **Ir、Id Calculating Formula**

1、 When 'General Differential' is selected, setting high side current (IA) as action current and low side current (IB) as brake current: $I_r = I_l$, $I_d = I_h$, you can set angle difference Φ (I_d 、 I_r) .

2、 When 'Microcomputer Difference' is selected, $I_d = I_h + I_l$ (vector sum of high-low side current is difference current). For I_r , many kinds of formula can be selected as the right diagram shows.



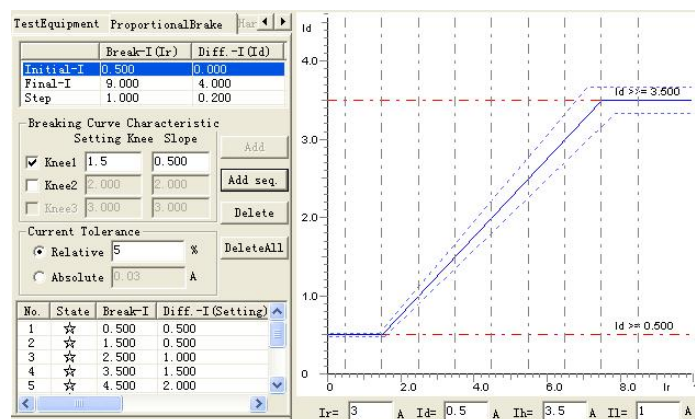
- **Proportional Restraint**

On this interface, you can set the range of characteristic search of proportional restraint and parameters of theoretical characteristic curve.

- **Searching Range**

Original value, final value and step size of brake current decide the position of search beam, and they are required to be higher than the differential current corresponding to the current of protection. If it is unknown, you can set it to be the max output current of tester in order to ensure that it can search out the whole curve .

Original value and final value of difference current determine the length of search line, which is required to be slightly smaller than threshold value of differential current, and the final value should be slightly larger than quick break value of differential current . Step size of differential current is only effective in the mode of unidirectional approaching, but



it is not effective in the mode of bidirectional approaching. Set step size of difference current according to the precision of protection. If high precision is required, the step size should be set smaller.

After completing the set of searching range, selecting 'Add Sequence' or "Add' for putting the data of search line in the testing data list. Then selecting 'start the test'. Selecting 'delete' or 'output all' for deleting all single or the whole search lines selected.

- **Definition of Characteristic Curve**

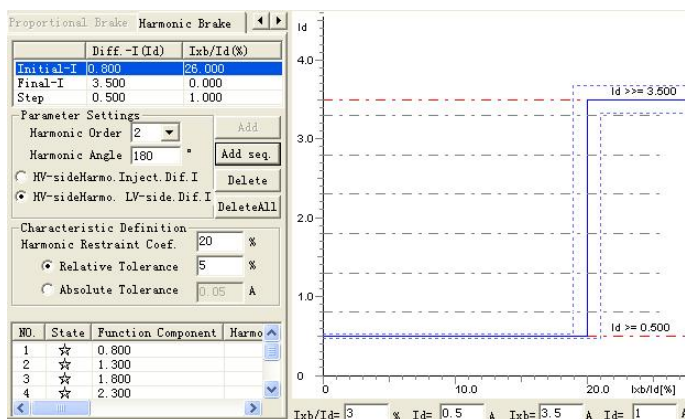
Setting brake current of all knee points and slope of all segments of broken line (proportional control factor), combining the differential current value and differential quick break current value in previous interface, it can draw theoretical control characteristic curve. Set the setting values of all knee points according to setting value of protection. If knee point value is not given by the protective setting value, you can set it by referring to action graph of protection on the protection instruction. If there are many segments of curve, several knee points should be set. We can tick the box in front of Knee 2 for setting the second knee. Then, the theoretical curve of three segments of curve can be drawn. At present, the program can only set three knee points at most, which means it can only draw 4 segments of curve at most.

■ Harmonic Restraint

On this interface, the range of characteristic search of harmonic suppression and parameters of theoretical characteristic curve can be set.

- **Range of Search**

Original value, final value and step size of differential current decide the position of search line. Original value, final value of I_{xb} / I_d decides the length of search line. Normally original value is required to be larger than setting value of harmonic controlling coefficient. Step size of I_{xb} / I_d is only effective in the



mode of 'Unidirectional Approaching', and it does not work in the mode of 'Bidirectional Approaching'. When setting parameters of the search line, the search lines should be distributed evenly between two horizontal lines, and also every search line should cover action area and non-action area. After completing the set of search range, you should select 'Add Sequence' or 'Add' for filling data of search lines in the testing data list. Selecting 'start the test' for starting the test. Selecting 'delete' or 'output all' for deleting search line.

- **Definition of Characteristic Curve**

Completing the setting of harmonic restraint coefficients, and combining difference current

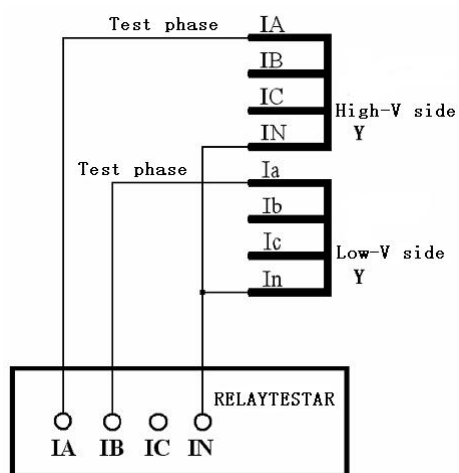
value and differential quick break current value in the previous page, the characteristic curve of theoretical harmonic restraint can be obtained

Section 2 Guidance for Test

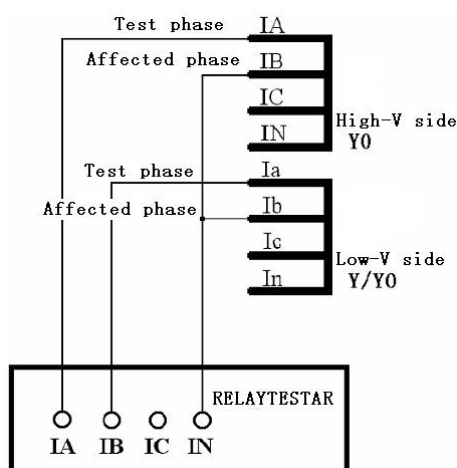
■ Connecting Mode of Six-Phase Current Difference

Connecting mode of six-phase current difference is very simple. No matter what kind of connecting mode is adopted by the transformer, the connecting modes are as following: connecting the first group three-phase Current IA, IB and IC of tester with Input terminals IA, IB and IC of high voltage side; connecting the second group of three-phase current Ia, Ib and Ic with input end Ia, Ib and Ic of low (middle) voltage side current of protection. The connecting mode is very simple.

■ Connecting Mode of Three-Phase Current Difference



1、Y (Y0) / Y (Y0) Connecting Mode:



There is phase adjustment on two side , but not zero sequence adjustment

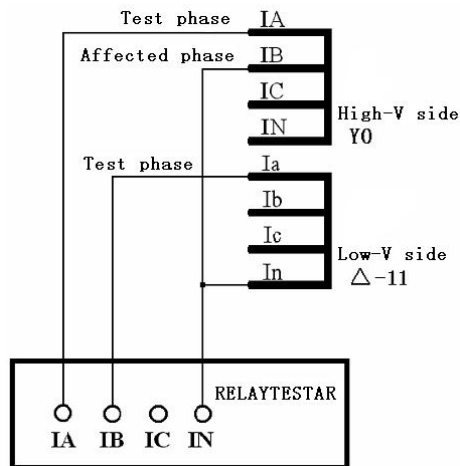
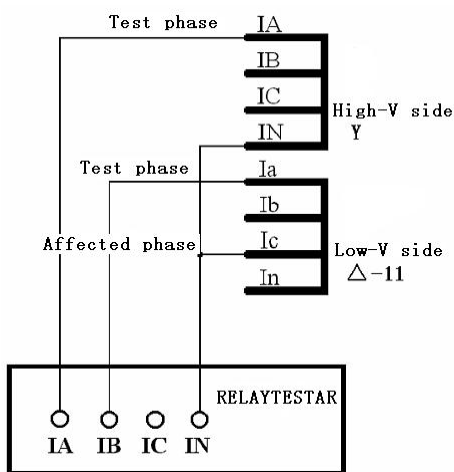
Two sides should all be connected in the mode of single phase short circuit.

circuit.

There is not phase adjustment on two sides ,but zero sequence adjustment.

For both sides, connecting testing phase with zero sequence adjusting phase in the mode of phase to phrase short

2、Y (Y0) / Δ-11Connecting Mode:



Y

side has phase adjustment, not zero sequence phase adjustment, connection in single phase mode.

$$IA' = IA - IB \quad IB' = IB - IC \quad IC' = IC - IA$$

Connecting the testing phase on Δ side with the phase

Connecting

influenced in phase to phase short circuit mode.

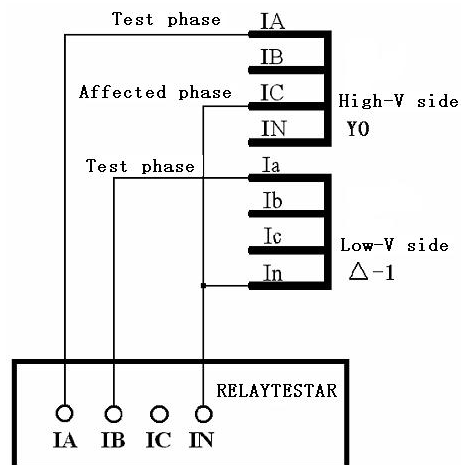
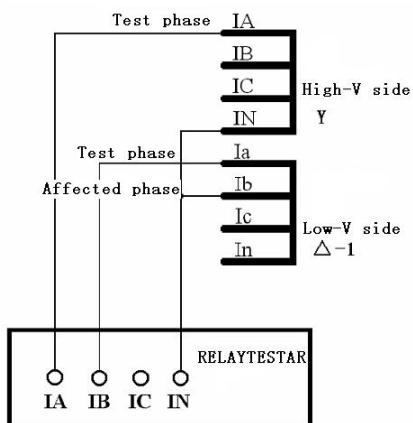
Δ side has phase adjustment, connecting in single adjustment, connection in single phase short circuit mode.

$$Ia' = Ia - Ic \quad Ib' = Ib - Ia \quad Ic' = Ic - Ib$$

Y0 side has zero sequence adjustment.

the testing phase on Y side with the phase influenced in phase to phase short circuit mode.

3、Y (Y0) / Δ -1 Connecting Mode:



Y side has phase adjustment, not zero sequence.
connecting in single phase short circuit mode.

$$I_{A'} = I_A - I_C \quad I_{B'} = I_B - I_A \quad I_{C'} = I_C - I_B$$

Connecting the testing phase on Δ side with the phase
Connecting the influenced in phase to phrase short circuit mode.
phase influenced

Δ side has phase adjustment, connecting in
single phase short circuit mode.

$$I_{a'} = I_a - I_b \quad I_{b'} = I_b - I_c \quad I_{c'} = I_c - I_a$$

Y0 side has zero sequence adjustment.
the testing phase On Side Y with the

in phase to phrase short circuit mode.

Attention:

Microcomputer differential protection is a relative complex protection, so you can't avoid coming across some problems during debugging. Generally the following points have significant influences on test result:

1、Setting equilibrium factor. Wrong equilibrium factor may lead to a large deviation between the curve tested and setting curve.

2、Selection of restraint formula. Wrong selection of restraint formula results in the testing curve and restraint coefficient calculated deviating from the setting value of protection, even completely wrong.

3、When doing the test by three-phase current, if compensating current does not be included, generally speaking ,if the first action point acts correctly, action points following it will act immediately after current is added. In this case,though the testing phase does not satisfy the condition of differential action, the differential current of compensating phase will exceed the setting value of differential action, so the protection will act quickly.

■ Instruction on parameters setting of several kinds of microcomputer's differential protection

The differential module can be tested not only by three-channel current but also by six-phase current. If you do the test by Model 802 tester, it can be done only by three-channel current. If the test is done by Model 1000/1200 , both three-channel current but also six-channel current can be employed. When three phase current is adopted, the largest output of every phase current can achieve 40A; when six-channel current is adopted, each phase current of Model 1200 can achieve 30A (the one of Model 1000 can achieve 20A)

- As for three-channel current difference, please refer to the instruction on the connection in

the chapter of ‘Differential Protection’;for six-channel current difference, connecting the first group IA, IB and IC of tester with three-phase current input terminals on high voltage side of protection; respectively connecting the second group Ia, Ib and Ic with three-phase current terminals on low (middle) voltage side of protection. When doing the test of six-channel current difference in ‘AC Test’, the phase difference and the connection type of the transformer are as the following form shown:

Connection type of Transformer	Phase of the Current on High Voltage Side	Phase of the Current on Low Voltage Side
Y/Y-12	0°	180°
Y/Δ-11	0°	210°
Y/Δ-1	0°	150°

Most of Parameters Setting Values of protection give the current value directly. For example, the value of differential threshold is 2A, the unit is A. However ,the setting values given by some protection are not current value but a coefficient. For example, the value of differential threshold is 0.3 without an unit. Actually, it is the setting value of protection given in the mode of ‘Per Unit Value’. You can convert per unit value to actual current as the following formula:
Actual current value = per unit value × rated current on high voltage side.

- Calculating method of Rated current:

$$I_{e1} = S_n / (1.732 * U_{1n} * CT1)$$

$$I_{e2} = S_n / (1.732 * U_{2n} * CT2)$$

In which:

I_{e1} 、 I_{e2} — transformer I、 II side secondary rated current

S_n — the largest rated capacity of transformer

U_{1n} 、 U_{2n} — transformer I、 II side primary rated voltage

$CT1$ 、 $CT2$ — CT ratio respectively on the primary side and on secondary side

Note : Some protections have calculation function themselves,in this case , I_{e1} 、 I_{e2} are calculated without considering 1.732 mentioned in above formula. For example, calculating I_{e1} , directly according to the formula: $I_{e1} = S_n / (1.732 * U_{1n} * CT1)$.The reason is that the equilibrium factor includes 1.732 when calculating the differential and brake current.

Take connection of transformer Y/Y/Δ-11 as example, calculating mode of each side’s equilibrium factor is as follows:

$$K1 = 1/1.732 = 0.577$$

$$K2=U2n * CT2/ (1.732 * U1n * CT1)$$

$$K2=U3n * CT3/ (U1n * CT1)$$

If setting equilibrium factor on high voltage side to be 1, and convert other sides to high voltage side, its calculation formula is as follows:

$$K1=1$$

$$K2=U2n * CT2/ (U1n * CT1)$$

$$K2=1.732 * U3n * CT3/ (U1n * CT1)$$

Calculating equilibrium factor in terms of current is as following:

$$K1=1$$

$$K2=Ie1/Ie2$$

$$K2= Ie1/Ie3$$

In which:

K1、K2、K3 — equilibrium factor on Transformer I、II、III side

Ie1、Ie2、Ie3 — secondary rated current on Transformer I、II、III side

U1n、U2n、U3n — primary rated voltage on Transformer I、II、III side

CT1、CT2、CT3 — CT transformation ratio on Transformer I、II、III side

Note :

Equilibrium factor of differential protection are not all the same, the calculating mode of some protections may not be the same as the above-mentioned one. Please refer to corresponding instruction when doing the test.

'High Voltage Side Phase Adjustment'; If the protection is designed to compensate by internal phase of low voltage side (such as the Type RCS-978 Protection of the Nanrui), s

◆ Sifang: CST-141B, -200B (High Voltage Side Phase Adjustment)

Ratio restrains formula:

Duplex winding, Y/△-11: $I_d=|I_1+I_2|$, $I_r=|I_1-I_2|/2$

Equilibrium factor: $K_1=1$, $K_2=K_{pl}$

Three- winding, Y/Y/△-11: $I_d=|I_1+I_2+I_3|$, $I_r=Max\{|I_1|、|I_2|、|I_3|\}$

Equilibrium factor: $K_1=1$, $K_2=K_{pm}$, $K_3=K_{pl}$

In which:

I1、I2、I3——The vector form in fact, which is writing with scalar form and considers the equilibrium factor, The following is the same.

Kpm、Kpl——The setting values of differential balance coefficient in the high or low

voltage side.

◆ Nanzi: PST-641 (Duplex winding transformer, Y/△-11, High Voltage Side Phase Adjustment)

Ratio restrains formula:

$$I_d=|I_1+I_2|, I_r=|I_1-I_2|/2$$

Equilibrium factor:

$$K_1=1.732, K_2=I_{e1}/I_{e2}$$

In which:

I_{e1} 、 I_{e2} ——High and low voltage side of the set values for the secondary rated current.

◆ Nanzi: PST-621/622 (Three- winding transformer, Y/Y/△-11-12, High Voltage Side Phase Adjustment)

Ratio restrains formula:

$$I_d=|I_1+I_2+I_3|, I_r=\text{Max}\{|I_1|、|I_2|、|I_3|\}$$

Equilibrium factor:

$$K_1=1.732, K_2=1.732 * U_{2n} * CT_2 / (U_{1n} * CT_1),$$

$$K_3= U_{3n} * CT_3 / (U_{1n} * CT_1)$$

◆ Nanzi: PST- (Three- winding transformer, Y/Y/△-11-12, High Voltage Side Phase Adjustment)

Ratio restrains formula:

$$I_d=|I_1+I_2+I_3|, I_r=\text{Max}\{|I_1|、|I_2|、|I_3|\}$$

Equilibrium factor:

$$K_1=1, K_2=U_{2n} * CT_2 / (U_{1n} * CT_1),$$

$$K_3= U_{3n} * CT_3 / (U_{1n} * CT_1)$$

◆ The type ISA of Nanrui (Three- winding transformer, Y/Y/△-11-12, High Voltage Side Phase Adjustment)

Ratio restrains formula:

$$I_d=|I_1+I_2+I_3|, I_r=||I_d|-|I_1|-|I_2|-|I_3||$$

Equilibrium factor:

$$K_1=1.732, K_2=1.732 * d_{35}, K_3=d_{36}$$

◆ Nanrui: RCS-9671 (Duplex winding transformer, Y/△-11, High Voltage Side Phase Adjustment)

Ratio restrains formula:

$$I_d=|I_1+I_2|, I_r=|I_1-I_2|/2$$

Equilibrium factor:

$$K1=1, K2=U2n * CT2 / (U1n * CT1)$$

◆ The type RCS-978, 985 of Nanrui (Duplex winding transformer, Y/Δ-11, Low Voltage Side Phase Adjustment, High Voltage Side zero sequence phase adjustment)

Ratio restrains formula:

$$Id=|I1+I2|, Ir=Max\{|I1|, |I2|\}$$

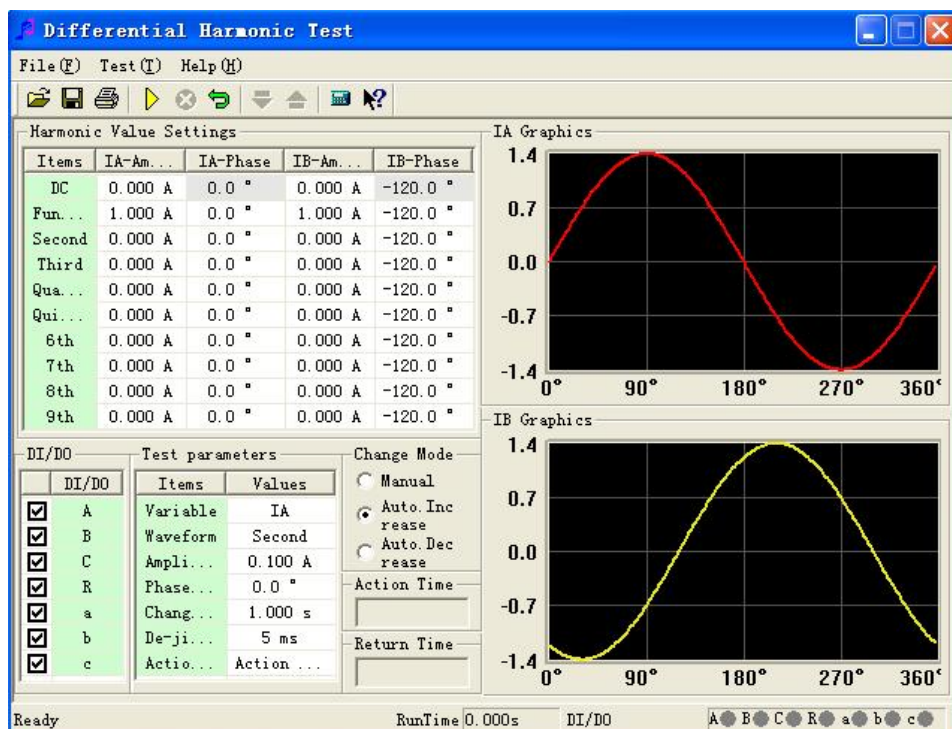
Equilibrium factor:

$$K1=1, K2=Ie1/Ie2=U2n * CT2 / (U1n * CT1)$$

Chapter 16 Differential Harmonic

This module is intended for testing the characteristic of harmonic control of differential protection, and it also can be used for testing other harmonic protections. It can test not only differential relay but also the differential protection of microcomputer. It outputs the differential current of harmonic superposition not only in one channel, but also in two channels by pressing the mode of 'one side differential current, another side harmonic'. It can output 9th harmonic at most, which satisfying basically the requirements of normal harmonic tests.

- Style of software interface is similar with the one of 'AC Test' for simply operation of test.
- It can arbitrarily superposition component of 9th harmonic at most, and the amplitude value or phase of every harmonic can be set arbitrarily.
- It can directly amend amplitude value, phase and step size of verification of current in the testing state of not stopping the output, or change phase of variable.
- You can select arbitrarily the varatioal mode of variable in hand movement or automatic increase and reduce for controlling flexibly.
- Displaying real-time waveform of two-way superposition in graph form so as to observe the testing process directly.



Section 1 Interface Instruction

■ Setting Parameter

Before doing the test, you should set original values of every channel on the interface. The component of needless harmonic should be set as 0. There will be output definitely in the channels whose values are in the interface. So, If you do not hope any output happened in certain channel, you should set all amplitude value of every waveform to be 0, or do not connecting with this channel.

When doing normal tests, phases of fundamental wave and harmonic are synclastic, such as all being set as 0° . It is can also set as reverse. This phase decides initiative angle of this waveform output by the tester when test is started. If initiative angles of all waveforms superpositioned are different or reverse, which may influence the test.

When doing the test in the mode of differential harmonic control, it can not only output harmonic by IA to high voltage side of protection, and outputting fundamental wave by IB to low voltage side of protection, but also outputting by reversing IA and IB, which won't influence normal testing.

■ Variable Option

Software only allows selecting one channel of IA and IB as variable. Select the channel at first, then, select certain harmonic component of this channel in pull-down menu below as variable. Which means only certain waveform component of one current (IA or IB) channel will vary during the test, and others are all 'constant'.

If you need to reset variable without stopping output during the test, you can select the mode of 'Hand Movement' in the column of vary modes, most of parameters on the interface can be amended at that time. After completing the amendment, data can be read in by pressing the 'confirmation' key on small keyboard on the tester or the 'enter' key on notebook computer. After that, the tester will output according to new data. The tester can also read in new data through switching current mode of 'HM test' to other automatic modes by the mouse. The effect is the same.

■ Action Mode

The following two kinds of modes are only effective to variational modes of 'automatically increase' or 'automatically reduce'.

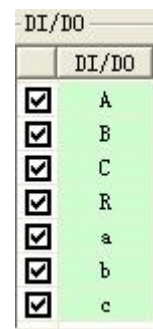
Action Stop If this mode is selected, the tester will stop test as soon as receiving action

signals of protection. This mode can only test actional value of protection. If you do the relay test, the 'flutter-proof time' should be set as 20ms or above for reducing the influence on test caused by 'flutter' of relay.

Action return When this mode is selected, supposing current variable varies according to the mode of 'automatically increase', the tester will transfer direction automatically to the mode of 'automatically reduce' as soon as it receives actional signals of protection. This mode not only can test the action value of protection but also can test automatically the return value. If doing relay test, you should also set 'flutter-proof time' to be 20ms and above.

■ Input Option & Action Display

All seven inputs on the default interface of software can be selected together, which are all effective. If you need to cancel the influence of certain input on the action signals of protection, you can cancel this option by mouse before the test.



Section 2 Test Guidance

■ Setting Parameter

- When doing the characteristic test of harmonic control of transformer, it can be loaded not only on high voltage side but also on low voltage side if single-phase current is selected for outputting differential current of harmonic superposition. When outputting it by adopting two-phase current synchronously, it loads the harmonic output by IA on high voltage side, and loading the fundamental wave output by IB on low voltage side. On the contrary, it can load fundamental wave on high voltage side by IA, and loading harmonic output by IB on low voltage side.
- For testing mode, you can fix fundamental wave, and adjusting harmonic from large to small in step size (harmonic should be set as variable at that time); or fixing the harmonic, and adjusting the fundamental wave from small to large in step size (fundamental wave should be set as variable at tht time). The testing effects are basically the same.

■ Testing Mode

Before the test, you can amend the connecting mode of transformer of differential protection to be Y (Y₀) / Y, and setting equilibrium factor of low (middle) vltge side to be 1, which will simplify the test. When doing the test, no matter only loading current on high voltage side or loading current on high and low voltage sides at the same time, its principle is as follows:

1、 Component of fundamental wave output must be larger than the action threshold current set by protection;

2、 Output initial harmonic content must be protected by reliable lock-out, which means it must be larger than the coefficient of harmonic control set by the protection.

If the connecting type of transformer of differential protection is Y (Y₀) / Δ, and the equilibrium factor of high and low voltage side are all not 1, how to test the ratio control coefficient of protection under the condition of not amending settings?

- **Outputting in the state of ‘differential current of harmonic superposition on high voltage side’**

Since component of harmonic and component of fundamental wave are all added on high voltage side, component of two kinds of waveforms influenced by equilibrium factor of high voltage are the same, they will be counteracted mutually. So its testing mode is as same as the statement of above paragraph. Please refer to it.

- **Outputting in the state of ‘harmonic on high voltage side, differential current on low voltage side’**

You must consider respectively the equilibrium factor of high and low voltage sides.

For being convenient to explanation, we hereby suppose the equilibrium factor of high and low voltage sides are respectively K_h and K_l, differential threshold value is I_{d0}, and harmonic control coefficient is K_{xb}, then:

a) The output component of fundamental wave (suppose it is output by I_B) must be larger than I_{d0} / K_l;

b) The output initial harmonic content (suppose it is output by I_A) must be larger than I_{d0} * K_{xb} * K_h.

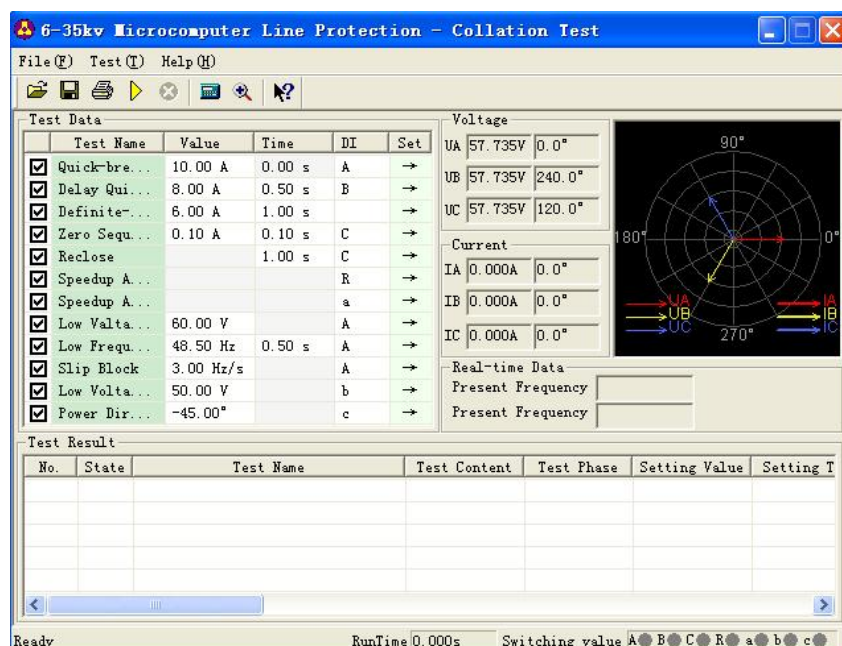
Start the test, and reduce harmonic in step size till differential action acts. Suppose the harmonic current and fundamental wave current output by tester is respectively I_{A1} and I_{B1} at that time, then the formula of computing the coefficient of harmonic control:

$$K_{xb} = I_{xb} / I_{jb} = (I_{A1} / K_h) / (I_{B1} * K_l)$$

Chapter 17 Comprehensive Test of Line Protection of 6-35 KV Microcomputer

This testing module concentrates most parts of test items of microcomputer line protection of low voltage, which is suitable for testing line protection of insulated system on 6~35KV neutral point. In whole testing process, we select the testing mode of 'Two Way Approaching' mostly, which enhance work efficiency of test.

- After all wires are connected, it can test completely all items in one time without human intervention.
- You need not to recede from other segments, just verifying settings of three segments of overcurrent protection in one time.
- Whole module adopts the testing mode of 'Two Way Approaching' mostly, which saves time and enhances test's effective.
- Gathering almost all kinds of testing functions of line protection of central point insulated system.
- Simple and clear interface. You only need to set a small quantity of testing coefficients. Some of them only need to input settings.
- In the test item of 'Power Direction', it blurs the positive and negative concepts of 'Sensitive Angle' on purpose. It can do the test correctly by inputting positive angle or negative angle.



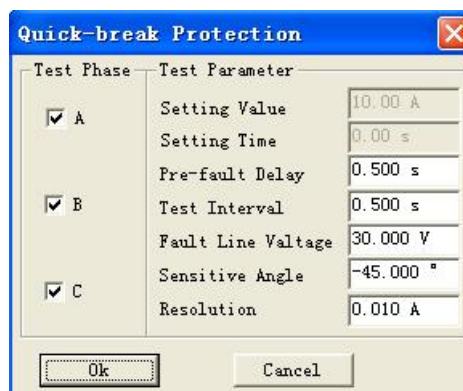
Section 1 Interface Instruction

■ Triple-segment type overcurrent protection: quick break, time delay quick break and time overcurrent limiting

These items are used specially for testing triple segments of overcurrent protection. After inputting correctly all segments of settings (including action value and action time) according to settings list, you can do one test without receding other segments.

When doing the test, select respectively the test item needs to be test, and set 'settings' and 'setting time' of all segments of actions. Then, click the '→' button by mouse

After that, set other testing parameter in a dialog box ejected. We hereby take 'quick break protection' as the example for detail explanation. See the right diagram:



Attention:

The 'settings' and 'setting time' required for output on the interface must be filled correctly according to actual settings set, otherwise, it may influence the result, and may even lead to unsuccessful test.

• Test Phase

The test is done through loading current on split phase, so Phase A, B and C is available for option. You can select single phase or several phases synchronously for testing, the software will do the test in sequence. When doing certain phase test, only this phase current has output, but other phase current is zero.

• Fault Line Voltage

For the protection have the function of 'low voltage lockout', triple current needs to be loaded. Only when line voltage is smaller than the settings of low voltage, it open overcurrent protection; otherwise, it will close down for protection, and it won't act even the current is very large. In this situation, it is required that this parameter should be smaller than the settings 'low voltage lockout' of protection. No matter you test which phase during the test, triple phase all has output, and UBA, UBC and UCA are all equal to setting fault line voltage.

Voltage		
UA	57.735V	0.0°
UB	57.735V	240.0°
UC	57.735V	120.0°
Current		
IA	0.000A	0.0°
IB	0.000A	0.0°
IC	0.000A	0.0°

During the test, you can observe clearly the amplitude value of current and phase output by current voltage and current channel from software's interface. When doing the test of low circle unloading item, you can also supervise frequency of output voltage as the right diagram shows:

- **Sensitive Angle**

Sensitive angle of power direction. For inputting power directional element, you should set correctly sensitive angle. Normally just do it according to default value.

- **Resolution**

This parameter decides precision of testing value. 0.01 resolution defaulted already can meet normal testing requirements of microcomputer's protection.

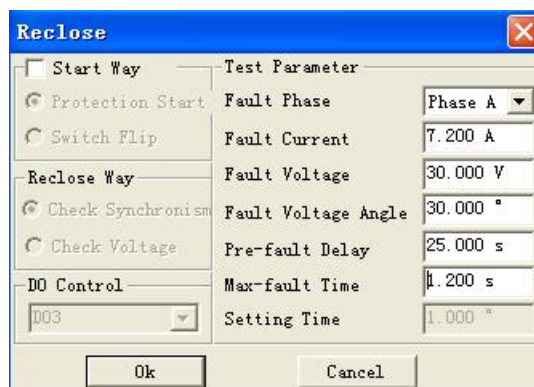
■ Zero Sequence Current Protection

The zero sequence current of lines of small earthing system is larger, so the protection also has functions of zero sequence current trip or alarming.

Setting mode of testing parameters on the interface is similar to the one of above-mentioned triple overcurrent. Please refer to it. The difference is: 'column of 'test phase' in the dialog box ejected is not opened. Since the protection only has individual phase zero sequence, zero sequence current is output settingly by IA phase of tester for doing the test. When doing the test, connect IA of tester with input end of zero sequence current of protection regarding as zero sequence current of protection.

■ Reclosing

This item is used for simulating action of triple phase primary automatic reclosing. Before the test, you must input the function of reclosing of protection firstly. During the test, set a fault current for making certain segment of overcurrent protection to act reliably. Tester will transfer to normal state for outputting at once. It will wait for success of coincidence within the time slightly longer than 'setting time reclosing'.



Attention: When switch is closed by hand or after reclosing acts, the reclosing discharges at once. The reclosing is in the locking state before fully charging again. Any faults will only trip without coinciding at that time. Charging time of reclosing is normally between 15s-25s. Parameters are as the right diagram shows:

The 'setting time' required by interface stands for the time of reclosing set by protection.

- **Fault Current, Fault Voltage and the Largest Fault Time**

Setting parameter of fault state before the protection coincides. This fault current and voltage should ensure reliable action of protection. 'Fault Current' is normally larger than certain segment of overcurrent setting value, and 'the Largest Fault Time' should be longer than the setting time of Period III, 0.2 or above, of overcurrent.

- **Time Delay before Fault**

If the reclosing does not charge fully, this parameter normally should be set between 15~25s so as to waiting for completely charging of reclosing. If the reclosing has charged fully before the test, this time can be set shorter in order to save testing time.

Attention:

Some protections require the switch to start reclosing only when it is on the switch-on position, which means it loads electric potential on the switching position end of protection for judging where the switch should be closed. During whole testing process, the Output 2 of tester outputs by simulating position of switch. It will open 2 closures in the state of 'before fault' and 'after coincidence', and will open 2 switch- off in the state of trip. So you can connect 'Output 2' with corresponding DC circuit in series for making the protection to distinguish switch's position correctly.

■ Acceleration after Time Delay Quick break & Acceleration after Overcurrent

These items are used for testing the process of trip of after-acceleration after the operation of reclosing in the state of permanent fault. When doing the test, tester will output again the same fault quantity as previous time after receiving action signals of reclosing of protection in order to wait for retrip of protection and testing of time of after-accelerated trip.

For doing the test, the following conditions need to be prepared:

- 1、 Fault current, voltage, sensitive angle and fault time set in parameters should ensure correct action of the segment of overcurrent tested. (Please refer to relevant instruction to overcurrent protection of previous paragraph);
- 2、 Providing protective functions of 'Acceleration After Time Delay Quick break' or 'Acceleration after Overcurrent' corresponding to this overcurrent segment;
- 3、 Providing the function of reclosing (please refer to relevant instruction to reclosing of previous paragraph);
- 4、 The protection of reclosing is started only when receiving signal of switching position. You should put in the contact signals of Output 2 correctly.

■ Low Voltage Latching Overcurrent

This item is used for testing the latching voltage value of protection of low voltage latching overcurrent, and this value is the line voltage value. You should put in the function of 'Low Voltage Latching' of protection of the segment of overcurrent waiting for test.

This item also does the test in three-phase successively. For example, when testing UAB, two phases of A and B are fault phases, Phase C is normal voltage, and UAB is fault voltage. No matter testing phase selects UAB, UBC or UCA, three-phase current all output current synchronously during the test. Amplitude values of three-phase current are all equal to the setting 'Fault Current', and they will be output in positive sequence phase

Test Phase	Test Parameter	Value
<input checked="" type="checkbox"/> UAB	Setting Value	60.00 V
	Setting Time	
<input checked="" type="checkbox"/> UBC	Pre-fault Delay	0.500 s
	Max-fault Time	1.200 s
<input checked="" type="checkbox"/> UCA	Fault Current	7.200 A
	Sensitive Angle	0.000 °
	Resolution	0.010 V

'Fault Current' and 'The Largest Fault Time' should be all respectively larger than corresponding setting value of the segment of overcurrent waiting for test. Please see the right diagram for reference.

For setting other parameters, please refer to relevant instruction to 'Triple Segments Type Overcurrent Protection' of previous paragraph.

■ Low Frequency Protection

This item is used for testing action frequency and action time of low or high frequency protection. Please see the right diagram for setting parameters.

- **Time Delay before Slip of Frequency**

Output firstly the voltage-current in initial frequency before doing the test every time. It can unlock low frequency protection through adopting 'Time Delay before Slip of Frequency', then, it begins to slip the

Test Parameter	Value
Delay Before Frequency Fall	5.000 s
Test Interval	0.500 s
Original Line Voltage	100.000 V
Voltage Angle	0.000 °
Three-phase Current	0.000 A
Initial Frequency	60.000 Hz
Final Frequency	45.000 Hz
df/dt	0.200 Hz/s
Setting Value	48.50 Hz
Setting Time	0.50 s

frequency. This time parameter is used for unlock frequency by protection.

- **Initial Line Voltage and Three-phase Current**

Some protections have the function of 'Low Voltage Locks Low Frequency', so 'Initial Line Voltage' should be larger than 'Latching Voltage' of protection. You can normally set it to be 100V defaulted.

Some protections require load current to open the function of low frequency. If there are not current or current is too small, the protection considers that it is no need to cut load, and then it will lock the low frequency function. So you should connect current testing lines in advance, then setting 'Three-phase Current' to be larger than 'Setting Value of Current' of protection. When doing the test, three-phase voltage and three-phase current will output at the same time, and it will change frequency synchronously.

- **Initial Frequency & End Frequency**

The basic principle of setting parameters is: Protection should not act reliably in initial frequency; protection should act reliably in end frequency.

For the protection having 'starting frequency', it is required that initial frequency must be larger than the value of 'starting frequency' of protection. 'Initial frequency' is normally set as 50Hz.

Normally end frequency should be at least 0.5Hz smaller than setting action frequency, but it also can't be set too small, otherwise protection may be locked. It should normally not lower than 45Hz.

- **Percentage Change df/dt of Frequency**

During the test, protection slips uniformly in setting df/dt at first. When it slips to the position of 'Setting Action Frequency + 0.1Hz', tester will change it to converse frequency measure by measure in the rate of '0.01Hz/ each step time' till protection acts. The action frequency and action time will be measured. Here 'each step time' is equal to 'Setting time+0.2s'.

■ Slip Latching

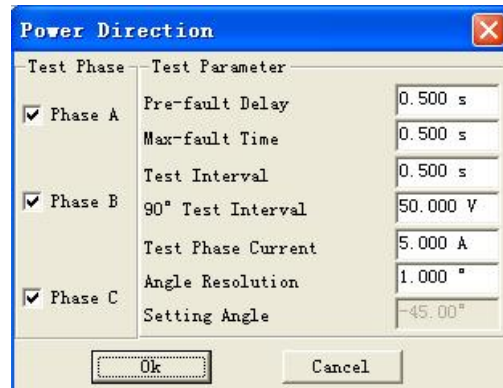
When frequency slips too quickly and df/dt is larger than the setting value of slip latching of protection, the protection will be locked without action; when df/dt is smaller than the setting value of slip latching, the protection will unlock it for allowing operation. If the protection is in the latching state originally, certain times will be needed for unlocking it from locking, so the 'Time Delay before Slip of Frequency' should be set enough large such as 5s. Meanwhile, low frequency has certain action delay, so end frequency should be set smaller than the action frequency set by protection such as 47Hz. Otherwise it may not act due to lack of sliding time. For the meanings and setting modes of parameters, please refer to the 'Low Frequency Protection mentioned in previous paragraph.

■ Low Voltage Latching Low Frequency

Different from the above-mentioned 'Slip Latching', here the low frequency protection locks when line voltage is lower than the latching voltage value set by protection. For modes of setting parameters, please refer to instructions to 'Low Frequency Protection' and 'Slip Latching' in previous paragraph.

■ Power Direction

Through this item, you can measure two boundaries of protection of power direction correctly and quickly, recording boundary angle and working out automatically the largest sensitive angle. Considering that differentiating positive pole from negative pole of the largest sensitive angle is difficult for some users on the spot, the technology for blurring output of setting



value of the largest sensitive angle has been used in the software. Suppose the largest sensitive angle of protection is -45° , no matter users input -45° or $+45^\circ$, there are not any influence on normal test. The right diagram shows the dialog box for setting parameters.

In this item, tests are also done in three-phase successively. You can select single phase or all phases synchronously to be test phases. When testing certain phase, only this phase outputs current, and current of other phases is zero.

- **Off-hours of Test**

For meeting the testing requirements of certain protections needs to be started by 'Mutation Start', we hereby set this parameter. When it is a non-zero value, basic process of test is: output voltage and current in normal state (voltage is the rated value, current is 0), maintain them till 'Time Delay before Fault' ends—output preset voltage and current in the state of fault, maintain them till 'The Largest Fault Time' ends —stop outputting till the 'Off-hours of Test' ends—— output again voltage and current in normal state, maintain them till 'Time Delay before Fault' ends—— output mutatedly the fault voltage and current in another state till 'The Largest Fault Time' ends—— stop outputting till 'Off-hours of Test' ends. Outputting circulatedly like this till it tests a actional boundary of protection.

- **Line Voltage of 90° Connection**

This software can only test protection of the power direction connected in the mode of 90° . When testing Phase A, Only IA can output current, and current of other phases is zero; only UB

and UC output voltage, and voltage of other phases is zero. In addition, amplitude value of Current IA is equal to setting 'Test Phase Current', amplitude value of line voltage UBC is equal to setting 'Line Voltage of 90°connection'.

- **Resolution of Angle**

This parameter decides the precision of test. When the software finds the angle difference value of current output two times is smaller than 'Resolution of Angle', it will automatically stop outputting and end the test. We normally set it as default value ,1°.

Chapter 18 Fault Review

Fault review is used for putting the data documents of current-voltage waveforms compiled in Data Format ANSI/IEEE C37.111-1991COMTRADE that is recorded by data recording equipment like fault waveform recorder in the tester, and its waveforms will be reviewed by tester for testing equipment like protection tester.

Each standard recording document consists of three kinds of documents. They are respectively pilot, configuration and data document. Names of these three kinds of documents are the same, which can be differed by different suffix names that are respectively .HDR, .CFG and .DAT. The review test can't be done unless three documents are complete.

Before the test, please open certain recording document at first. Recording document can be laid in any subentry that can be found in the dialog box of 'open the document'. The program will list all documents whose suffix name is .CFG after finding the subentry. After selecting certain document, the program will transfer automatically the .CFG and .DAT documents of this name, and display all voltage-current waveforms and name of channel on the screen. In addition, you can also check document's attribute, waveform discretion sampling point, etc. through the buttons in tool column.

Press the 'Test' key to enter a dialog of several pages testing options:

Page 1: Select wave recording voltage and current line needs to be tested. You can select in the mode of whole group of voltage, whole circuit of current, and also can select separately and independently three-phase voltage or three-phase current.

Page 2: Selecting the wave recording segment of time, starting-end points, needs to be reappeared. Basic unit of time point is according to numbers of waveform sampling point. You can input data on time point, and also can increase or reduce it by pressing the '↑' key and '↓' key on keyboard.

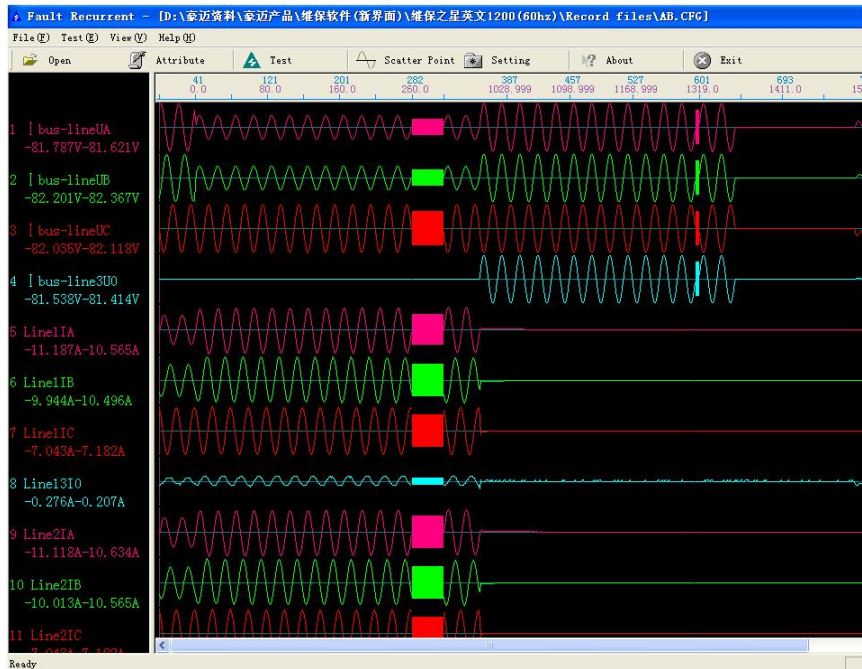
Page 3: Outputting it in original ratio or outputting it after the change of PT and CT in transformation ratio. When outputting in transformation ratio, you should divide the data by this transformation ratio value. In addition, if data of certain phase needs to output after 180° reverse phase, you can set the transformation ratio to be a negative number such as '-1/1', then this phase will be output in original anti-phase ratio.

Page 4: Transmit automatically all selected data to the lower machine for waiting for reappearance output.

Page 5: Do the reappearance test officially. The 'upper button' on this page makes the tester to output circularly the first periodical waveform, and waiting for your pressing of 'lower button'; press the 'lower button', the tester will output all recording waveforms till the end point of reappearance time segment for reappearing whole process. You can also don't press 'up key' but press directly 'down key', it will reappear completely all waveforms from starting time segment to end time segment in one time.

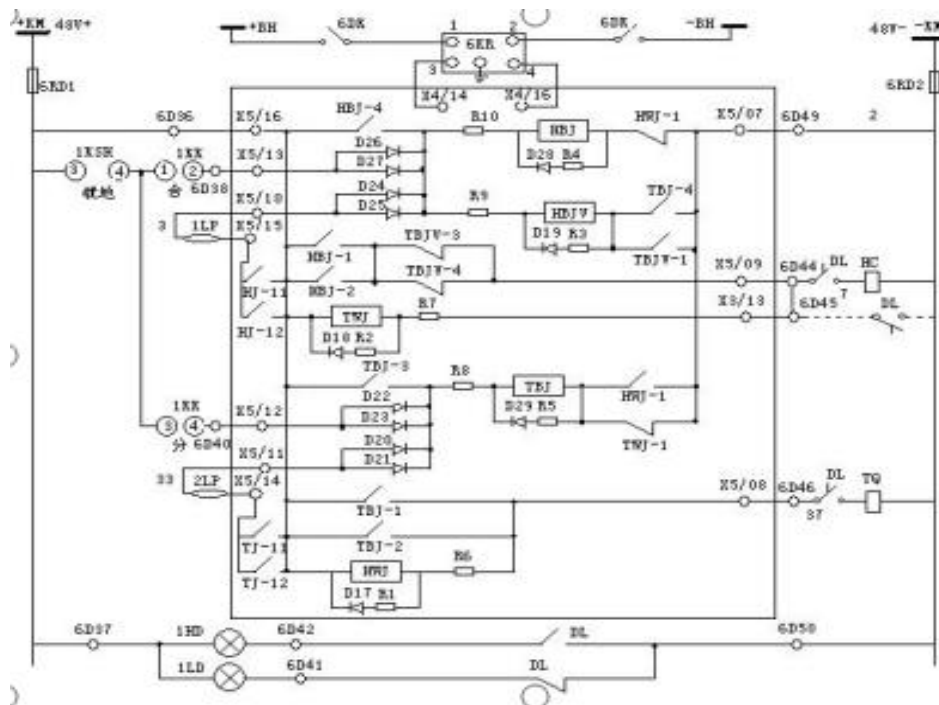
After ending the test, computer will file the testing result in the subentry of 'test report\fault

reappearance' in text format, and it can be displayed or printed by pressing the 'print' key. You can also copy it to be compiled or amended by compiling tools like WORD.



Appendix 1: Example of wiring method for line protection test

During the microcomputer protection test, various types of microcomputer protection are encountered. The internal structure of various protective devices or the terminals on the rear panel of the device often have large or small differences. Therefore, it is often difficult to test the wiring on site, especially to find the output terminal of the protection device (tripping A, tripping B, tripping C, reclosing, etc.). The following is a brief analysis of the field wiring, especially the output wiring method, based on the secondary wiring diagram of a set of protective devices in an electric power bureau. As shown in the figure below:



+KM → X5/16 → TBJ-1 (TBJ-2) → X5/08 → TQ coil → - KM

Thus, the tripping coil TQ of the circuit breaker is started to realize manual tripping.

(2) Fault trip

The CT secondary three-phase current is connected to the three-phase current contact of the protection, that is, the protection tripping coil corresponding to TJ-11 and TJ-12 in the figure (not shown in the figure). In case of fault, TJ-11 and TJ-12 contacts are closed, so the tripping process in case of fault is as follows:

+KM → X5/16 → TJ-11 (TJ-12) → X5/14 → 2LP → X5/11 → TBJ coil → HWJ-1 (TWJ-1) → X5/07 → - KM;

In this way, the TBJ coil is started, and the two normally open auxiliary contacts TBJ-1 and TBJ-2 of TBJ are closed

+KM → X5/16 → TBJ-1 (TBJ-2) → X5/08 → TQ coil → - KM.

Thus, the circuit breaker tripping coil TQ is started to realize fault tripping.

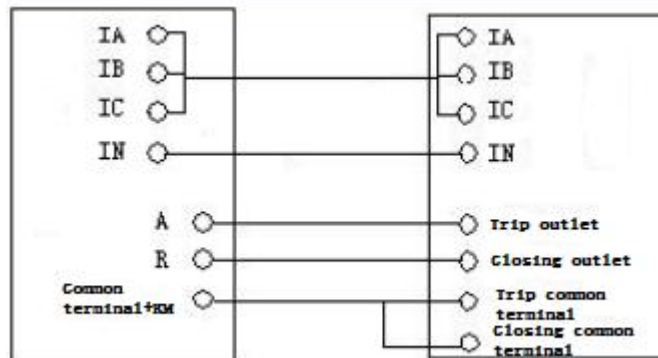
(3) Manual closing and automatic reclosing:

The process of manual closing and automatic reclosing is similar to the above tripping process, which will not be described here.

(4) Wiring method:

After understanding the tripping and closing process in the above figure, it is very easy to start the test. The wiring method is as follows:

The three-phase current output terminals IA, IB and IC of the tester are respectively connected to the three-phase current input terminals of the protection;



The input common terminal+KM of the tester is connected to the X5/16 contact of the positive power input terminal of the protection, the tripping input terminal of the tester is connected to the tripping outlet terminal X5/14 of the protection, and the closing input terminal of the tester is connected to the closing outlet terminal X5/15 of the protection. In fact, it is connected to both ends of protective tripping contacts TJ-11 and TJ-12 and closing contacts HJ-11 and HJ-12. Please refer to the figure on the right:

(5) Precautions

The input common terminal+KM of the tester must be connected to the positive power supply for protection;

During the test, the protective DC working power supply shall be put into operation. If DC power supply is not available on site, consider using the DC power supply belt on the back panel of the tester for protection, but pay attention to whether the rated DC input for protection is 110V or 220V, and use a multimeter to measure and adjust the DC of the back panel of the tester accurately.

During the test, the protection should exit the normal operation, disconnect the original CT and PT wiring, open the protection tripping and closing pressing plates (i.e. disconnect 1LP and 2LP in the figure above), and absolutely avoid tripping the lines in normal operation

during the protection test;

When conducting reclosure and post acceleration trip tests, some protections adopt the method of starting reclosure and post acceleration in the wrong position. At this time, if the tripping and closing circuit is disconnected, the reclosure or post acceleration of the protection will not be started. At this time, the tripping and closing can be put into operation, or the simulation circuit breaker can be used to replace the real tripping and closing switch for testing.

(6) Supplementary content

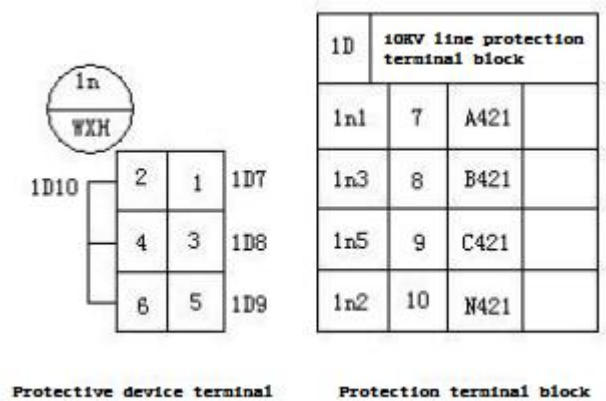
During the field test, because the protection device is installed on the protection screen, it is not convenient to lead the terminal directly from the protection device, but from the terminal strip of the protection screen. Therefore, when looking at the field protection installation wiring diagram, there is a problem of identifying the corresponding contact between the protection device and the contact on the protection terminal block. This problem is briefly described as follows in the form of an example. As shown in the figure above:

First find the corresponding terminal part of the protective device to be tested in the terminal strip. In the above figure, the left side is the local terminal diagram on the protection device, and the right side is the corresponding local terminal diagram on the protection screen terminal strip;

The left contact of the terminal block of the protection screen is to the protection device, and the right contact is the incoming and outgoing line connected with the equipment outside the protection screen;

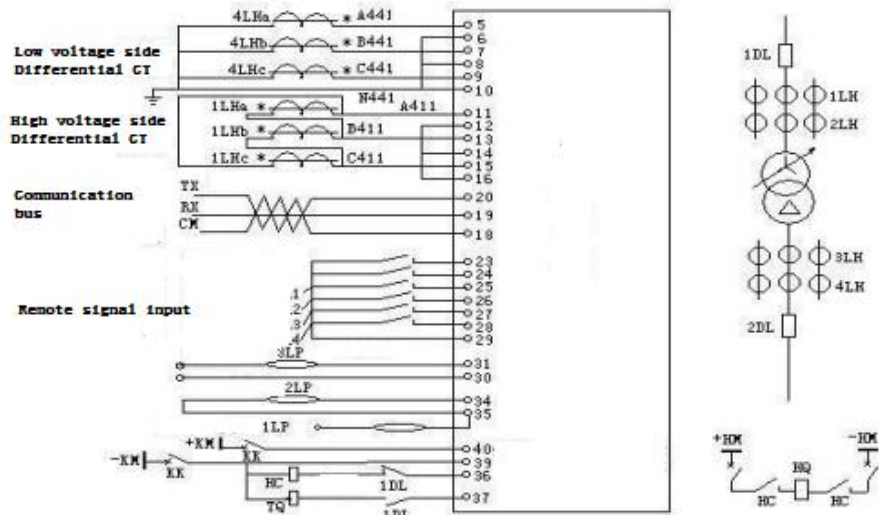
Their corresponding rules are: the terminal serial number of the protection device, such as 1, 3, 5, 2, etc., corresponds to 1n1, 1n3, 1n5, 1n2, etc. on the left side of the screen terminal sequence number. In fact, the serial numbers of the panel terminal strip, such as 7, 8, 9, 10, etc., also correspond to 1D7, 1D8, 1D9, 1D10, etc. on the right side of the terminal serial number of the protection device;

It is worth noting that the name annotation of each terminal on the rear panel of the protection device can only serve as a reference. To find the auxiliary contact of the tripping coil of the protection device, it is more reliable to carefully look for the secondary wiring diagram of the protection device.



Appendix 2: Example of Differential Protection Test Wiring Method

The wiring diagram in Appendix 2 shows the logic structure diagram of the control loop inside the protection device, but the logic structure diagram is not shown in the wiring drawings of many devices. This brings some trouble to the wiring during the field test, especially to finding the corresponding terminal of the input value. In fact it is also very simple to



Note: The large wire frame represents the internal circuit of the microcomputer device

master the wiring rules. The principle wiring diagram of a differential protection device is taken as an example for analysis. See the right figure:

(1) Device terminal table:

Terminal	Terminal description
5	1 # differential CT current A into
6	1 # differential CT current A out
7	1 # differential CT current B into
8	1 # differential CT current B out
9	1 # differential CT current C into
10	1 # differential CT current C out of
11	2 # differential CT current A into
12	2 # differential CT current A out of
13	2 # differential CT current B into
14	2 # differential CT current B out
15	2 # differential CT current C into
16	2 # differential CT current C out
18	downlink communication GND
19	downstream communication RX
20	downlink communication TX
23	main transformer local weight gas remote signal
24	# main transformer body light gas remote signal
25	remote signal input 1
26	remote signal input 2
27	remote signal input 3
28	remote
29	remote
30	intertrip
31	intertrip
34	protection action relay outlet
35	connected to manual tripping circuit
36	connected to breaker closing circuit
37	connected to breaker tripping circuit
39	power supply
40	power supply

positive pole

(2) General wiring

Relay protection tester is used. IA, IB and IC are respectively connected to terminals 11, 13 and 15 on the high-voltage side. Short circuit terminals 12, 14 and 16, and then connect them to IN of the tester; The tester Ia, Ib and Ic are respectively connected to terminals 5, 7 and 9 at the low voltage side. Short circuit terminals 6, 8 and 10, and then connect them to In of the tester. The 40 and 39 terminals are respectively connected to the positive and negative electrodes of the DC power supply.

(3) Input wiring

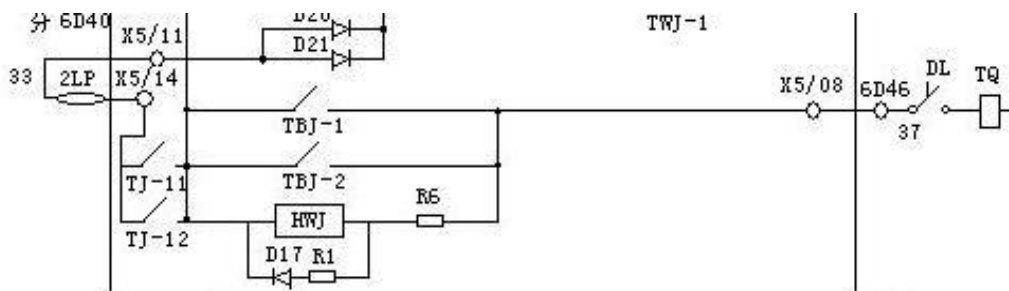
Wiring error:

Terminals 37 and 36 in the figure are easily mistaken as auxiliary contacts of tripping and closing coils of the protection device, so the input A of the tester is connected to 37 and the input R is connected to 36. In fact, these two terminals are tripping and closing outlets to protect the field circuit breaker. TQ and HC in the figure are the tripping and closing coils of the circuit breaker, not the tripping and closing coils inside the protection device. 1DL in the figure is also the auxiliary contact of the circuit breaker, not the auxiliary contact of the tripping and closing coils inside the protection device.

Of course, this connection method can also be tested, but it requires the closing and opening operation of the circuit breaker when participating in the test, which will affect the service life of the circuit breaker. At the same time, it also requires a line outage, otherwise it will cause a major accident of line false outage. Therefore, we do not advocate such wiring methods!

Wiring analysis:

By careful comparison with the device terminal table and the wiring diagram in "Appendix 1", it can be found that terminal 34 is the "protection action relay outlet", and "differential tripping 2LP" is next to terminal 34, that is, the hard strap for differential protection tripping. Therefore, this is the outlet terminal of the auxiliary contact of the tripping coil inside the protection device. It is equivalent to X5/14 contact in the example diagram of "Appendix 1". As shown in the figure below (only part of the example in Appendix 1 is selected):



According to the above figure, we are returning to the content mentioned in the "wiring error" above. The TQ just mentioned is equivalent to the TQ in the above figure; The 1DL just mentioned is equivalent to the DL in the above figure; The 37 terminal just mentioned is equivalent to X5/08 contact in the figure above. So it is not correct.

The correct wiring method is to try every means to find the outgoing terminals of TJ-11 and TJ-12 contacts in the above figure. Through analysis and comparison, it is determined that terminal 34 is the required terminal.

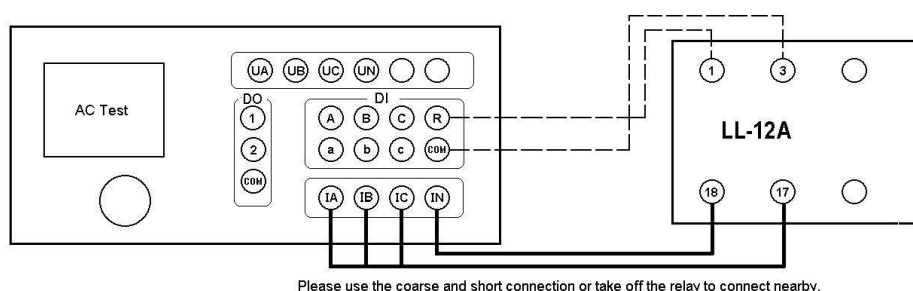
Correct wiring:

The input A of the tester is connected to terminal 34, and the input common terminal COM (or+KM) is connected to the positive terminal 40 of the DC power supply. In order to prevent the misoperation of the field circuit breaker caused by the operation of the protective device during the test, please open the hard strap at the protection tripping outlet during the test. As shown in this example, the pressing plate of "differential tripping 2LP" should be opened.

Appendix 3: Test Methods for Various Relays

1. AC Voltage / Current / Inverse Current Relay Calibration

In AC test, U_a (or U_{ab})/ I_a is set to an initial value, and set step, then press the key of “▲”, “▼” or rotated button to increase or decrease the voltage/current, which also can be realized by the method of automatic test. The action value, return values, action time and the return time of voltage / current / inverse current relay can be measured, and the return coefficient can be calculated. As below, it is the wiring diagram of LL-12A overcurrent relay.



2. DC Voltage / Current Relay Calibration

In DC test, U_a (or U_{ab})/ I_a is set to an initial value, and set step, then press the key of “▲”, “▼” or rotated button to increase or decrease the voltage/current, which also can be realized by the method of automatic test. The action value, return values, action time and the return time of voltage / current relay can be measured, and the return coefficient can be calculated.

3. Time Relay Calibration

The action value, return value and action time, return time can be measured by the DC or AC voltage relay test method when using the manual test method.

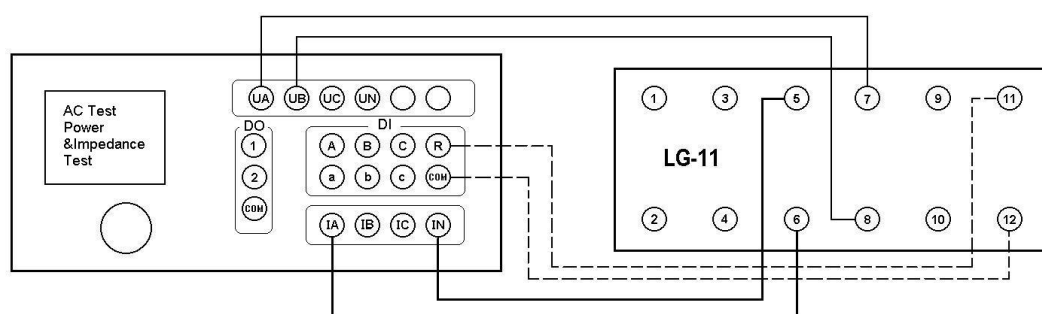
4. Power Relay Calibration

(1) The operating of power directional relay and measurement of sensitive angle

In power test and impedance test, U_{ab} , I_a is set to rated value, and set U_{ab} as phase step, then increase or decrease the voltage phase angle which also can be realized by the method of automatic test. This can measure the either side of boundary angle φ_1 and φ_2 in the action zone, and the sensitive angle $\varphi_{LM} = \frac{1}{2} (\varphi_1 + \varphi_2)$.

(2) Measurement of minimum action power

The angle is arranged in the sensitive angle φ_{LM} , and I_a (or U_{ab}) is set to rated value, U_{ab} (or I_a) is set to zero.



The step of U_{ab} (or I_a) is set, and increase the voltage (or current). Measure the minimum action power, as shown above.

(3) Creeping test

When the current loop is open, the initial value of the U_{ab} is zero, the step length is the rated voltage, and the voltage is suddenly added or removed, the relay contacts should not have the phenomenon of transient connecting.

When the voltage loop is shorted by 20 ohm resistor, set the initial value of I_a is zero, the step length is several times of the rated current, and the current is suddenly add or subtract, relay contacts should not have the phenomenon of transient connecting.

(4) Memory function test

When I_a is set to 0.5 times and some times rated current in the sensitive angle, U_{ab} by 100V sudden drop to zero, the relay action should be reliable, which show that memory function is good.

5. Impedance Relay Calibration

(1) Sensitive angle of the impedance relay and measurement of setting impedance

In power test and impedance test, I_a is set to 5A (or 1A), and set U_{ab} to 0.7 times of the

voltage of the setting impedance, then increase or decrease the voltage phase angle which also can be realized by the method of automatic test. This can measure the either side of boundary angle φ_1 and φ_2 in the action zone, and the sensitive angle $\varphi_{LM} = \frac{1}{2} (\varphi_1 + \varphi_2)$.

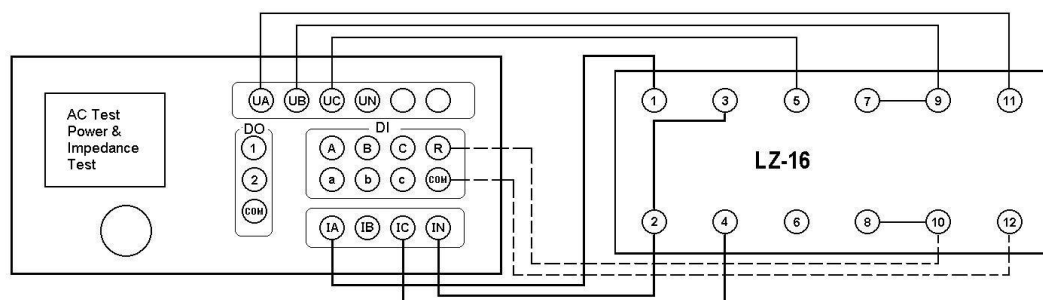
The phase angle is set to φ_{LM} , the voltage is changed from high to low to make the relay operate, the action voltage of U_{DZ} can be got. According to $Z_{SET} = U_{DZ} / I$, the setting impedance of Z_{SET} can be calculated

(2) Measurement of the seiko current curve

The angle between the voltage and current is fixed as φ_{LM} , the current lab is successive changed, then increase or decrease the voltage U_{ab} of each phase current which also can be realized by the method of automatic test. The action value can be measured, and the the seiko current curve can be made by $Z=f(I)$.

(3) 'Bird pecking' phenomenon

When the current loop is open, the initial value of the U_{ab} and step are set is to rated voltage, and the voltage by rated voltage is suddenly drop to zero, the relay contacts should not have the phenomenon of transient connecting. The wiring diagram as shown below.



6. Synchronizing Checking Relay Calibration

(1) Polarity relation check of two coils

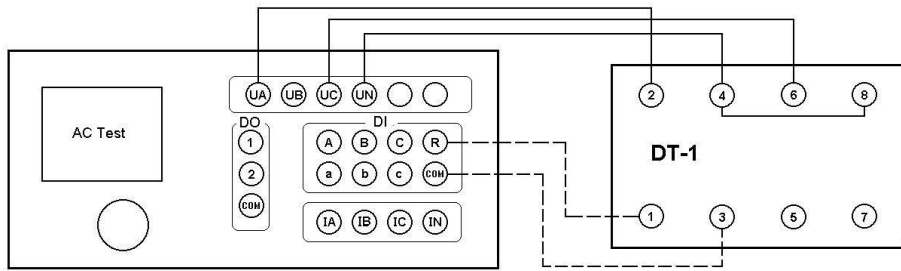
In the AC Test, U_a and U_c are set to rated voltage and connect two coils. The relay won't operate unless any coil is disconnected, which show the 2, 6 is a polar terminal, otherwise 2, 4 for polar terminal.

(2) Measurement of action angle

Adjust the polar terminal, and set U_a, U_c to the rated voltage, and change the angle between the two voltages, the action value and return value can be measured.

(3) Measurement of action voltage and return voltage

Set voltage of a coil is zero, the voltage of another coil from zero gradually increased, which also can be realized by the method of automatic test, to measure action voltage. Then gradually reduce the voltage to measure the return voltage. Exchange coils do the same test. The wiring diagram as shown below.



7. Low Cycle Relay Calibration

In the High-Low Frequency Test, the voltage and current are set to rated value, and the frequency to initial value. Then the frequency step value is changed by manual and the frequency value decreases gradually to measured frequency value and action time of low cycle.

Set the frequency conversion way to automatic frequency conversion mode, and set the $\Delta f/\Delta t$ value of the mode to set value. When reduce the frequency, the relay should not operate, and in the several consecutive tests, the relay still cannot operate.

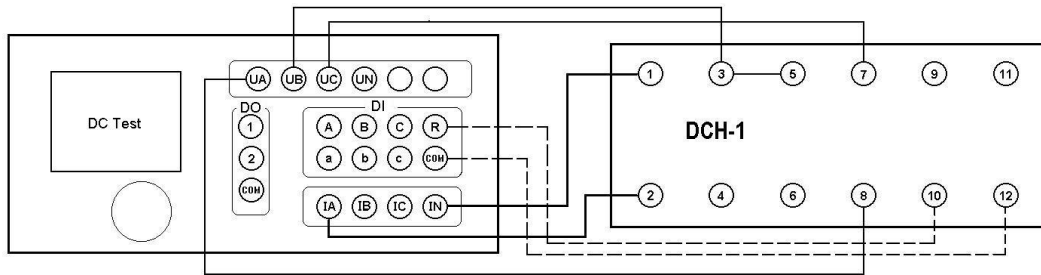
8. Reclosing Relay Calibration

In the DC test, I_a is set to holding current of the intermediate relay, and U_{ab} of charging voltage on the capacitor is set to 220V, which U_a is set to +110V and U_b is set to -110V, and U_c is set to +110V. Then press the key of 'Confirm' and 'Start' to output the voltage of 220V.

Waiting for 15-25 seconds, reclosing capacitor will charge full and signal lights. Then in the output state, click the U_c box, direct input -110, and press the key of enter to set voltage value of U_c to -110V. It is equal to add the start voltage at the seventh terminal to start the reclosing. Then waiting for the reclosing time is over and contact operates to measure the action time.

Note that check the holding current whether output when the reclosing can charge but not operate. During charging, the current output circuit is disconnected and the light of the tester which indicates the current output circuit open should be lighted. And the light shall be

extinguished when reclosing.



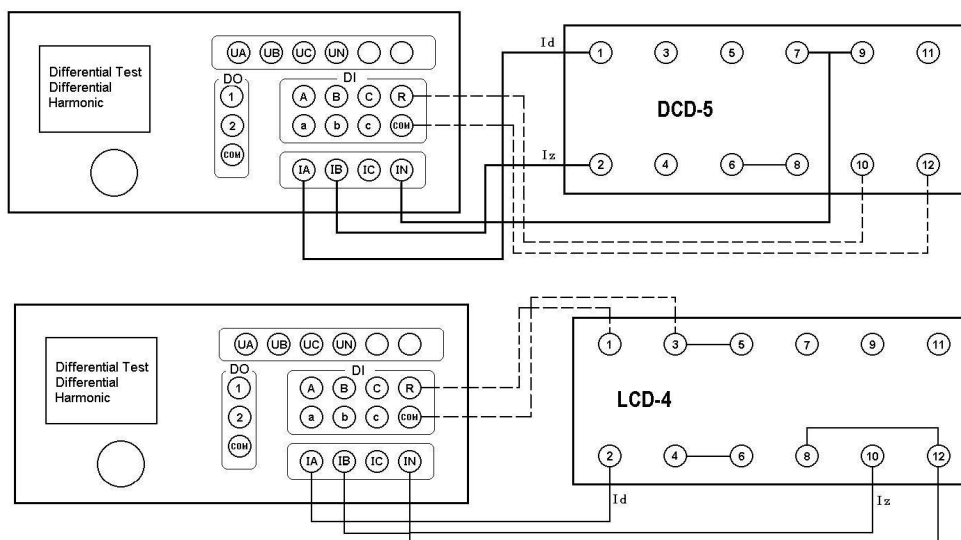
9. Differential Relay Calibration

(1) Measurement of DC magnetic feature

In the differential test, the I_{zd} of braking current is set as the DC current, and change the I_{zd} value gradually, then increase or decrease the action current I_{dz} of each auxiliary magnetic current which also can be realized by the method of automatic test. The I_{dz} of action current can be measured and the braking characteristic curve can be drawn.

(2) Measurement of ratio braking feature

The I_{zd} of braking current is set as the fundamental current, and change the I_{zd} value gradually, then increase or decrease the action current I_{dz} of each braking current. The I_{dz} of action current can be measured and the braking characteristic curve can be drawn.



Attention:

If the differential relay is DCD-----2 (A) , the test wiring is as follows: IA-----7, IB-----9,

IN-----1, DI A-----10, the common terminal of DI +COM-----12, the terminal 3 and 5,6 and 8 of the relay can be shorted respectively.

(3) Measurement of the second harmonic restraint characteristics

The Izd of braking current is set as the current of the second harmonic, and change the Izd value gradually, then increase or decrease the action current Idz of each braking current. The IDZ of action current can be measured and the second harmonic restraint characteristics curve can be drawn.

(4) Measurement of the high harmonic restraint characteristics

In the differential harmonic test, the Izd of braking current is set as the superposition current of each harmonic, and change the Izd value of one harmonic gradually to measure the IDZ of action current.

Appendix 4: Experience Reference for Relay Protection Commissioning

1. The debugging points of overcurrent protection

According to the different object of protection, the one, two or three sections of over-current protection is often used in the test. The three sections of over-current protection will be as an example to start a discussion by a brief description of several key points in the field debugging.

The Calibration of the overcurrent protection generally chooses 'AC test' module.

- If protection does not have direction, only need to add the fault current. Otherwise, the voltage source should be connected to protection. Click the button of 'short-circuit calculation' to do the corresponding short-circuit calculation, and pay attention to the choice of the fault direction.
- When input the fault current to protection alone and if the three-phase input at the same time, please set IA, IB, IC three-phase current of tester to the positive phase, namely 0° , -120° , 120° .
- When adopt the automatic test method to search protection setting value, and if the setting action time of the period which will be operated is tms, the data of $(t+200)$ ms or above can be written in the 'interval time' box to ensure the accuracy of the test value.
- In generally, the 'full-automatic' or 'semi-automatic' mode is always used. It can test the action value of protection by the mode of 'increase progressively' or 'decrease progressively' variable. But the action time is measured by the mode of 'manual'.

Near the critical action, no matter the relay or microcomputer protection, the fault quantity and action time always have the feature of 'inverse time characteristics'. That means the greater the amount of fault quantity or the smaller the distance protection, the the smaller the action time of protection. In order to make the action time tested more accurately in manual mode, the fault quantity, such as voltage amplitude or current amplitude, output by tester should be 1.2 times more than the setting value. Fault impedance output by tester should be 0.8 times less than the setting value. That can make the protection operate more reliable and the action time tends to be stable to closer to the setting action time of protection.

- To the three section of overcurrent protection, it is better to check the the action value of

III segment which has the smaller action current. Please withdraw the the three section of overcurrent protection when check the II section. As well as, please withdraw the the two and three section of overcurrent protection when check the I section. This way can prevent other sections to interference test.

- Sometimes, the setting action current of speed protection in the I section is greatly large and exceeds the maximum current of tester output by single phase. In this time, two-phase or three-phase current of tester can be parallel output.
- The angle of two-phase or three-phase current which has been paralleled should be set to the same, so that the actual output current is the sum of the amplitude of them.
- For the convenience of the recorded data, just choose one phase current as a variable to increase or decrease the current which has been parallel output to make the protection operate.
- The current which come back the IN of tester is always greatly large, please use the thick wire or make two wires be paralleled and make the time of high current should be as short as possible, to ensure the safety of equipment.

When check the relay, in order to prevent the relay contacts jitter, the change of step size should not be set too small, otherwise it will affect the accuracy. In addition, 'The confirm time of switch changed position' should be set to lager, such as 20ms or 40ms, to ignore the relay contacts jitter

2. The debugging scheme of compound voltage lockout overcurrent protection

For the convenience of discussion, suppose that the value of a protection is that the value of overcurrent is 5A, the value of low voltage blocking is 60V, and the value of negative sequence voltage is 6V.

(1) The preparations shall be made as following before the test

The wiring is correct: three-phase voltage terminal should be respectively connected with the three-phase voltage UA, UB, UC of tester. IA of tester should connect with the input terminal of a phase current, such as A phase. Binary input terminals A and common port +KM of tester should be respectively connected to the two terminals of protection tripping. When the protection is active contact, common port +KM of tester should be ensured that it connected with the positive

supply side of protection. It is worth noting that some negative sequence voltage and low voltage of protection are connected with the different voltage terminal, so The wiring should be respectively connected when do the test of 'check the blocking voltage value' and 'check the negative sequence voltage value'.

Please check the value of protection, the function of the compound voltage lockout overcurrent should be put into. If the overcurrent protection action value of II segment is operate, the function of the compound voltage lockout overcurrent of II segment should be put into.

(2) Check the blocking situation

Test parameter is set as shown on the right. The line voltage output by tester is 70V, which the single-phase voltage is 40.4V and the pahse of three-phase voltage UA, UB, UC are 0° -120°, 120°. The line voltage is greater than the blocking voltage of 60V and

Parameter	Amplitude	Change	Step	Max	Phase
<input checked="" type="checkbox"/> UA	40.400		1.000	120	0.0
<input checked="" type="checkbox"/> UB	40.400		1.000	120	-120.0
<input checked="" type="checkbox"/> UC	40.400		1.000	120	120.0
<input checked="" type="checkbox"/> IA	3.000	**	0.100	30	0.0
<input checked="" type="checkbox"/> IB	0.000		1.000	30	-120.0
<input checked="" type="checkbox"/> IC	0.000		1.000	30	120.0
<input checked="" type="checkbox"/> U ₀	10.000		1.000	120	0.0
<input checked="" type="checkbox"/> Hz	50.000		0.000	1000	

the protection is in a locking state. The initial value of the phase current output by the tester is 3A and the step is 0.1A, and then gradually increases the phase current value to 7A to check the protection should not operate.

(3) Check the value of overcurrent

The line voltage output by tester is 50V, which the single-phase voltage is 28.8V and the pahse of three-phase voltage UA, UB, UC are 0°, -120°, 120°. The line voltage is less than the blocking voltage of 60V and the protection which is out of a locking state allow operating.

Parameter	Amplitude	Change	Step	Max	Phase
<input checked="" type="checkbox"/> UA	28.800		1.000	120	0.0
<input checked="" type="checkbox"/> UB	28.800		1.000	120	-120.0
<input checked="" type="checkbox"/> UC	28.800		1.000	120	120.0
<input checked="" type="checkbox"/> IA	3.000	**	0.100	30	0.0
<input checked="" type="checkbox"/> IB	0.000		1.000	30	-120.0
<input checked="" type="checkbox"/> IC	0.000		1.000	30	120.0
<input checked="" type="checkbox"/> U ₀	10.000		1.000	120	0.0
<input checked="" type="checkbox"/> Hz	50.000		0.000	1000	

The initial value of the phase current output by the tester is 3A and the step is 0.1A, and then gradually increases the phase current value to make the protection operate. Then the current of protection can be measured and compared with the overcurrent value of protection setting.

Test parameter is set as shown on the right.

(4) Check the value of blocking voltage

The line voltage output by tester is 70V which is greater than the blocking voltage. The initial

current is 7A, which is greater than the value of overcurrent. Set the voltage as a variable and the step of three-phase voltage is 0.1V. The protection is in a locking state after beginning the test. Then gradually decreases the line voltage value to make the protection operate. Then the line voltage of protection can be measured and compared with the low voltage value of locking.

Note that there is a certain degree of delay from the blocking state to remove blocking state, when reduce the voltage and close to protection action, every step reduced should have enough time to wait for the protection action to ensure the accuracy of the test.

Parameter	Amplitude	Change	Step	Max	Phase
<input checked="" type="checkbox"/> UA	40.400	**	0.100	120	0.0
<input checked="" type="checkbox"/> UB	40.400	**	0.100	120	-120.0
<input checked="" type="checkbox"/> UC	40.400	**	0.100	120	120.0
<input checked="" type="checkbox"/> IA	7.000		0.100	30	0.0
<input checked="" type="checkbox"/> IB	0.000		1.000	30	-120.0
<input checked="" type="checkbox"/> IC	0.000		1.000	30	120.0
<input checked="" type="checkbox"/> Ux	10.000		1.000	120	0.0
<input checked="" type="checkbox"/> Hz	50.000		0.000	1000	

Test parameter is set as shown on the right.

(5) Check the value of negative sequence voltage

Due to the value of the negative sequence voltage is less than the low voltage value of blocking. In order to prevent interference, the the low voltage blocking value of protection is set to 3V, less than the negative sequence voltage.

The initial value of the line negative sequence voltage output by tester is 4V, that the single-phase voltage is 2.3V and the angel of three-phase voltage UA, UB, UC are 0°, -120°, 120°. The line voltage is less than the negative sequence voltage. The initial value of current is 7A , greater than the value of overcurrent. Set the voltage as a variable and the step is 0.1V which the step of UA, UB, UC should be the same. The protection should not be operated after beginning the test. Gradually increases the line voltage value to make the protection operate. Then the voltage of protection can be measured and compared with the value of the negative sequence voltage.

Parameter	Amplitude	Change	Step	Max	Phase
<input checked="" type="checkbox"/> UA	2.300	**	0.100	120	0.0
<input checked="" type="checkbox"/> UB	2.300	**	0.100	120	-120.0
<input checked="" type="checkbox"/> UC	2.300	**	0.100	120	120.0
<input checked="" type="checkbox"/> IA	7.000		0.100	30	0.0
<input checked="" type="checkbox"/> IB	0.000		1.000	30	-120.0
<input checked="" type="checkbox"/> IC	0.000		1.000	30	120.0
<input checked="" type="checkbox"/> Ux	10.000		1.000	120	0.0
<input checked="" type="checkbox"/> Hz	50.000		0.000	1000	

Test parameter is set as shown on the right.

Note that the phase of the three-phase voltage is negative

(6) The whole transmission test

After the each value of protection is set to the initial value, the line voltage which is positive voltage output by tester is 50V and the initial current is set to 7A. Close the breaker to start the

test and make the protection operate to check whether the switch trip successfully.

3. The knowledge of microcomputer transformer differential protection

(1) Transformer connection

The transformer connection type of protection setting is the actual wiring of primary side of transformer, which has the type of $Y/\Delta-11$, $Y/Y(Y0)$, $Y/\Delta-1$ and so on. For the three volume change in the test, the two volumes of them are generally taken out to test and the method of two volumes is the same.

(2) The balance coefficient of high-pressure side

At present, most microcomputer protection always adopts the way of calculation to make the data and phase of $Y-\Delta$ self-correction in the internal protection. Therefore, the external connection is simpler, although the transformer is $Y/\Delta-11$ connection and the CT is Y/Y connection. Of course, there is also a part of the microcomputer protection is not so, which is still CT connection of transformer is corrected.

The setting value of differential protection does not have the balance coefficient of high-pressure side, which brings inconvenience to the test and calculation. We know that the balance coefficient of high-pressure side is 1 by default, but the actual value of balance coefficient is often measured as 1.732. The balance coefficient of high-pressure side can be got as the following method.

In the differential threshold and instantaneous value test, if the actual value of action current is equal to 1.732 times of the setting value, the balance coefficient of high-pressure side is set to 1.732 when computing. If the actual value of action current is equal to the setting value, the balance coefficient of high-pressure side is set to 1 when computing.

(3) The wiring method in the test

When the transformer connection type is $Y/Y(Y0)$, the test wiring is simple. When testing the phase A, the IA of tester is connect with the phase A of high-pressure side and the IB of tester is connect with the phase a of low-pressure side. After the the neutral line of the high and low pressure side shorted, connect with the IN of tester and there does not exist the problem of the compensation current. If the phase B or phase C is tested, the wiring is similar to the above.

When the transformer connection type is Y / Δ-11, the common wiring is that when testing the phase A, the IA of tester is connect with the phase A of high-pressure side and the IB , IC of tester is respectively connect with the phase a, phase c of low-pressure side. After the the neutral line of the high and low pressure side shorted, connect with the IN of tester and the IC is set as compensation current. But how is it to wiring if the phase B or phase C is asked to be tested.

As shown by the vector map on the right the current of high voltage side after conversion should be $I'A = (IA - IB) / 1.732$, $I'B = (IB - IC) / 1.732$, $I'C = (IC - IA) / 1.732$. If phase A of high-pressure side is provided a current value and phase B, phase C are not provided, the three-phase current of high-pressure side after conversion should be as below.

$$I'A = (IA - IB) / 1.732 = (IA - 0) / 1.732 = IA / 1.732;$$

$$I'B = (IB - IC) / 1.732 = (0 - 0) / 1.732 = 0;$$

$$I'C = (IC - IA) / 1.732 = (0 - IA) / 1.732 = - IA / 1.732.$$

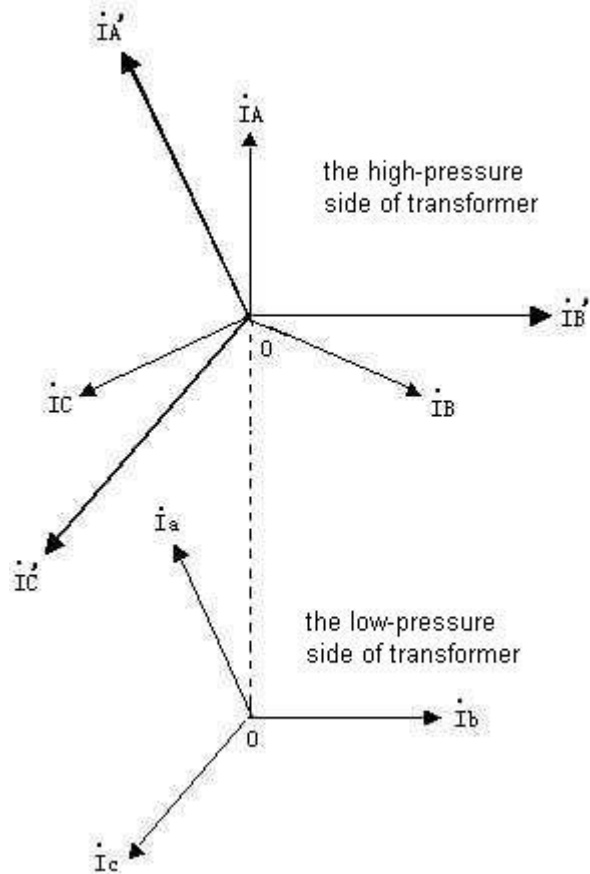
So phase C of high-pressure side is provided a current value, which is equal to the value of phase A and the direction is opposite. During the experiment, in order to balance the current value of phase C of high-pressure side, phase c of low-pressure side should be provided compensation current. And the value of compensation current should be equal to the value of phase a of low-pressure side and the direction is opposite

Similarly, if the phase B of test transformer, the pahse B of high-pressure side should be provided a current value and the phase A or phase C is not provided. According to the above formula, we can get as below.

$$I'A = (IA - IB) / 1.732 = (0 - IB) / 1.732 = -IB / 1.732;$$

$$I'B = (IB - IC) / 1.732 = (IB - 0) / 1.732 = IB / 1.732;$$

$$I'C = (IC - IA) / 1.732 = (0 - 0) / 1.732 = 0.$$



This shows that the phase A of high-pressure side has an equal and opposite current and phase a of low-pressure side should be compensated in the test. Therefore, the correct wiring is that the IA of tester is connect with the phase B of high-pressure side and the IB , IC of tester is respectively connect with the phase B, phase a of low-pressure side. After the the neutral line of the high and low pressure side shorted, connect with the IN of tester and the IC is set as compensation current.

Considering the two current of low-pressure side has the characteristics of 'equal and opposite', the two current for protection can be provided in the test. The correct wiring is that the IA of tester is connect with the phase A of high-pressure side and the IB of tester is connect with the phase a of low-pressure side and the phase a, C negative terminal of protection low-pressure side should be shorted. After the phase c of low-pressure side and the the neutral line of the high and low pressure side shorted, connect with the IN of tester.

From the above analysis is not difficult to find that the current value of the protection low-pressure side should have the opposite with the current value of the high-pressure side and the compensation current value of the low-pressure side should have the opposite with the corresponding current value of the low-pressure side. So when the phase A of transformer is tested and the IA of tester is set to 0°, the current value of IB ,IC of tester should be respectively set to 180°, 0°.

(4) The action equation of protection

Suppose that the differential current of protection is set as I_r , the differential current threshold value is set as I_{cd} , the differential speed concluded value is I_{sd} , inflection point 1 is I_{g1} , the braking coefficient of proportion is $K1$, inflection point 2 is I_{g2} , the braking coefficient of proportion is $K2$, the vast majority of action equations of protection in china is shown as below.

$$I_d > I_{cd} \quad \text{when } I_r < I_{g1};$$

$$I_d > I_{cd} + K * (I_r - I_{g1}) \quad \text{when } I_{g2} > I_r > I_{g1};$$

$$I_d > I_{cd} + K1 * (I_{g2} - I_{g1}) + K2 * (I_r - I_{g2})$$

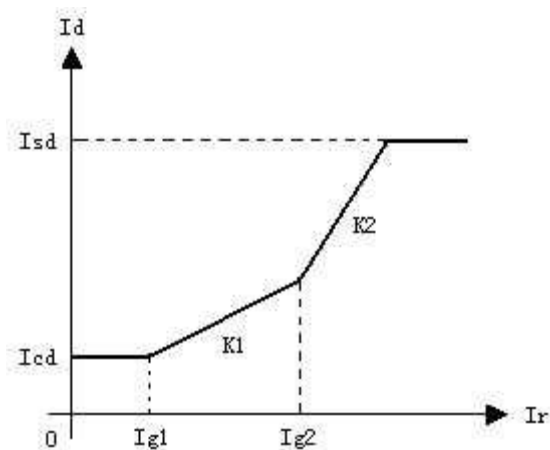
$$\text{when } I_r > I_{g2};$$

$$I_d > I_{sd}$$

The proportion of braking curve is as shown on the right.

As long as one of the above four action equations is satisfied, the action of protection will be exported.

At present, most differential protection only use a



inflection point. Even the differential protection has two inflection points, in order to test more convenient and simple, the setting value of protection is often modified as that $I_{g1} = I_{g2}; K1 = K2$, which can make it be tested by the method of one inflection point. The action equation of proportional braking which has only one one inflection point is as following.

$$I_d > I_{cd} + K * (I_r - I_g) \quad \text{when } I_r > I_g;$$

For the microcomputer differential protection, in fact, the proportion of braking and speed concluded protection is two sets of protection. So many of the protections are set up control word to cast or back the two protections.

No matter the proportion of braking protection or speed concluded protection, the export action time of them is short, which is generally between 30ms and 60ms. They often share a common exit port which brings some inconvenience to the test. Generally, the protection of 'proportion of braking' should be exit by the control word when test the differential protection of speed concluded. If not or some protection do not have this function, the output current should be increased after the proportion of braking protection operating to judge whether the differential protection of speed concluded quickly operate or not by the light of protection or the relevant report.

(5) The relationship between the current value of high and low press side and the value of differential current and braking current

It is worth noting that, during the test, by changing a phase current of tester to make the protection operate, the output current of tester is not action current or braking current and can not influence by the the action principle of differential relays, which will take it for granted that the current of high-pressure side is action current and current of low-pressure side is braking current. The microcomputer differential protection does not directly compare the action current value of the high-pressure side with the action current value of the low-pressure side. It always judge whether has meet the above action equation. What is the relationship between the current value of high and low press side and the value of differential current and braking current?

In general, the differential current of protection in china are always use the equation that $I_d = | I_h + I_l |$, which can be expressed that the value of differential current is equal to and absolute value of the high and low pressure side of vector sum. Therefore, the current direction of the high and low pressure side must be paid attention.

The equations of the braking current often vary between the brand and model, and the most common formula of protection has three kinds in china as below.

1. $I_r = \max \{ | I_h | | I_l | \}$. The correct expression is that the vaule of braking current is equal to

the maximum current amplitude of high and low pressure side.

2. $I_r = (|I_h| + |I_l|) / K$. The correct expression is that the value of braking current is equal to the 1/K times the sum of current amplitude of high and low pressure side.

3. $I_r = |I_l|$. The correct expression is that the value of braking current is equal to the current amplitude of high and low pressure side.

In the formula 2, the value of K in the mostly protection is 2, and in the individual protection is 1.

Besides, The other two formulas will also adopt the equation that $I_r = |I_h - I_l| / K$, $I_r = (|I_d| - |I_h| - |I_l|) / K$.

In fact, the value value of IA, IB output by tester cannot equal to the current value of high and low pressure side when the critical protection operating is record in the test. The balance coefficient of high and low pressure side should be considered. Assume that the IA of tester output to the high-pressure side, the IB of tester output to the low-pressure side, the balance coefficient of high and low pressure side is respectively K1, K2. The current of high-pressure side is set to $I_h = K1 * I_A$, $I_l = K2 * I_B$. Then use the formula of differential current and braking current to calculate the differential current and braking current.

4. Differential protection test

For the convenience of discussion, it is assumed that the setting value of a certain protection is: transformer capacity: 6300 KVA; Rated voltage at high voltage side: 35 KV; CT transformation ratio at high voltage side 150/5; Rated voltage at low voltage side: 6 KV; CT transformation ratio at low voltage side 400/5; Threshold: 2 A; Quick break value: 10A; Inflection point value: 4 A; Proportional braking slope: 0.5; Balance coefficient at low voltage side: 1.38; Transformer wiring type: Y/Δ - 11, harmonic braking coefficient: 0.18.

(1) Correct wiring

The tester IA is connected to protect phase A at the high voltage side, the tester IB is connected to protect phase A at the low voltage side, and the tester IC is connected to protect phase C at the low voltage side; After the N-phase at the high and low voltage sides of the protection is short circuited, connect the IN of the tester.

(2) Differential threshold and quick break value inspection

The tester outputs single-phase current to phase A at the high-voltage side. The initial value is 0, and the step size is 0.1A. Slowly increase the current until the protection acts. Compare the measured action current with the threshold setting of the protection. Generally, the measured

action current is 1.732 times of the protection threshold setting value. This is because the protection has considered the value and phase compensation when processing star delta conversion, otherwise the measured action current should be equal to the protection threshold setting value.

Before measuring the speed break, exit the "proportional braking" protection through the protection control word. The test method is the same as above. Generally, the measured action current is 1.732 times of the protection quick break setting value. If the quick break action value of 1.732 times is large, the tester can be used for two-phase current parallel output (two-phase current phase should be the same), or the quick break setting value in the protection can be set smaller.

(3) Inspection of proportional braking coefficient

Calculation of rated current at high and low voltage sides

$$I_{e1} = (6300 / 35) / (150 / 5) = 6 \text{ A};$$

$$I_{e2} = (6300 / 6) / (400 / 5) = 7.88 \text{ A}$$

Start test

Set $I_A = I_{e1} = 6 \text{ A}$, the phase is 0° ; $I_B = I_{e2} = 7.88 \text{ A}$, phase 180° ; $I_C = I_{e2} = 7.88 \text{ A}$, phase is 0° ;
Set I_A as the variable, and the step size is 0.1 A .

Click the "Start Test" button, and the protection shall not act. Gradually reduce I_A to protection action, record the values of I_A and I_B at this time, assuming $I_A = 5.5 \text{ A}$, $I_B = 7.88 \text{ A}$. In this way, after the first group of data is tested, the initial I_A and I_B (I_C) can be set to be 1.5 times, 2 times, 2.5 times and 3 times of the rated current at the high and low voltage sides respectively. Of course, a group of I_A and I_B values can also be randomly selected, as long as the protection does not act at the start of the test. In addition, it is not necessary to reduce the variables to the protection action. Adding variables can also make the protection action. The measured data also meet the requirements. According to the above method, the I_A and I_B values of other groups of protection actions are tested to verify more groups of data.

Calculation verification

This step is the most critical. For different protections, although the calculation formula of differential current is generally: $I_d = |I_h + I_l|$, the formula of braking current is often different. It also involves the balance coefficient of high and low voltage sides. Because some protections themselves consider the problem of star triangle conversion, while others do not, the balance coefficient of the high-voltage side should sometimes be taken as 1, and sometimes 1.732. Here, taking two common braking current formulas for domestic mainstream protection as examples,

the details are as follows:

(4) Determine the balance coefficient of high voltage side

During the differential threshold and quick break value test, if the measured action current is equal to 1.732 times of the setting value, the HV side balance coefficient is 1.732 during the calculation; if the measured action current is equal to the setting value, the HV side balance coefficient is 1 during the calculation.

$$\text{When } I_r = \max(|I_h|, |I_l|)$$

The high and low voltage side currents measured in the third step above when the protection is critical are: $I_h = I_A = 5.5 \text{ A}$, $I_l = 7.88 \text{ A}$. Assuming that the balance coefficient of the high voltage side has been determined as 1 according to the above method, the differential current and braking current are respectively:

$I_d = |I_h + I_l| = |5.5 - 1.38 \times 7.88| = 5.37 \text{ A}$; Remarks: $I_A (I_h)$ is opposite to $I_B (I_l)$ in phase, and in the formula is the vector sum of high and low voltage side currents

$$I_r = \max\{|I_h|, |I_l|\} = \max\{5.5, 1.38 \times 7.88\} = 10.87$$

For the braking curve with only one inflection point, the action equation of general proportional braking is: $I_d > I_{cd} + K * (I_r - I_g)$, where I_{cd} is the differential gate setting value, I_g is the inflection point setting value, and K is the proportional braking slope required here. The above formula equals sign to get the following equation:

$$I_d = I_{cd} + K * (I_r - I_g),$$

$$5.37 = 2 + K * (10.87 - 4), K = 0.49$$

Compare the measured value with the set proportional braking slope.

$$\text{When } I_r = (|I_h| + |I_l|) / 2$$

Assuming that the method of adding I_A to the protection action is changed from the third step above, a group of high and low voltage side currents measured during the critical action of the protection are: $I_h = I_A = 5.41 \text{ A}$, $I_l = 4.08 \text{ A}$, and assuming that the balance coefficient of the high voltage side has been determined as 1.732 according to the above method, the differential current and braking current are respectively:

$I_d = |I_h + I_l| = |5.41 \times 1.732 - 1.38 \times 4.08| = 3.74 \text{ A}$; Remarks: $I_A (I_h)$ is opposite to $I_B (I_l)$ in phase, and in the formula is the vector sum of high and low voltage side currents

$$I_r = 0.5 * (|I_h| + |I_l|) = 0.5 * (5.41 \times 1.732 + 1.38 \times 4.08) = 7.5 \text{ A}$$

The action equation is substituted as follows:

$$I_d = I_{cd} + K * (I_r - I_g),$$

$$3.74 = 2 + K * (7.5 - 4), K = 0.497$$

Compare the measured value with the set proportional braking slope.

(5) Harmonic braking coefficient test

The tester outputs harmonics to the high-voltage side of the protection, the tester IB outputs harmonics, and the low-voltage side outputs fundamental waves. Output by tester IA. Set the initial output current of the tester to 1A, the IA of the output fundamental wave as a variable, and the step size is 0.1A. After starting the test, the protection does not act. Gradually increase IA to protection action, and record the action value of IA at this time. The harmonic braking coefficient of the protection is:

$$K = (IB / IA) * 100\%$$

Compare the measured braking coefficient with the setting value.

5. RCS — 900 series protection test

(1) RCS — 900 series protective device

model	Main functions	Scope of application
RCS— 901	High frequency locking direction, high frequency locking zero sequence Power frequency variation impedance, two or four section zero sequence Three section grounding and interphase distance, reclosing	220KV and above voltage level transmission line
RCS— 902	High frequency locking distance, high frequency locking zero sequence Power frequency variation impedance, two or four section zero sequence Three section grounding and interphase distance, reclosing	
RCS— 931	Longitudinal split phase differential protection, high-frequency blocking zero sequence Power frequency variation impedance, two or four section zero sequence Three section grounding and interphase distance, reclosing	

RCS— 941	<p>High frequency locking distance, high frequency locking zero sequence (type B)</p> <p>Three section grounding and interphase distance, four section zero sequence</p> <p>Low cycle protection, asymmetric sequential quick action</p> <p>Double circuit line sequential quick action (type B none), reclosing</p>	110KV voltage level transmission line
RCS— 943	<p>Longitudinal split phase differential protection, three section grounding and interphase distance</p> <p>Four section zero sequence, reclosing</p> <p>Asymmetrical sequential quick action and dual circuit line sequential quick action</p>	
RCS— 951	<p>High frequency blocking phase to phase distance (type B), three section phase to phase distance</p> <p>Four section overcurrent, reclosing, low cycle protection</p> <p>Asymmetrical sequential quick action, dual circuit line sequential quick action (type B none)</p>	35~66KV voltage level transmission line
RCS— 953	<p>High frequency blocking phase to phase distance (type B), three section phase to phase distance</p> <p>Four section overcurrent, reclosing, low cycle protection</p> <p>Asymmetrical sequential quick action, dual circuit line sequential quick action (type B none)</p> <p>longitudinal split phase differential protection, three section interphase distance</p> <p>Four section overcurrent, reclosing</p> <p>Asymmetrical sequential quick action and dual circuit line sequential quick action</p>	
RCS— 921	Failure protection and automatic reclosing	
RCS— 922	Proportional differential protection and charging protection	Short circuit device for 3 2 connection and angle type connection of 35~66KV power transmission line

RCS— 923	Failure starting and auxiliary protection	Short circuit breaker failure starting and auxiliary protection can also be used as current protection of buscouple or section switch
RCS— 925	Overvoltage protection and fault starting device	Local discrimination of transmission line overvoltage protection and remote tripping

(2) Directional protection of longitudinal variation (taking locking type as an example for RCS — 901)

Set the transceiver at the "load" position, or connect the sending output of the device to the receiving input to form a spontaneous self receiving. Only the main protection pressing plate is put into operation, and the reclosing handle is switched to "comprehensive weight mode". In the setting protection setting value control word, "Enable pilot distance protection" is set to 1, "Permitted channel" is set to 0, "Enable reclosing" is set to 1, and "Enable reclosing is not checked" is set to 1.

In "AC test", set three-phase normal voltage (amplitude is 57.735V, positive sequence phase), and select "manual test" mode. Start the test and wait for protection charging until the "charging" light is on. Under the condition of not stopping the output, directly change IA to 5A, and change the three-phase voltage to 20V, and then press the "OK" button (note: press the "OK" button after the voltage and current parameters have been modified). At this time, the tester outputs a sudden fault.

According to the above methods, single-phase grounding, two-phase short circuit, two-phase grounding and three-phase positive instantaneous faults can be simulated respectively. The corresponding tripping light on the device panel is on, the LCD displays "longitudinal variation direction", and the action time is 15-30ms. Simulate the above reverse fault, and the pilot protection will not act.

(3) Longitudinal distance protection (RCS — 902/941B/951B, taking locking type as an example)

Set the transceiver at the "load" position, or connect the sending output of the device to the receiving input to form a spontaneous self receiving. Only the main protection pressing plate is put into operation, and the reclosing handle is switched to "comprehensive weight mode". In the setting protection setting value control word, "Enable pilot distance protection"

is set to 1, "Permitted channel" is set to 0, "Enable reclosing" is set to 1, and "Enable reclosing is not checked" is set to 1.

In "AC test", set three-phase normal voltage (amplitude is 57.735V, positive sequence phase), and select "manual test" mode. Start the test and wait for protection charging until the "charging" light is on. Under the condition of not stopping the output, directly change IA to 5A, and change the three-phase voltage to $U=0.95 * I * ZF$ (fixed value of ZF longitudinal distance impedance), and then press the "OK" button (note: press the "OK" button after the voltage and current parameters have been modified). At this time, the tester outputs a sudden fault.

Simulate single-phase grounding, two-phase short circuit, two-phase grounding and three-phase positive instantaneous faults respectively. The corresponding tripping light on the device panel is on, the LCD displays "longitudinal distance direction", and the action time is 15-30ms. Simulate the above reverse fault, and the pilot protection will not act.

(4) Pilot zero sequence protection (RCS — 901/902/941B)

Set the transceiver at the "load" position, or connect the sending output of the device to the receiving input to form a spontaneous self receiving. Enable the main protection pressing plate and zero sequence pressing plate, and switch the reclosing handle to the "comprehensive weight mode". In the setting protection setting value control word, "Enable pilot distance protection" is set to 1, "Permitted channel" is set to 0, "Enable reclosing" is set to 1, and "Enable reclosing is not checked" is set to 1.

In "AC test", set three-phase normal voltage (amplitude is 57.735V, positive sequence phase), and select "manual test" mode. Start the test and wait for protection charging until the "charging" light is on. Under the condition of not stopping the output, directly modify IA to be greater than the overcurrent setting in the zero sequence direction, change the three-phase voltage to 20, and then press the "Confirm" button (note: press the "Confirm" button after the voltage and current parameters have been modified). At this time, the tester outputs a sudden fault quantity to simulate single-phase positive direction transient fault.

The corresponding tripping light on the device panel is on, the LCD displays "longitudinal zero sequence protection", and the action time is 15-30ms. Simulate the above reverse direction fault, and the pilot protection does not act

(5) Optical fiber longitudinal differential protection (RCS — 931/943/953)

Short connect the receiving "RX" and sending "TX" of the optical transceiver (on the CPU plug-in) with pigtails to form a spontaneous self receiving mode. Only the main

protection pressing plate is put into operation, and the reclosing handle is switched to "comprehensive weight mode". In the setting protection setting value control word, "enabling pilot distance protection", "dedicated optical fiber", "channel self loop", "enabling reclosing" and "enabling reclosing unchecked" are all set to 1.

In "AC test", set three-phase normal voltage (amplitude is 57.735V, positive sequence phase), and select "manual test" mode. Start the test and wait for protection charging until the "charging" light is on. Directly modify IA to $I > 1.05 * 0.5 * \text{Max}$ (high fixed value of differential current, $4 * (57.7 / \text{XC1})$) without stopping output, and simulate single-phase or multi-phase faults. Then press the "OK" key (note: press the "OK" key after the voltage and current parameters have been modified).

The corresponding tripping light on the device panel is on, the LCD displays "current differential protection", and the action time is 40~60ms.

Repeat the above test and add fault current $I < 0.95 * 0.5 * \text{Max}$ (low setting of differential current, $1.5 * (57.7 / \text{XC1})$), and the device shall be reliable without action.

(6) Distance protection

Only the distance protection pressing plate is put into operation, and the reclosing handle is switched to the "comprehensive weight mode"; In the setting protection setting value control word, set "Enable the grounding distance of section I" to 1, "Enable the interphase distance of section I" to 1, "Enable re closing" to 1, and "Enable re closing unchecked" to 1

In "AC test", set three-phase normal voltage (amplitude is 57.735V, positive sequence phase), and select "manual test" mode. Start the test and wait for protection charging until the "charging" light is on. Under the condition of not stopping the output, directly modify IA to 5A, and the three-phase voltage to $U = 0.95 * I * \text{ZZD1}$ (ZZD1 is the fixed value of distance I section impedance). Then press the "Confirm" button (note: press the "Confirm" button after the voltage and current parameters have been modified) to simulate the three-phase positive instantaneous fault.

Simulate the single-phase grounding and two-phase grounding positive direction transient faults respectively, the corresponding lights on the device panel are on, the LCD displays "distance I action", and the action time is 10-25ms.

Verify the distance protection of section II and III respectively according to the above method, and note that the time for adding fault value shall be greater than the protection setting time.

Apply fault current of 20A and fault voltage of 0V, respectively simulate single-phase grounding, two-phase short circuit, two-phase grounding and three-phase reverse fault, and distance protection will not act.

(7) Power frequency variation distance protection

Only the distance protection pressing plate is put into operation, and the reclosing handle is switched to the "comprehensive weight mode"; The "power frequency variation impedance" in the setting protection setting value control word is set to 1, and the distance between phases and grounding sections is set to 0.

In "AC test", set three-phase normal voltage (amplitude is 57.735V, positive sequence phase), and select "manual test" mode. Start the test and wait for protection charging until the "charging" light is on. Under the condition of not stopping the output, the current is directly changed to $I = 2I_N$, and the three-phase voltage is changed to be within the range of 0- U_N . Then press the "Confirm" button (note: press the "Confirm" button after the voltage and current parameters have been modified). At this time, the tester outputs a sudden change of fault quantity, respectively simulating the instantaneous fault of A, B, C phase single phase grounding, and the instantaneous fault between AB, BC, CA phases (at the same time, the fault voltage should be within the range of 0-100V);

Analog single-phase ground fault voltage: $U = (1 + K) I * DZZD + (1 - 1.05m) U_N$

Analog interphase fault voltage: $U = 2I * DZZD + (1 - 1.05m) * 100 V$

In the formula, $m=0.9, 1, 1.2$, DZZD - power frequency variation distance setting;

When the power frequency variation impedance is $m=1.1$, it should act reliably, when $m=0.9$, it should not act reliably, when $m=2$, the action time is less than 10ms, and the corresponding light on the device panel is on.

Apply fault current $I < U_n / DZZD$ to simulate various types of outlet faults in the opposite direction respectively, and the power frequency variation distance protection shall not act.

be careful:

The current and voltage must change simultaneously when the test equipment used in the test simulates the fault;

When testing positive direction fault, it must be noted that the full impedance relay restraining DZ action shall be able to be in action state in case of fault.

(8) Zero sequence protection (RCS — 901/902/931)

Only the zero sequence protection pressing plate is enabled, and the reclosing handle is switched to the "integrated weight mode"; In the setting protection setting value control word, "Zero sequence section III passing direction" is set to 1, "switching on again" is set to 1, and "switching on again is not checked" is set to 1

In "AC test", set three-phase normal voltage (amplitude is 57.735V, positive sequence phase), and select "manual test" mode. Start the test and wait for protection charging until the "charging" light is on. Under the condition of not stopping the output, directly modify the current to $I = 1.05 * I_{0Nzd}$ (where I_{0Nzd} is the fixed value of zero sequence overcurrent section I-IV, the same below), and change the three-phase voltage to 20V. Then press the "Confirm" button (note: press the "Confirm" button after the voltage and current parameters have been modified). At this time, the tester outputs a sudden fault quantity to simulate single-phase positive fault.

The corresponding light on the device panel is on, and the LCD displays "zero sequence overcurrent section I" or "zero sequence overcurrent section II" or "zero sequence overcurrent section III" or "zero sequence overcurrent section IV";

Apply fault voltage of 30V, fault current of $0.95 * I_{0Nzd}$, simulate single-phase positive fault, and the zero sequence overcurrent protection will not operate;

Apply fault voltage of 30V, fault current of $1.2 * I_{0Nzd}$, simulate single-phase reverse fault, and the zero sequence overcurrent protection will not operate;

(9) Zero sequence protection (RCS — 941/943)

Only the zero sequence protection pressing plate is enabled, and the reclosing handle is switched to the "integrated weight mode"; In the setting protection setting value control word, "zero sequence section I passing direction" is set to 1, "switching on again" is set to 1, and "switching on again is not checked" is set to 1

In "AC test", set three-phase normal voltage (amplitude is 57.735V, positive sequence phase), and select "manual test" mode. Start the test and wait for protection charging until the "charging" light is on. Under the condition of not stopping the output, directly change the current to $I = 1.05 * I_{0Nzd}$ (where I_{0Nzd} is the fixed value of zero sequence overcurrent section I, the same below), and change the three-phase voltage to 20V. Then press the "OK" key (note: press the "OK" key after the voltage and current parameters have been modified). At this time, the tester outputs a sudden fault quantity to simulate single-phase positive fault.

The corresponding light on the device panel is on, and the LCD displays "Zero sequence overcurrent section I";

Apply fault voltage of 30V, fault current of $0.95 * I_{0Nzd}$, simulate single-phase positive fault, and the zero sequence overcurrent protection will not operate;

Apply fault voltage of 30V, fault current of $1.2 * I_{0Nzd}$, simulate single-phase reverse fault, and the zero sequence overcurrent protection will not operate;

Verify the zero sequence overcurrent protection of section II, III and IV according to the above method, and note that the time for adding fault value shall be greater than the protection setting time.

(10) Overcurrent protection (RCS — 951/953)

Enable only the pressing plate of overcurrent protection section I. In the setting protection setting value control word, "Enable overcurrent direction of section I" is set to 1, "Enable reclosing" is set to 1, and "Enable reclosing is not checked" is set to 1.

In "AC test", set three-phase normal voltage (amplitude is 57.735V, positive sequence phase), and select "manual test" mode. Start the test and wait for protection charging until the "charging" light is on. Under the condition of not stopping the output, directly change the current to $I = 1.05 * I_{1ZD}$ (where I_{1ZD} is the fixed value of overcurrent section I), and change the three-phase voltage to 20V. Then press the "OK" key (note: press the "OK" key after the voltage and current parameters have been modified). At this time, the tester outputs a sudden fault quantity to simulate single-phase, two-phase and three-phase positive fault respectively.

The corresponding light on the device panel is on, and the LCD displays "overcurrent section I";

Apply fault voltage of 30V, fault current of $0.95 * I_{1ZD}$, simulate single-phase, two-phase and three-phase positive fault, and over-current protection will not operate;

Apply fault voltage of 30V, fault current of $1.2 * I_{1ZD}$, simulate single-phase, two-phase and three-phase reverse fault, and the over-current protection will not operate;

Verify the zero sequence overcurrent protection of section II, III and IV according to the above method, and note that the time for adding fault value shall be greater than the protection setting time.

(11) Low cycle protection (RCS — 941/951)

Only the low cycle protection strap is enabled. Set "Enable low cycle protection" to 1, "Enable reclosing" to 1, and "Enable reclosing unchecked" to 1 in the setting protection

setting value control word.

In the "frequency and high and low cycles" module, select the "action frequency" test item, and set the "delay before frequency change" as 20s. On the "Operation frequency" page, set the three-phase current as 2A (all should be greater than 0.06IN), set the initial frequency as 50Hz, the termination frequency as less than the set frequency value, and set the "df/dt value during test" as 0.5Hz/s.

After starting the test, the tester outputs three-phase symmetrical voltage (the voltage between three phases should be greater than the low cycle low voltage setting), three-phase current simulates the normal system state, and waits for protection charging until the "charging" light is on.

After the end of "time delay before frequency change", the tester automatically and smoothly reduces the frequency of three-phase voltage to below the low frequency setting value of low cycle protection, and waits for the device action outlet. The corresponding tripping light on the device panel is on, the "charging" light is off (low cycle protection action lockout reclosing), and the LCD displays "low cycle action";

Set "low cycle protection slip locking" in setting protection setting value control word to 1.

Select the test item of "df / dt locking". On the "df/dt lockout" page, set the initial value of df/dt change to be greater than the set slip lockout value, and the final value to be less than the set slip lockout value, with a change step of 0.1 Hz/s. Simulate that when the slip applied in the test is less than the low cycle slip locking value, the protection will open the low cycle protection. When the slip applied in the test is greater than the low cycle slip locking value, the protection should reliably lock the low cycle protection.

The software can automatically change the system output frequency according to different df/dt values, and gradually search out the df/dt value of critical action of the device, which is considered as "df/dt lockout".

(12) Channel joint commissioning (RCS — 941/951)

High frequency channel

Turn on the protection devices on both sides and the transceiver, set the transceiver at the channel position, enable the main protection, distance protection, zero sequence overcurrent protection strap, and close the circuit breaker;

Channel test:

Press the "Channel Test" button on the protection screen, the local side will send a message immediately, stop the message after 200ms of continuous sending, the opposite side will send a message to the local side for 10ms of continuous sending via the remote start circuit, and stop the message after 5s of continuous receiving on the local side, the local side will send a message again for 10s, and then stop the message;

Failure test:

Apply fault voltage of 0V and fault current of 10A to simulate various positive faults. The pilot protection shall not act. Turn off the power supply of the transceiver on the opposite side. With the fault amount, the pilot protection shall act.

Digital channel

Connect the optical transceiver (CPU plug-in) of the devices on both sides through a special optical fiber or PCM machine. Set the "channel self loop" in the protection setting control word to 0. If the channel is normal, the "channel abnormal" indicator of the devices on both sides will not be on.

6. Partial protection of NARI

(1) RCS-901 microcomputer line protection

be careful:

During the test, the "state before fault" of sufficient length shall be output first, and the "TV disconnection" light shall be off; If the reclosing condition is to be tested, wait until the reclosing charging indicator is on. Therefore, the time before fault may be set to a large value, such as 28s (longer than the reclosing charging time). Each positive sequence sensitive angle or zero sequence sensitive angle of each test shall be set according to the setting sheet.

- Direction of longitudinal change

Enable only the main protection strap, simulate the distance or zero sequence fault of section II, and the text of the protection action report is: "Direction of longitudinal variation".

- Longitudinal zero sequence direction

Enable the main protection and zero sequence pressing plate, simulate the zero sequence fault of section II, and the text of the protection action report is: "longitudinal variation direction" and "longitudinal zero sequence direction". If it is required to report only the "longitudinal zero sequence direction", the "longitudinal change direction" in the control word can be set to 0 before the test.

Simulate the reverse direction fault in the software, and the protection shall not act.

- Power frequency variation impedance

Only the distance protection strap is put into use and tested in the "Power frequency variation impedance setting verification" test item of the "Line protection" module. Input the fixed value of "power frequency variation impedance", and set the fault current large enough, such as 10A or above, otherwise the calculated voltage may be negative. Simulate reliable action at 1.1 times, reliable inaction at 0.9 times, and test action time at 1.2 times. The text of protection action is "power frequency variation impedance".

- Distance protection

Only the distance protection strap is put into use and tested in the "impedance setting verification" test item of the "line protection" module. When checking the grounding distance impedance, ensure that the zero sequence compensation coefficient is set correctly before the test. The report of protection action is: "Distance XX section". Observe whether the test phase in the message is consistent with the current simulated fault.

When single phase grounding distance section I and II act, the protection shall be single tripping, and when section III acts, the protection shall be triple tripping. The interphase grounding distance and each section of interphase distance act, and the protection is triple tripping.

- Zero sequence protection

Only the zero sequence protection strap is enabled and tested in the "Zero sequence current setting verification" test item of the "Line protection" module. The report of protection action is: "Zero sequence XX section". Observe whether the test phase in the message is consistent with the current simulated fault.

When zero sequence section I and II act, the protection shall be single tripping, and when section III acts, the protection shall be triple tripping.

- Reclosing and post acceleration

If the zero sequence protection is simulated, only the zero sequence protection strap will be enabled. If the distance protection is simulated, only the distance protection strap will be enabled and tested in the "Automatic reclosure and post acceleration" test item of the "Line protection" module. For setting two faults before and after reclosing, various time parameters can be set larger, such as 3s or 5s. The tester can control the test process according to the received protection signal, and the time before fault should be greater than the protection charging time.

If the grounding distance fault is simulated, the zero sequence compensation coefficient

should also be correctly set.

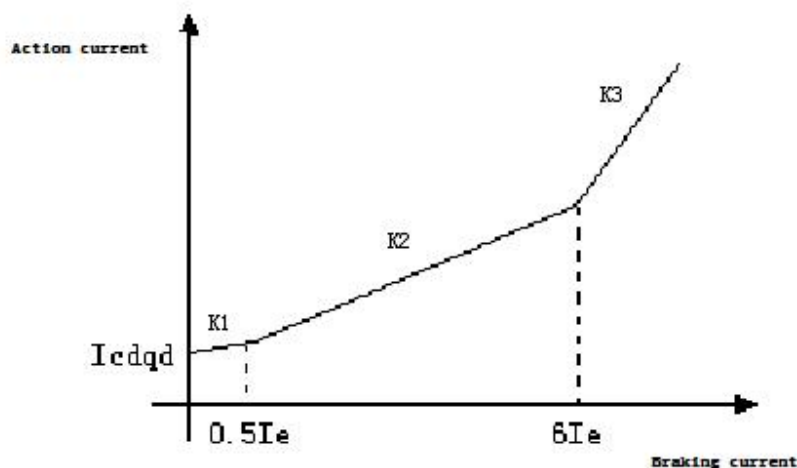
- TV short line phase overcurrent or TV short line zero sequence overcurrent

Enable zero sequence pressing plate, output single-phase current greater than the setting value in "AC test", or simulate zero sequence fault. The fault shall be output before the "TV short line" signal lamp is off. Both tests report "TV short line overcurrent".

(2) RCS-978 transformer differential protection

- Braking characteristics
- Description of braking characteristics: the above curve actually has three inflection points, $I_{g1}=0$, $I_{g2}=0.5I_e$, $I_{g3}=6I_e$
- Test wiring

This protection is different from the transformer protection of common high-voltage side corner because it is a low-voltage side corner protection.



6 current outputs

Y/Y side test (hereinafter referred to as side I and side II)

The three phases at side I and II are connected with positive polarity, and the corresponding phase currents at side I and II are staggered by 180° . Apply the current I^* (per unit value, I^* times the rated current, and its base value is the rated current of the corresponding side) to both sides I and II with "AC test", and the device shall have no differential current.

For example, if I^* is 0.5, $0.5 \cdot I_{e1}$ (I_{e1} is the rated current of side I) three-phase current should be applied at Y side, and $0.5 \cdot I_{e2}$ (I_{e2} is the rated current of side Δ) three-phase current should be applied at II side. The device should have no differential current.

Y/ Δ - 11 Two side test (hereinafter referred to as side I and III)

Three phases at side I and III are connected with positive polarity, and the current at side I shall be 150° ahead of the corresponding phase current at side III. Apply the current I^* (per unit value, I^* times the rated current, and its base value is the rated current of the corresponding side) to both sides I and III with "AC test", and the device shall have no differential current.

For example, if I^* is taken as 1, $1 \cdot I_{e1}$ (I_{e1} is the rated current of Y side) three-phase

current should be applied at I side, and $1 \cdot I_{e2}$ (I_{e2} is the rated current of Δ side) three-phase current should be applied at III side, and the device should have no differential current.

3 current outputs

Y/Y side test (hereinafter referred to as side I and side II)

When conducting side I and II (Y/Y connection) tests, apply current I^* to phase A on either side. According to the phase adjustment methods of the device, there are (the current in the following formula is vector):

$$I_{A'} = I_A - I_0; \quad I_{B'} = I_B - I_0; \quad I_{C'} = I_C - I_0$$

And because: $|3I_0'| = |I_A + I_B + I_C| = I^*$

therefore: $|I_{A'}| = 2I^*/3$

$$|I_{B'}| = I^*/3$$

$$|I_{C'}| = I^*/3$$

Therefore, both B and C phases will be affected. In order to avoid this impact and make the test easier, the wiring mode adopted on both sides I and II is: the current enters from the polarity end of phase A, flows out into the non polarity end of phase B, and flows back to the tester from the polarity end of phase B. In this way:

$$|3I_0'| = |I_A + I_B + I_C| = |I^* + (-I^*) + 0| = 0$$

therefore: $|I_{A'}| = I^*$

$$|I_{B'}| = -I^*$$

$$|I_{C'}| = 0$$

1. The phase angle of the current applied at side II is 180° , the size is I^* , and the device should have no differential current.

Y/ Δ - 11 Two side test (hereinafter referred to as side I and III)

During the I and III tests, the wiring mode adopted is: the current at side I enters from the polarity terminal of phase A, flows out and enters the non polarity terminal of phase B, and flows back to the tester from the polarity terminal of phase B; The current at side III enters from the polarity terminal of phase A and flows back to the tester from the non polarity terminal of phase A.

In this way, there are:

$$|I_{A'}| = I^*$$

$$|I_{B'}| = -I^*$$

$$|I_{C'}| = 0$$

Side III:

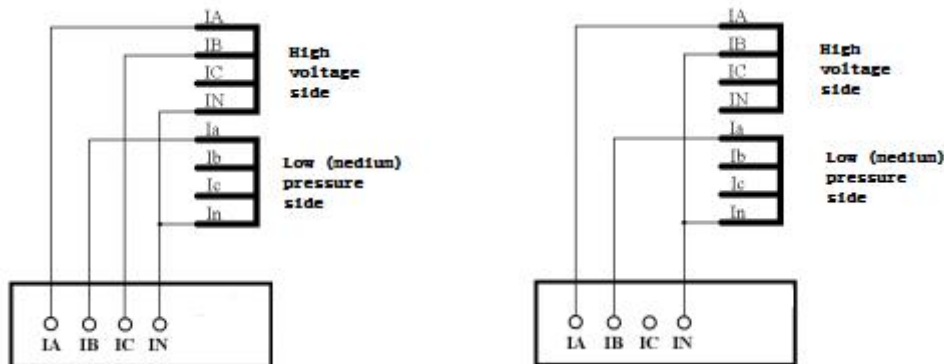
$$|I_{a'}| = |(I_a - I_c)| / 1.732 = I^* / 1.732;$$

$$|I_b'| = |I_b - I_a| / 1.732 = I^* / 1.7322;$$

$$|I_c'| = |I_c - I_b| / 1.732 = 0$$

For side III, the phase angle of the current added to side I and III is 180°, the size of side I is I^* , and that of side III is $1.732 I^*$. The device should have no differential current.

The wiring diagram is as follows:



The tester outputs three circuits of current, and the IC is the compensation current. The tester outputs two circuits of current for self compensation

Equilibrium coefficient

Calculation of primary rated current at each side of transformer

$$I_{1n} = S_n / (1.732 \cdot U_{1n})$$

Where S_n is the maximum rated capacity of the transformer and U_{1n} is the rated voltage at the calculation side of the transformer.

Calculation of secondary rated current at each side of transformer

$$I_{2n} = I_{1n} / n_{LH}$$

Where I_{1n} is the primary rated current at the calculation side of the transformer, n_{LH} is the TA transformation ratio at the calculation side of the transformer.

Calculation of balance coefficient at each side of transformer

$$K_{ph} = K_b \cdot I_{2n \min} / I_{2n}, \text{ where } K_b = \min(I_{2n \max} / I_{2n \min}, 4)$$

Where, I_{2n} is the secondary rated current at the calculation side of the transformer, $I_{2n \min}$ is the minimum secondary rated current at each side of the transformer, and $I_{2n \max}$ is the maximum secondary rated current at each side of the transformer.

test method

The following only discusses the test of Y/ Δ - 11 side, and only describes the proportional braking test method. For the convenience of illustration, it is assumed that the parameters and calculated values of a transformer are:

project	High	Medium	Medium
---------	------	--------	--------

	pressure side (I side)	pressure side (II side)	pressure side (II side) Low pressure side (III side)
Maximum capacity of transformer Se	180MVA		
Voltage level Ue	225.5KV	118KV	37.5
Wiring mode	Y	Y	Δ -11
TA transformation ratio at each side nTA	1200A/5A	1200A/5A	2000A/5A
Transformer primary rated current I1e	460.87A	880.73A	2771.36A
Transformer secondary rated current I2e	1.920A	3.665A	6.925A
Balance coefficient K on each side	3.606	1.889	0.999

Setting value of transformer main protection:

Differential starting current: 0.3Ie

Proportional braking coefficient: 0.5

Differential quick break: 6.0Ie

Sampling value check

In the "AC test", when $1 * 1.920A = 1.920A$ (1 is the standard unit value) single-phase current is applied to phase A on side I, and $1 * 1.732 * 6.925A = 11.994A$ single-phase current is applied to phase A on side III, the device shall have no differential current.

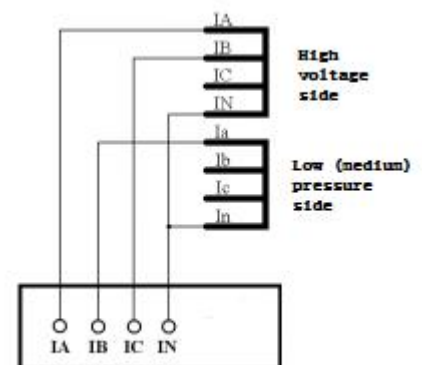
When only $1 * 1.920A = 1.920A$ single-phase current is applied to phase A at side I, the phase difference current A of the device shall be $0.667Ie$, and the phase difference current B and C shall be $0.333Ie$.

Test and calculation of proportional braking coefficient

The test wiring is shown in the right figure:

In the "AC test", set the initial current $I_A = 3$, the phase is 0° , $I_B = 3$, the phase is 180° , $I_C = 3$, and the phase is 0° ; Set I_C as the variable and the step size is $0.1A$.

At the beginning of the test, the differential



protection shall not act. Reduce IC by step (note: variable can also be added) to differential protection action, record the value of IC at this time, and assume it is IC1. In this way, a group of data is obtained: the current on the high voltage side is 3A, and the current on the low voltage side is IC1.

Perform data processing as follows:

Look for another set of data. In the "AC test", set the initial current IA=5, the phase is 0 °, IB=5, the phase is 180 °, IC=5, and the phase is 0 °; Set IC as the variable and the step size is 0.1A.

At the beginning of the test, the differential protection shall not act. Reduce IC by step to differential protection action, record the value of IC at this time, and assume it is IC2. In this way, another set of data is obtained: the current on the high-voltage side is 5A, and the current on the low-voltage side is IC2.

(3)BP-2B bus differential protection

The action expression is:

$$I_d > I_{dset}$$

$$I_d > K_r * (I_r - I_d)$$

Where I_{dset} is the fixed value of differential threshold, K_r is the complex proportional coefficient (braking coefficient).

And:

I_d =absolute value of current vector sum of each element on the bus

I_r =scalar sum of current of each element on the bus

A Analog bus out of area fault

Conditions: No voltage is applied to make the "Lock Open" light on

a) Select any two branches on the same bus with the same transformation ratio, and use the "AC test" to output two currents of equal size and opposite direction to the two branches (both connected to the A-phase input of the branch).

b) When the two currents are changed in the same step size, the bus differential protection shall not act at all times;

c) In the observation panel display, the large differential current and small differential current should always be equal to zero.

B Simulate fault in bus area

Conditions: No voltage is applied to make the "Lock Open" light on

1 Verify differential threshold

a) Select a branch on the bus optionally, use "AC test" to output a phase current to a certain phase of the branch, and gradually increase the output current value from 0 to the protection action. Compare the action current with the setting value of differential threshold.

b) The bus differential protection shall act instantaneously, cut off the bus coupler and all branches on the bus where the branch is located, and the bus differential action signal light is on.

2. Check the high value of differential proportional braking coefficient (the differential threshold can be appropriately lowered)

- a) Buscouple switch
- b) Select two branches on bus I with the same transformation ratio, and use "AC test" to output two currents of equal size and opposite direction to two branches (both connected to the A-phase input of the branch).
- c) Select a branch on bus II with the same transformation ratio, and use "AC test" to output another phase current to phase A of the branch. Adjust the output current to make bus II differential action.
- d) Record the applied current and verify the large difference proportional coefficient.

3. Check the low value of large difference proportional braking coefficient (the differential threshold can be appropriately lowered)

- a) Buscouple breaking switch
- b) Select two branches on bus I with the same transformation ratio, and use "AC test" to output two currents of equal size and opposite direction to the two branches (both connected to the A-phase input of the branch).
- c) Then select a branch on bus II with the same transformation ratio, and use "AC test" to output another phase current to phase A of the branch. Adjust the output current to make bus II differential action.
- d) Record the applied current and verify the large difference proportional coefficient.

4. Check the differential proportional braking coefficient (the differential threshold can be appropriately lowered)

- a) Select two branches on bus I with the same transformation ratio, and use the "AC test" to output the currents with different two-phase sizes and opposite directions to the two branches (both connected to the A-phase input of the branch).
- b) Set the current output of one circuit unchanged, and adjust the current of the other phase to make the bus differential action.
- c) Record the applied current and verify the small difference proportional coefficient.

C Simulate fault in bus zone during double bus switching operation

Conditions: No voltage is applied to make the "Lock Open" light on

- 1 Select any branch on a bus and close bus I and bus II switches of the branch.
- 2 Use "AC test" to output a phase current to a phase in the branch, and the current value is greater than the differential threshold setting value.
- 3 The bus differential protection shall act instantaneously to cut off the bus coupler and all branches on the bus.
- 4 The differential action signal lamps of bus I and bus II are on.

D Failure protection outlet logic test

Conditions: No voltage is applied to make the "Lock Open" light on

1 Select a branch on the bus optionally, and input the "failure start" pressing plate of the branch.

2 On the cabinet terminal strip, short circuit the "failure start" input terminal of the branch with the "input circuit common terminal" terminal.

3 After a short time delay t_1 , the protection will cut off the bus coupler, and after a long time delay t_2 , the protection will cut off all the branches of the bus where the branch is located.

4 The failure action signal lamp is on.

E Buscouple failure protection test

Conditions: No voltage is applied to make the "Lock Open" light on

1 Select two branches on the bus, and place the two branches on bus I and bus II respectively.

2. Use "AC test" to output three-phase currents with the same size and direction to two branch circuits and buscouple (both connected to the A-phase input of the two branch circuits and the A-phase input of the buscouple, and simulate the buscouple CT at the I-bus side of the switch). BP-2B protection default bus coupler belongs to II bus element.

3 The applied single-phase current shall be greater than the overcurrent setting of bus coupler failure protection (and greater than the differential threshold setting), and the bus coupler current shall be continuously loaded.

4 The bus differential protection shall operate instantaneously to cut off all branches on the bus coupler and bus II first, and the device will cut off other branches on bus I through "bus coupler failure delay".

F Bus charging protection

Conditions: No voltage is applied to make the "Lock Open" light on

1 Put the "bus charging protection" strap into operation.

2. Disconnect the bus coupler switch.

3 Use "AC test" to output a phase current to a certain phase of bus coupler, and the current is greater than the fixed value of charging protection current.

4 The bus charging protection operates in a delayed manner, and the bus coupler switch is cut off.

5 The charging protection action signal lamp is on.

6 Buscouple overcurrent protection

Conditions: No voltage is applied to make the "Lock Open" light on

7 Put the pressing plate of "bus overcurrent protection" into operation.

8 correspondingly, the fixed value of non test items in buscouple overcurrent or buscouple zero sequence overcurrent is temporarily increased, or the three-phase short-circuit fault output can be simulated during the test overcurrent (there is no zero sequence current at this time).

9 Use "AC test" to output a phase current to a phase input of the bus coupler. The current value is greater than the bus coupler overcurrent setting value and less than the bus coupler zero sequence current setting value. The bus coupler overcurrent protection acts and the bus coupler switch is cut off.

10 Buscouple overcurrent protection action signal lamp is on.

11 Disconnect the overcurrent and recover the signal.

12 Use "AC test" to output a phase current to a phase input of the bus coupler. The current value is greater than the bus coupler zero sequence overcurrent setting value and less than the bus coupler overcurrent setting value.

13 The bus coupler overcurrent protection acts and the bus coupler switch is cut off.

14 Buscouple overcurrent protection action signal lamp is on.

15 Composite voltage lockout

16 Use "AC test" to output three-phase normal symmetrical voltage (amplitude is 57.735V, positive sequence phase) to bus I voltage input circuit.

17 Select a branch on bus I optionally, and use "AC test" to output a phase current to a phase input of the branch, and the current value is greater than the threshold setting value.

18 The bus differential protection shall not act.

(4) RCS-915 bus differential protection

The test method is basically the same as BP-2B, please refer to it!

The action expression is:

$$I_d > K_r * I_r$$

Where I_r is the braking current and K_r is the multiple proportional coefficient (braking coefficient).

And:

I_d =absolute value of current vector sum of each element on the bus

I_r =scalar sum of current of each element on the bus

- Buscouple dead zone protection

- Female union position

Simulate the fault in the bus area. After the protection sends the bus trip order, continue to connect the fault current. After the setting delay T_{sq} , the bus tie dead zone protection acts to cut off the other bus.

- Buscouple split position

Simulate the fault in the bus area, and the protection shall only trip the bus at the dead zone side. (Note: Before the fault, the voltage of both buses must meet the voltage locking conditions)

- Constant value analysis

- ILcd

Low setting of differential starting current. The setting value is set to prevent the tripping of the large power supply side of the bus fault and the return of the differential starting element. It can meet the sufficient sensitivity setting according to the removal of the small power supply. If there is no large or small power supply, set it to $0.9 I_{hcd}$.

K L

Low setting of proportional braking coefficient. When the bus coupler switch is disconnected and the weak power supply bus fails, the large difference proportional differential element has sufficient sensitivity.